Formerly Utilized Sites Remedial
Action Program (FUSRAP)

Maywood Chemical Company Superfund Site

ADMINISTRATIVE RECORD

Document Number

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US Army Corps
of Engineers®

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SEP 29 1989

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Attention: Robert G. Atkin
Technical Services Division

Subject: Bechtel Job No. 14501, FUSRAP Project
DOE Contract No. DE-AC05-81OR20722
Publication of Radiological Characterization Report
for seventeen residential properties, four municipal
properties, and seven commercial properties in
Lodi and Maywood, New Jersey
Code: 7315/WBS: 138

Dear Mr. Atkin:

Enclosed is one copy each of the 28 subject published reports for the properties listed in Attachment 1. These reports incorporate all comments received in this review cycle (CCNs 063165, 063327, 062285, and 061568) and are being published with approval of Steve Oldham, as reported in CCN 063868.

Also enclosed (as Attachment 2) is a proposed distribution list for these reports. Please send us any changes to the proposed distribution list at your earliest convenience so we may distribute the reports.

BNI would like to express our thanks to Mr. Oldham for his cooperation and efforts to review these drafts in an accelerated manner. His efforts have allowed us to publish these reports on schedule. If you have any questions about these documents, please call me at 576-4718.

Very truly yours,

R. C. Robertson
R. C. Robertson
Project Manager - FUSRAP

RCR:wfs:1756x
Enclosure: As stated

cc: J. D. Berger, ORAU (w/e)
N. J. Beskid, ANL (w/e)

CONCURRENCE

[illegible]	[illegible]			

DOE/OR/20722-253

RADIOLOGICAL CHARACTERIZATION REPORT FOR THE COMMERCIAL PROPERTY AT 80 HANCOCK STREET LODI, NEW JERSEY

SEPTEMBER 1989

Prepared for

UNITED STATES DEPARTMENT OF ENERGY

OAK RIDGE OPERATIONS OFFICE

Under Contract No. DE-AC05-81OR20722

By

N. C. Ring, D. J. Whiting, and W. F. Stanley

Bechtel National, Inc.

Oak Ridge, Tennessee

Bechtel Job No. 14501

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ABBREVIATIONS

cm	centimeter
cm^2	square centimeter
cpm	counts per minute
dpm	disintegrations per minute
ft	foot
h	hour
in.	inch
km^2	square kilometer
L	liter
L/min	liters per minute
m	meter
m^2	square meter
MeV	million electron volts
μR/h	microroentgens per hour
mi	mile
mi^2	square mile
min	minute
mrad/h	millirad per hour
mrem	millirem
mrem/yr	millirem per year
pCi/g	picocuries per gram
pCi/L	picocuries per liter
WL	working level
yd	yard
yd^3	cubic yard

1.0 INTRODUCTION AND SUMMARY

This section provides a brief description of the history and background of the Maywood site and its vicinity properties. Data obtained from the radiological characterization of this vicinity property are also presented.

1.1 INTRODUCTION

The 1984 Energy and Water Appropriations Act authorized the U.S. Department of Energy (DOE) to conduct a decontamination research and development project at four sites, including the site of the former Maywood Chemical Works (now owned by the Stepan Company) and its vicinity properties. The work is being administered under the Formerly Utilized Sites Remedial Action Program (FUSRAP) under the direction of the DOE Division of Facility and Site Decommissioning Projects. Several residential, commercial, and municipal properties in Lodi, New Jersey, are included in FUSRAP as vicinity properties. Figure 1-1 shows the location of the Lodi vicinity properties in relation to the former Maywood Chemical Works.

The U.S. Government initiated FUSRAP in 1974 to identify, clean up, or otherwise control sites where low-activity radioactive contamination (exceeding current guidelines) remains from the early years of the nation's atomic energy program or from commercial operations that resulted in conditions Congress has mandated that DOE remedy (Ref. 1).

FUSRAP is currently being managed by DOE Oak Ridge Operations. As the Project Management Contractor for FUSRAP, Bechtel National, Inc. (BNI) is responsible to DOE for planning, managing, and implementing FUSRAP.

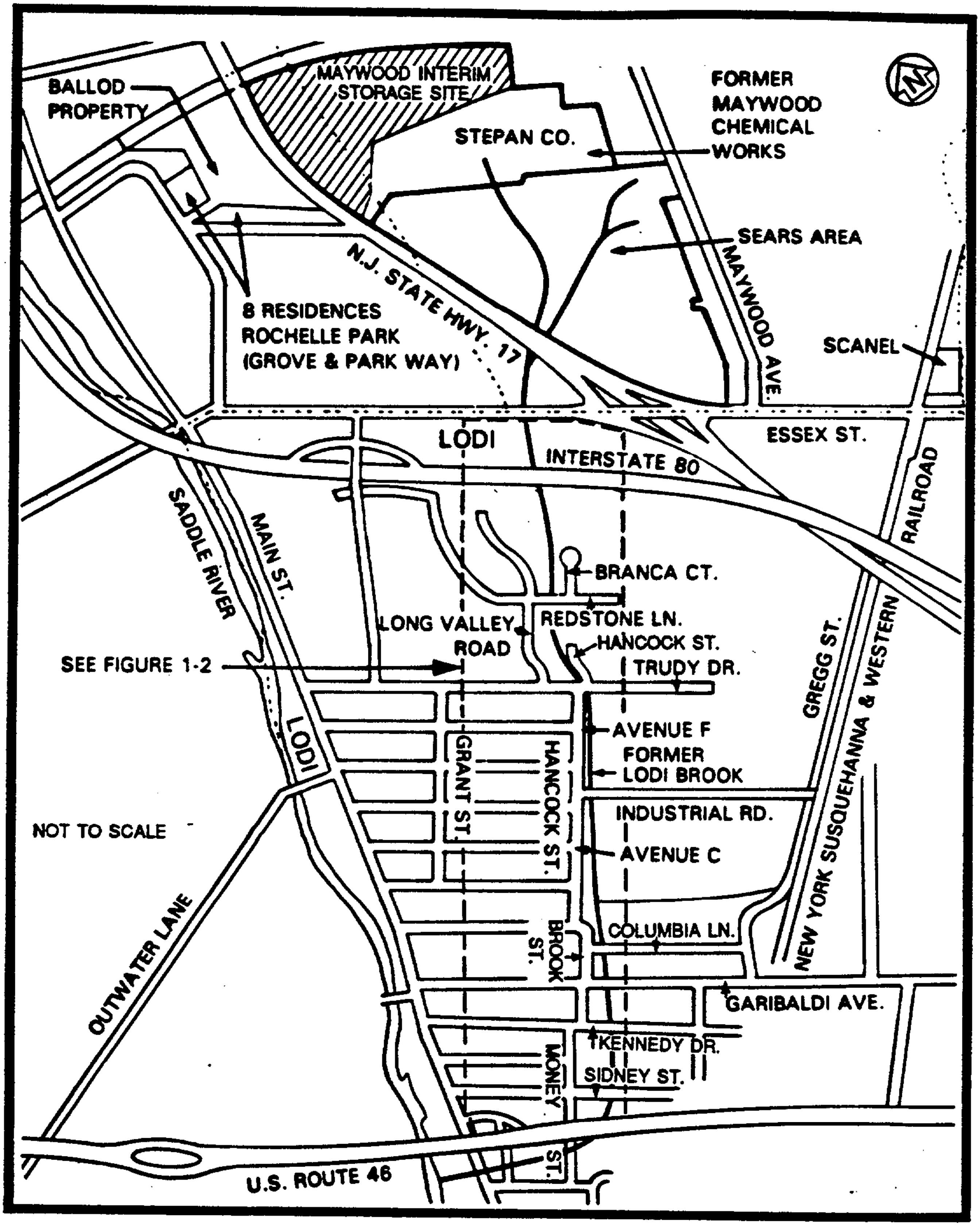

FIGURE 1-1 LOCATION OF LODI VICINITY PROPERTIES

1.2 PURPOSE

The purpose of the 1987 survey performed by BNI was to locate the horizontal and vertical boundaries of radionuclide concentrations exceeding remedial action guidelines.

1.3 SUMMARY

This report details the procedures and results of the radiological characterization of the property at 80 Hancock Street (Figure 1-2) in Lodi, New Jersey, which was conducted in December 1987. Additional data were obtained in September and December 1988 to complete characterization of the property.

Ultimately, the data generated during the radiological characterization will be used to define the complete scope of remedial action necessary to release the site.

The property located at 80 Hancock Street is a commercial property used primarily for the filling and distribution of liquid gas cylinders. It consists of a concrete block structure, with an office area in the front and a work area (including loading docks) in the rear. The structure is bordered on three sides by an asphalt-paved parking/shipping area. The property is situated on the corner of Hancock Street and Industrial Road in a densely populated residential neighborhood. It is bordered on three sides by other commercial properties, with residences located across from it on Hancock Street. Because of the significant safety hazards presented by the type of business operated on this property, indoor characterization activities were severely limited and had to be confined to the office area of the building.

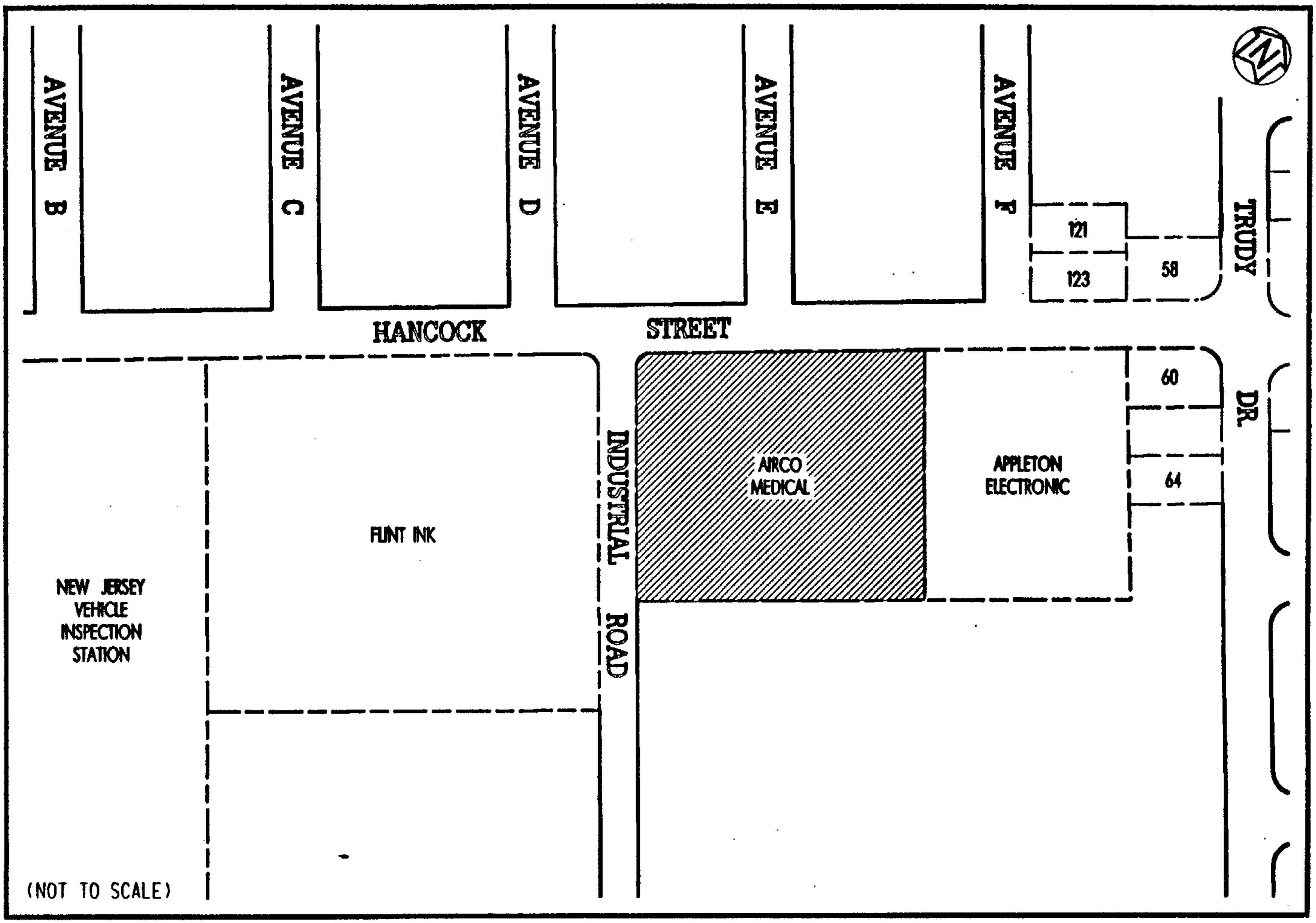

FIGURE 1-2 LOCATION OF 80 HANCOCK STREET

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This characterization confirmed that thorium-232 is the primary radioactive contaminant at this property. Results of surface soil samples for 80 Hancock Street showed maximum concentrations of thorium-232 and radium-226 to be less than 8.6 and less than 1.4 pCi/g, respectively. The maximum concentration of uranium-238 in surface soil samples was less than 7.7 pCi/g.

Subsurface soil sample concentrations ranged from 0.4 to 34.8 pCi/g for thorium-232 and from 0.3 to 4.0 pCi/g for radium-226. The average background level in this area for both radium-226 and thorium-232 is 1.0 pCi/g. The concentrations of uranium-238 in subsurface soil samples ranged from 0.5 to 31.8 pCi/g. Because the major contaminants at the vicinity properties are thorium and radium, the decontamination guidelines provide the appropriate guidance for the cleanup activities. DOE believes that these guidelines are conservative for considering potential adverse health effects that might occur in the future from any residual contamination. The dose contributions from uranium and any other radionuclides not numerically specified in these guidelines are not expected to be significant following decontamination. In addition, the vicinity properties will be decontaminated in a manner so as to reduce future doses to levels that are as low as reasonably achievable (ALARA) (Ref. 2).

Soil analysis data for this property indicated surface contamination. Subsurface investigation by gamma logging indicated contamination to a depth of 1.83 m (6.0 ft).

Exterior gamma radiation exposure rates ranged from 4 to 9 μR/h, including background. The indoor measurement showed a rate of 13 μR/h, including background.

The radon-222 measurement inside the office area indicated a concentration of 1.1 pCi/L, which is within the DOE guideline of 3.0 pCi/L.

The measurement for radon daughters was 0.001 working level (WL), and the measurement for thoron daughters was 0.001 WL.

All data tables for this property appear at the end of this report.

1.4 CONCLUSIONS

Evaluation of data collected, analyses performed, and historical documentation reviewed indicates the presence of radiological contamination on the property located at 80 Hancock Street. This contamination is primarily subsurface contamination ranging from a depth of 0.30 m (1.0 ft) to 1.83 m (6.0 ft) with an isolated area of surface contamination in front of the building. In addition, the subsurface contamination appears to extend beneath the building, and there is a high probability that the contamination extends beneath the streets (Hancock Street and Industrial Road) adjacent to the property. The total affected area is estimated to be approximately 70 percent of the property. These conclusions are supported by documentation that establishes the presence of the former channel of Lodi Brook in this area. This channel is the suspected transport mechanism for the radiological contamination.

From review of aerial photographs of the area, it has been determined that the former channel of Lodi Brook was realigned and buried in concrete conduit parallel to Hancock Street on this property. Prior to this realignment, it is suspected that the former channel flowed across the property in a southwesterly direction in the area where the building now stands. Confirmation of this suspicion could not be obtained because of severe access limitations to the interior of the building other than the office area. Indoor boreholes could not be drilled to confirm the presence of contamination beneath the building because of the significant safety hazards associated with drilling in areas where gas cylinders are filled, stored, and handled.

2.0 SITE HISTORY

The Maywood Chemical Works was founded in 1895. The company began processing thorium from monazite sand in 1916 (during World War I) for use in manufacturing gas mantles for various lighting devices. Process wastes from manufacturing operations were pumped to two areas surrounded by earthen dikes on property west of the plant. Subsequently, some of the contaminated wastes migrated onto adjacent and vicinity properties.

In 1928 and again between 1944 and 1946, some of the residues from the processing operations were moved from the company's property and used as mulch and fill in nearby low-lying areas. The fill material consisted of tea and coca leaves mixed with other material resulting from operations at the plant. Some fill material apparently contained thorium process wastes (Ref. 3).

Uncertainty exists as to how the properties in Lodi were contaminated. According to an area resident, fill from an unknown source was brought to Lodi and spread over large portions of the previously low-lying and swampy area. For several reasons, however, a more plausible explanation is that the contamination migrated along a drainage ditch originating on the Maywood Chemical Works property. First, it can be seen from photographs and tax maps of the area that the course of a previously existing stream known as Lodi Brook, which originated at the former Maywood Chemical Works, generally coincides with the path of contamination in Lodi. The brook was subsequently replaced by a storm drain system as the area was developed. Second, samples taken from Lodi properties indicate elevated concentrations of a series of elements known as rare earths. Rare earth elements are typically found in monazite sands, which also contain thorium. This type of sand was feedstock at the Maywood Chemical Works, and elevated levels are known to exist in the by-product of the extraction process. Third, the ratio of thorium to other radionuclides found on these Lodi properties is comparable to the ratio found in contaminated material on other properties in Lodi (Ref. 4). And finally, long-time residents of Lodi recalled chemical odors in and around the brook in Lodi and steam rising off the water. These observations suggest that discharges of contaminants occurred upstream.

The Stepan Chemical Company (now called the Stepan Company) purchased Maywood Chemical Works in 1959. The Stepan Company itself has never been involved in the manufacture or processing of any radioactive materials (Ref. 5).

2.1 PREVIOUS RADIOLOGICAL SURVEYS

Numerous surveys of the Maywood site and its vicinity properties have been conducted. Among the past surveys, three that are pertinent to this vicinity property are detailed in this section.

January 1981--The Nuclear Regulatory Commission directed that a survey be conducted of the Stepan Company property and its vicinity properties in January 1981. Using the Stepan Company plant as the center, a 10.3-km^2 (4-mi^2) aerial survey was conducted by the EG&G Energy Measurements Group, which identified anomalous concentrations of thorium-232 to the north and south of the Stepan Company property. The Lodi vicinity properties were included in this survey (Ref. 6).

June 1984--In June 1984, Oak Ridge National Laboratory (ORNL) conducted a "drive-by" survey of Lodi using its "scanning van." Although not comprehensive, the survey indicated areas requiring further investigation (Ref. 7).

<u>September 1986</u>--At the request of DOE, ORNL conducted radiological surveys of the vicinity properties in Lodi in September 1986 to determine which properties contained radioactive contamination in excess of DOE guidelines and would, therefore, require remedial action (Ref. 8).

2.2 REMEDIAL ACTION GUIDELINES

Table 2-1 summarizes the DOE guidelines for residual contamination. The thorium-232 and radium-226 limits listed in Table 2-1 will be used to determine the extent of remedial action required at the vicinity properties. DOE developed these guidelines to be consistent with the guidelines established by the U.S. Environmental Protection Agency (EPA) for the Uranium Mill Tailings Remedial Action Program.

TABLE 2-1
SUMMARY OF RESIDUAL CONTAMINATION GUIDELINES

BASIC DOSE LIMITS

The basic limit for the annual radiation dose received by an individual member of the general public is 100 mrem/yr.

SOIL GUIDELINES

Radionuclide	Soil Concentration (pCi/g) Above Background[a,b,c]
Radium-226 Radium-228 Thorium-230 Thorium-232	5 pCi/g when averaged over the first 15 cm of soil below the surface; 15 pCi/g when averaged over any 15-cm-thick soil layer below the surface layer.
Other Radionuclides	Soil guidelines will be calculated on a site-specific basis using the DOE manual developed for this use.

STRUCTURE GUIDELINES

Airborne Radon Decay Products

Generic guidelines for concentrations of airborne radon decay products shall apply to existing occupied or habitable structures on private property that has no radiological restrictions on its use; structures that will be demolished or buried are excluded. The applicable generic guideline (40 CFR 192) is: In any occupied or habitable building, the objective of remedial action shall be, and reasonable effort shall be made to achieve, an annual average (or equivalent) radon decay product concentration (including background) not to exceed 0.02 WL[d]. In any case, the radon decay product concentration (including background) shall not exceed 0.03 WL. Remedial actions are not required in order to comply with this guideline when there is reasonable assurance that residual radioactive materials are not the cause.

External Gamma Radiation

The average level of gamma radiation inside a building or habitable structure on a site that has no radiological restrictions on its use shall not exceed the background level by more than 20 μR/h.

Indoor/Outdoor Structure Surface Contamination

	Allowable Surface Residual Contamination[e] (dpm/100 cm²)		
Radionuclide[f]	Average[g,h]	Maximum[h,i]	Removable[h,j]
Transuranics, Ra-226, Ra-228, Th-230, Th-228 Pa-231, Ac-227, I-125, I-129	100	300	20
Th-Natural, Th-232, Sr-90, Ra-223, Ra-224 U-232, I-126, I-131, I-133	1,000	3,000	200
U-Natural, U-235, U-238, and associated decay products	5,000 α	15,000 α	1,000 α
Beta-gamma emitters (radionuclides with decay modes other than alpha emission or spontaneous fission) except Sr-90 and others noted above	5,000 β - γ	15,000 β - γ	1,000 β - γ

TABLE 2-1
(CONTINUED)

[a]These guidelines take into account ingrowth of radium-226 from thorium-230 and of radium-228 from thorium-232, and assume secular equilibrium. If either thorium-230 and radium-226 or thorium-232 and radium-228 are both present, not in secular equilibrium, the guidelines apply to the higher concentration. If other mixtures of radionuclides occur, the concentrations of individual radionuclides shall be reduced so that 1) the dose for the mixtures will not exceed the basic dose limit, or 2) the sum of ratios of the soil concentration of each radionuclide to the allowable limit for that radionuclide will not exceed 1 ("unity").

[b]These guidelines represent allowable residual concentrations above background averaged across any 15-cm-thick layer to any depth and over any contiguous 100-m^2 surface area.

[c]Localized concentrations in excess of these limits are allowable, provided that the average concentration over a 100-m^2 area does not exceed these limits. In addition, every reasonable effort shall be made to remove any source of radionuclide that exceeds 30 times the appropriate soil limit, regardless of the average concentration in the soil.

[d]A working level (WL) is any combination of short-lived radon decay products in 1 liter of air that will result in the ultimate emission of 1.3 x 105 MeV of potential alpha energy.

[e]As used in this table, dpm (disintegrations per minute) means the rate of emission by radioactive material as determined by correcting the counts per minute observed by an appropriate detector for background, efficiency, and geometric factors associated with the instrumentation.

[f]Where surface contamination by both alpha- and beta-gamma-emitting radionuclides exists, the limits established for alpha- and beta-gamma-emitting radionuclides should apply independently.

[g]Measurements of average contamination should not be averaged over more than 1 m^2. For objects of less surface area, the average shall be derived for each such object.

[h]The average and maximum radiation levels associated with surface contamination resulting from beta-gamma emitters should not exceed 0.2 mrad/h and 1.0 mrad/h, respectively, at 1 cm.

[i]The maximum contamination level applies to an area of not more than 100 cm^2.

[j]The amount of removable radioactive material per 100 cm^2 of surface area should be determined by wiping that area with dry filter or soft absorbent paper, applying moderate pressure, and measuring the amount of radioactive material on the wipe with an appropriate instrument of known efficiency. When removable contamination on objects of surface area less than 100 cm^2 is determined, the activity per unit area should be based on the actual area and the entire surface should be wiped. The numbers in this column are maximum amounts.

3.0 HEALTH AND SAFETY PLAN

BNI is responsible for protecting the health of personnel assigned to work at the site. As such, all subcontractors and their personnel were required to comply with the provisions of BNI health and safety requirements and as directed by the on-site BNI Health and Safety Officer.

3.1 SUBCONTRACTOR TRAINING

Before the start of work, all subcontractor personnel attended an orientation session presented by the BNI Health and Safety Officer to explain the nature of the material to be encountered in the work and the personnel monitoring and safety measures that are required.

3.2 SAFETY REQUIREMENTS

Subcontractor personnel complied with the following BNI requirements:

- Bioassay--Subcontractor personnel submitted bioassay samples before or at the beginning of on-site activity, upon completion of the activity, and periodically during site activities as requested by BNI.
- Protective Clothing/Equipment--Subcontractor personnel were required to wear the protective clothing/equipment specified in the subcontract or as directed by the BNI Health and Safety Officer.
- Dosimetry--Subcontractor personnel were required to wear and return daily the dosimeters and monitors issued by BNI.
- Controlled Area Access/Egress--Subcontractor personnel and equipment entering areas where access and egress were controlled for radiation and/or chemical safety purposes were surveyed by the BNI Health and Safety Officer (or personnel representing BNI) for contamination before leaving those areas.

- o Medical Surveillance--Upon written direction from BNI, subcontractor personnel who work in areas where hazardous chemicals might exist were given a baseline and periodic health assessment defined in BNI's Medical Surveillance Program.

Radiation and/or chemical safety surveillance of all activities related to the scope of work was under the direct supervision of personnel representing BNI.

Health and safety-related requirements for all activities involving exposure to radiation, radioactive material, chemicals, and/or chemically contaminated materials and other associated industrial safety hazards are generated in compliance with applicable regulatory requirements and industry-wide standards. Copies of these requirements are located at the BNI project office for use by project personnel.

4.0 CHARACTERIZATION PROCEDURES

A master grid was established by the surveyor. BNI's radiological support subcontractor, Thermo Analytical/Eberline (TMA/E), established a grid on individual properties. The size of the grid blocks was adjusted to characterize each property adequately. The grid origin allows the grid to be reestablished during remedial action and is correlated with the New Jersey state grid system. All data correspond to coordinates on the characterization grid. The grid with the east and north coordinates is shown on all figures included in Sections 4.0 and 5.0 of this report.

4.1 FIELD RADIOLOGICAL CHARACTERIZATION

This section provides a description of the instrumentation and methodologies used to obtain exterior surface and subsurface measurements during radiological characterization of this property.

4.1.1 Measurements Taken and Methods Used

An initial walkover survey was performed using an unshielded gamma scintillation detector [5.0- by 5.0-cm (2- by 2-in.) thallium-activated sodium iodide probe] to identify areas of elevated radionuclide activity. Near-surface gamma measurements taken using a cone-shielded gamma scintillation detector were also used to determine areas of surface contamination. The shielded detector ensured that the majority of the radiation detected by the instrument originated from the ground directly beneath the unit. Shielding against lateral gamma flux, or shine, from nearby areas of contamination minimized potential sources of error in the measurements. The measurements were taken 30.4 cm (12 in.) above the ground at the intersections of

3.0-m (10-ft) grid lines. The shielded detector was calibrated at the Technical Measurements Center (TMC) in Grand Junction, Colorado, to provide a correlation of counts per minute (cpm) to picocuries per gram (pCi/g). This calibration demonstrated that approximately 11,000 cpm corresponds to the DOE guideline of 5 pCi/g plus local average background of 1 pCi/g for thorium-232 in surface soils (Ref. 9).

A subsurface investigation was conducted to determine the depth to which the previously identified surface contamination extended and to locate subsurface contamination where there was no surface manifestation. The subsurface characterization consisted of drilling 16 boreholes (Figure 4-1), using either a 7.6-cm- (3-in.-) or 15.2-cm- (6-in.-) diameter auger bit, and gamma logging the boreholes. The boreholes were drilled to depths determined in the field by the radiological and geological support representatives.

The downhole gamma logging technique was used because the procedure can be accomplished in less time than collecting soil samples, and the need for analyzing these samples in a laboratory is eliminated. A 5.0- by 5.0-cm (2- by 2-in.) sodium iodide gamma scintillation detector was used to perform the downhole logging. The instrument was calibrated at TMC where it was determined that a count rate of approximately 40,000 cpm corresponds to the 15-pCi/g subsurface contamination guideline for thorium-232. This relationship has also been corroborated by results from previous characterizations where thorium-232 was found (Ref. 9).

Gamma radiation measurements were taken at 15.2-cm (6-in.) vertical intervals to determine the depth and concentration

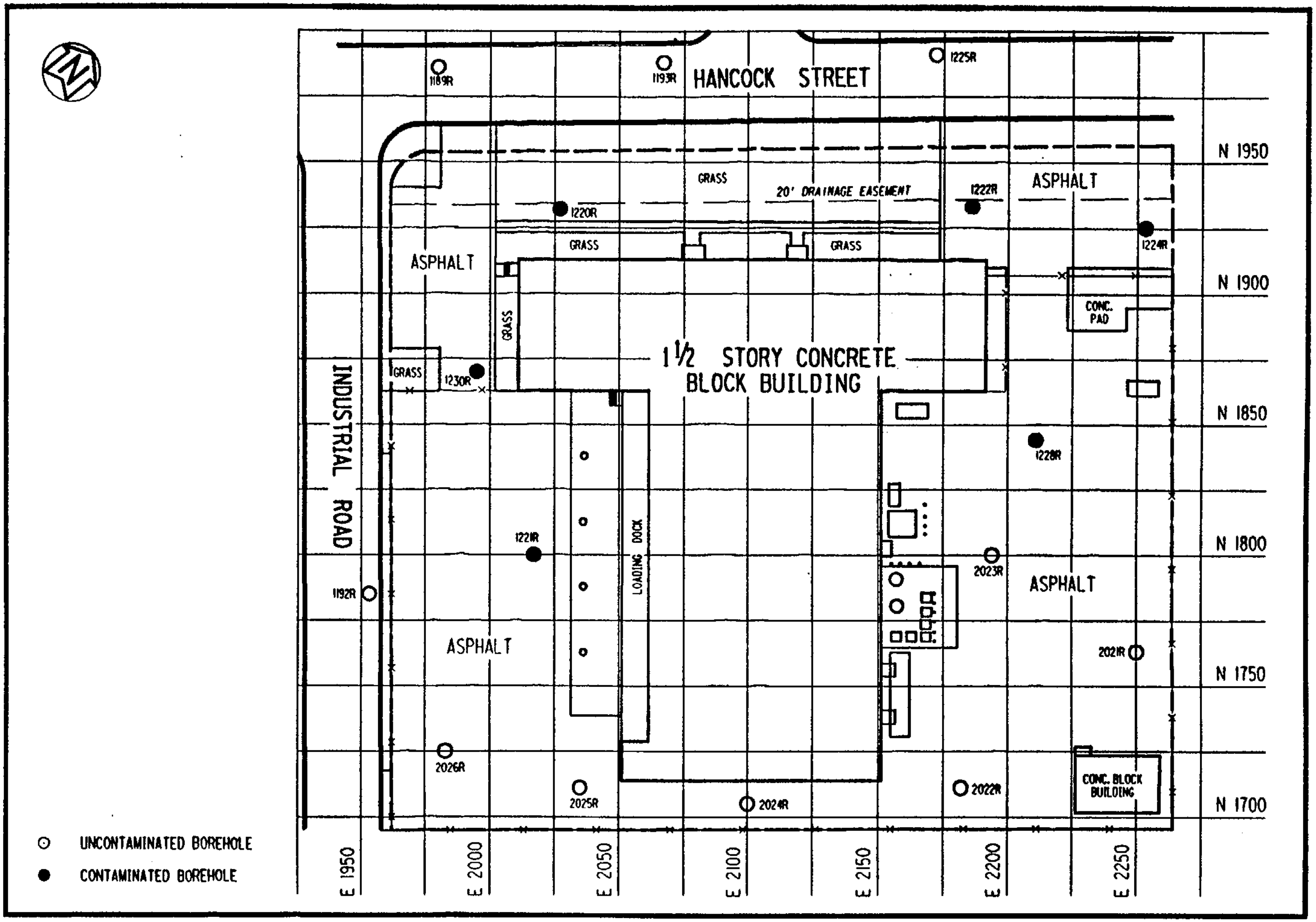

FIGURE 4-1 BOREHOLE LOCATIONS AT 80 HANCOCK STREET

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of the contamination. The gamma-logging data were reviewed to identify trends, whether or not concentrations exceeded the guidelines.

4.1.2 Sample Collection and Analysis

To identify surface areas where the level of contamination exceeded the DOE guideline of 5 pCi/g for thorium-232, areas with measurements of more than 11,000 cpm were plotted. Using these data as well as data from previous surveys (Refs. 5, 6, 7, and 8), the locations of biased surface soil samples were selected to better define the limits of contamination. Surface soil samples were taken at ten locations (Figure 4-2) and analyzed for thorium-232, uranium-238, and radium-226. Each sample was dried, pulverized, and counted for 10 min using an intrinsic germanium detector housed in a lead counting cave lined with cadmium and copper. The pulse height distribution was sorted using a computer-based, multichannel analyzer. Radionuclide concentrations were determined by comparing the gamma spectrum of each sample with the spectrum of a certified counting standard for the radionuclide of interest.

Subsurface soil samples were collected from 15 locations (Figure 4-2) using a 7.6-cm (3.0-in.) outside diameter (O.D.) split-spoon sampler mounted on a tripod or attached to a truck-mounted auger stem. The subsurface soil samples were analyzed for radium-226, uranium-238, and thorium-232 in the same manner as the surface soil samples.

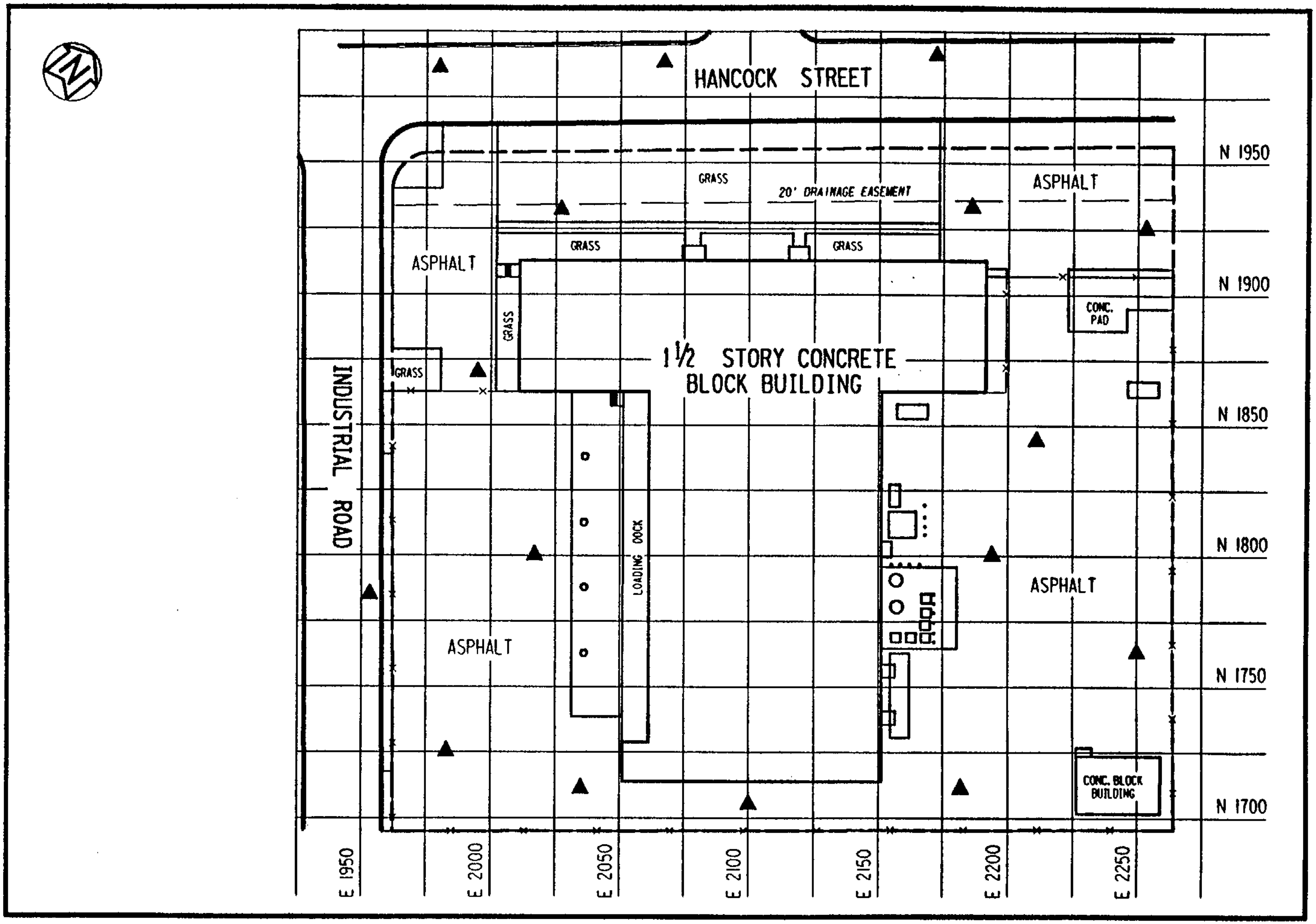

FIGURE 4-2 SURFACE AND SUBSURFACE SOIL SAMPLING LOCATIONS AT 80 HANCOCK STREET

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4.2 BUILDING RADIOLOGICAL CHARACTERIZATION

After evaluating previous radiological survey data as well as data from this characterization, it was suspected that contamination might be present under the foundation of the building. A radon measurement was obtained to verify the presence of contaminated material under the building and to estimate potential occupational exposures during future remedial actions.

An indoor radon measurement was made using the Tedlar bag method. Samples were collected by pumping air into a Tedlar bag at a rate of approximately 2 L/min. The air sample was transferred directly into a scintillation cell with an interior coating of zinc sulfide and an end window for viewing the scintillations. Analysis of the sample was simplified by allowing the radon decay products to build up over time. This method allowed all the radon decay products to come into secular equilibrium with the radon. The scintillation cell was placed in contact with a photomultiplier tube, and the scintillations were counted using standard nuclear counting instrumentation.

Indoor air samples were also collected to determine a WL for radon and thoron daughters. To measure radon daughters, an air sample was collected for exactly 5 min through a 0.45-micron membrane filter at a rate of 11 L/min for a total sample volume of 55 L. Alpha particle activity on the filter paper was counted 40 to 90 min after sampling. An alpha scintillation detector coupled to a count-rate meter or a digital scaler was used. Measurements for thoron daughters were made using the same method as for radon daughters with the exception of the time between collection of the air sample and counting of the alpha particle activity. In the case of thoron daughters, the sample was allowed to age for at least 5 h after sampling before alpha activity was counted. This elapsed time allowed radon daughters, which may have been present with the thoron daughters, to decay sufficiently so as not to interfere in calculating the WL for thoron daughters.

Exterior gamma exposure rate measurements were made at seven locations throughout the property grid system and at one location inside the office area of the building. To obtain these measurements, either a 5.0- by 5.0-cm (2- by 2-in.) thallium-activated sodium iodide gamma scintillation detector designed to detect gamma radiation only or a pressurized ionization chamber (PIC) was used. Measurement locations are shown in Figure 4-3. The PIC instrument has a response to gamma radiation that is proportional to exposure in roentgens. A conversion factor for gamma scintillation to the PIC was established through a correlation of these two measurements at four locations in the vicinity of the property. The unshielded gamma scintillation detector readings were then used to estimate gamma exposure rates for each location. These measurements were taken 1 m (3 ft) above the ground. The locations were determined to be representative of the entire property. Interior measurements are generally obtained with the gamma scintillation instrument rather than the PIC because of its smaller size and the desire to minimize the technician's time inside the building.

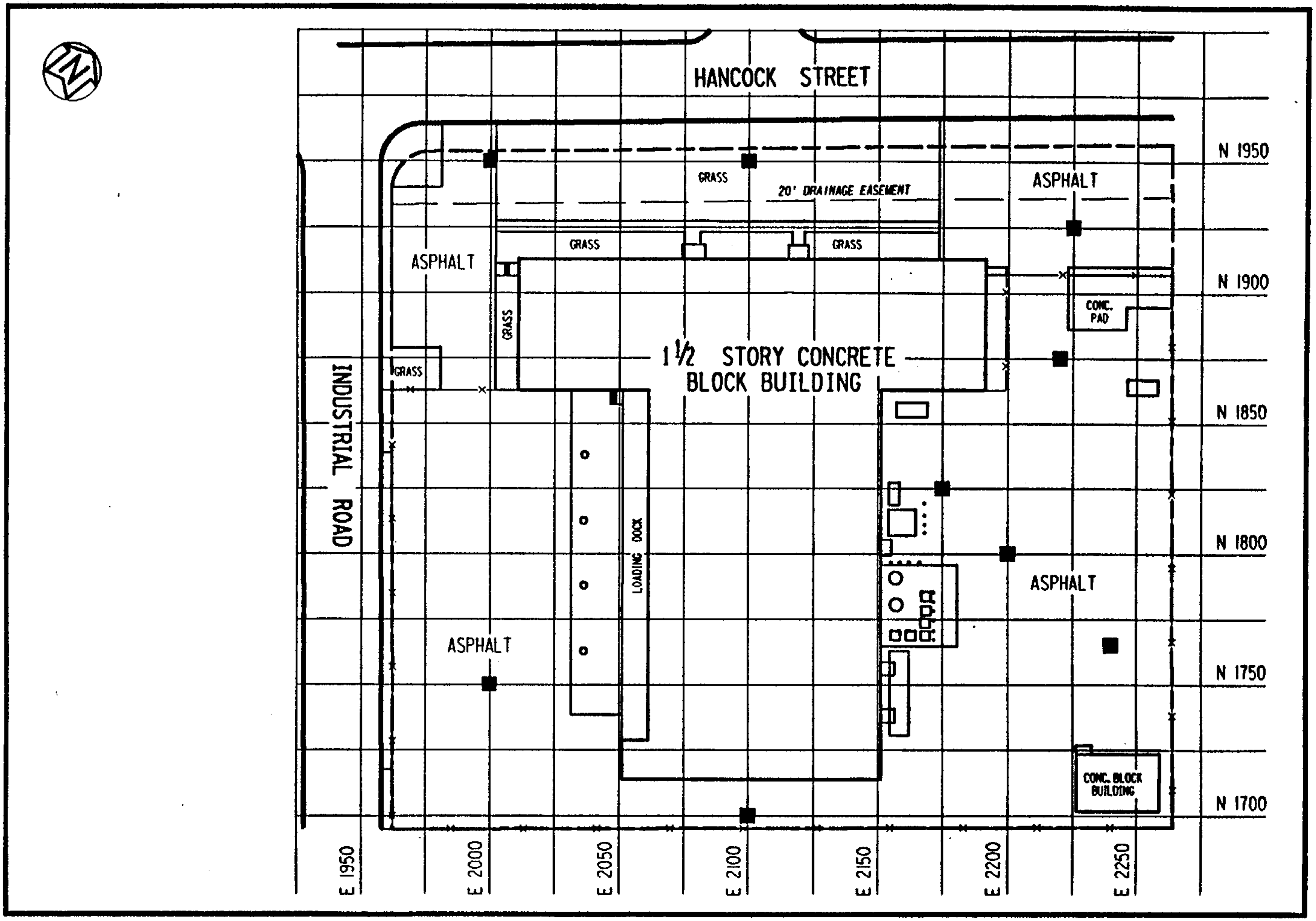

FIGURE 4-3 GAMMA EXPOSURE RATE MEASUREMENT LOCATIONS AT 80 HANCOCK STREET

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5.0 CHARACTERIZATION RESULTS

Radiological characterization results are presented in this section. The data included represent exterior surface and subsurface radiation measurements and interior radiation measurements.

5.1 FIELD RADIOLOGICAL CHARACTERIZATION

Near-surface gamma radiation measurements on the property ranged from 5,000 cpm to approximately 13,000 cpm. The average background level for this area is 5,000 cpm. A measurement of 11,000 cpm is approximately equal to the DOE guideline for thorium-232 of 5 pCi/g above background for surface soil contamination. Using this correlation, the near-surface gamma measurements were used to determine the extent of surface contamination and the basis for selecting the locations of soil samples. Areas of surface contamination are shown in Figure 5-1.

Surface soil samples [depths from 0.0 to 15.2 cm (6.0 in.)] were taken at six locations on the property and four locations in the streets (Hancock Street and Industrial Road) adjacent to the property (Figure 4-2). These samples were analyzed for thorium-232, uranium-238, and radium-226. The concentrations in these samples ranged from 1.9 to less than 7.7 pCi/g for uranium-238, from less than 1.0 to 8.6 pCi/g for thorium-232, and from less than 0.6 to less than 1.4 pCi/g for radium-226. Analytical results for surface soils are provided in Table 5-1; these data showed that concentrations of thorium-232 in one soil sample exceeded DOE guidelines (5 pCi/g plus background of 1 pCi/g for surface soils) with a maximum concentration of 8.6 pCi/g. Use of the "less than" (<) notation in reporting results indicates that the radionuclide was not present in

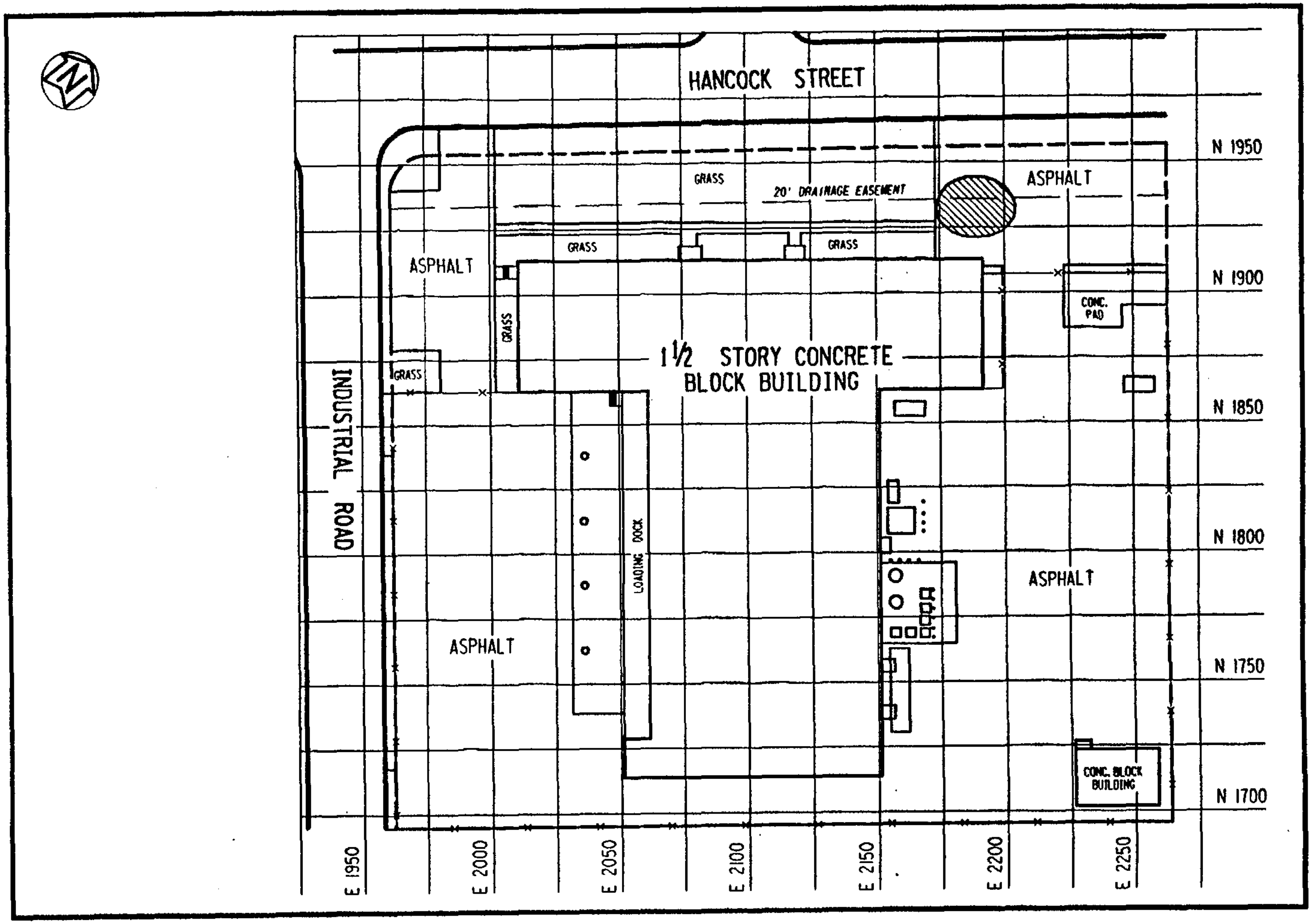

FIGURE 5-1 AREAS OF SURFACE CONTAMINATION AT 80 HANCOCK STREET

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concentrations that are quantitative with the instruments and techniques used. The "less than" value represents the lower bound of the quantitative capacity of the instrument and technique used. The "less than" value is based on various factors, including the volume, size, and weight of the sample; the type of detector used; the counting time; and the background count rate. The actual concentration of the radionuclide is less than the value indicated. In addition, since radioactive decay is a random process, a correlation between the rate of disintegration and a given radionuclide concentration cannot be precisely established. For this reason, the exact concentration of the radionuclide cannot be determined. As such, each value that can be quantitatively determined has an associated uncertainty term (±), which represents the amount by which the actual concentration can be expected to differ from the value given in the table. The uncertainty term has an associated confidence level of 95 percent.

Thorium-232, the primary contaminant at the site, is the radionuclide most likely to exceed a specific DOE guideline in soil. Parameters for soil sample analysis were selected to ensure that the thorium-232 would be detected and measured at concentrations well below the lower guideline value of 5 pCi/g in excess of background level. Radionuclides of the uranium series, specifically uranium-238 and radium-226, are also potential contaminants but at lower concentrations than thorium-232. Therefore, these radionuclides (considered secondary contaminants) would not be present in concentrations in excess of guidelines unless thorium-232 was also present in concentrations in excess of its guideline level. Parameters selected for the thorium-232 analyses also provide detection sensitivities for uranium-238 and radium-226 that demonstrate that concentrations of these radionuclides are below guidelines. However, because of the relatively low gamma photon abundance of uranium-238, many of the uranium-238 concentrations were below the detection sensitivity of the analytical procedure; these concentrations are reported in the data tables as "less than" values. To obtain more sensitive readings for the uranium-238 radionuclide with these analytical methods, much longer instrument counting times would be required than were necessary for analysis of thorium-232, the primary contaminant.

Analytical results for subsurface soil samples are given in Table 5-1, and gamma logging data are given in Table 5-2. The results in Table 5-2 showed a range from 5,000 cpm to 184,000 cpm. A measurement of 40,000 cpm is approximately equal to the DOE guideline for subsurface contamination of 15 pCi/g. Analyses of subsurface soil samples indicated uranium-238 concentrations ranging from 0.5 to 31.8 pCi/g, thorium-232 concentrations ranging from 0.4 to 34.8 pCi/g, and radium-226 concentrations ranging from 0.3 to 4.0 pCi/g.

On the basis of near-surface gamma radiation measurements, surface and subsurface soil sample analyses, and downhole gamma logging, contamination on this property is believed to consist primarily of subsurface contamination at depths ranging from 0.30 m (1.0 ft) to 1.83 m (6.0 ft). The areas of subsurface contamination are shown in Figure 5-2. The subsurface contamination appears to extend beneath the building and the streets (Hancock Street and Industrial Road) adjacent to the property.

It is apparent from review of historical documentation (e.g., aerial photographs of the area, interviews with local residents, and previous radiological surveys) that the subsurface contamination on this property lies along the former channel of Lodi Brook and its associated floodplain.

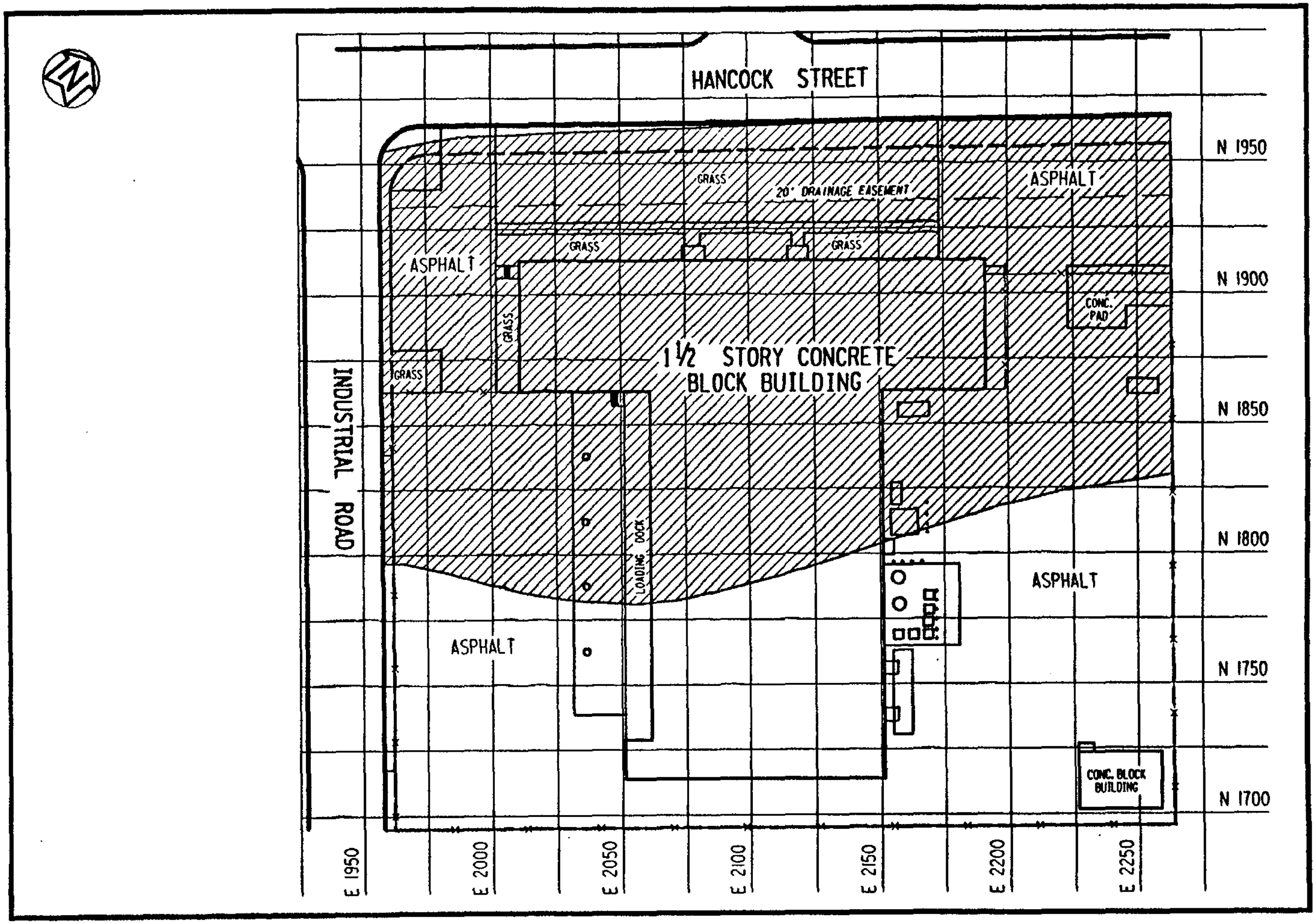

FIGURE 5-2 AREAS OF SUBSURFACE CONTAMINATION AT 80 HANCOCK STREET

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The contamination is similar to contamination found on two commercial properties in close proximity to this property. It has been established that the Lodi Brook channel through these neighboring properties once occupied locations connecting to those where stream sediments were found at 80 Hancock Street. Thus, the elevated gamma readings shown on gamma logs from boreholes drilled on this property serve as further indication of the suspected mechanism of transport for radiological contamination (i.e., stream deposition from Lodi Brook).

The vertical and horizontal limits of contamination as determined by this characterization effort are being evaluated to determine the volume of contaminated material that will require remedial action. To develop this estimate, BNI will consider the location of the contamination, construction techniques, and safety procedures.

5.2 BUILDING RADIOLOGICAL CHARACTERIZATION

Results of an indoor radon measurement using the Tedlar bag method indicated a concentration of 1.1 pCi/L. This measurement was substantially less than the applicable DOE guideline of 3.0 pCi/L above background (Ref. 10).

Results of a measurement for radon daughters was 0.001 WL. This result was substantially less than the applicable generic guideline detailed in the Code of Federal Regulations, 40 CFR 192 (Ref. 10), which states that an annual average (or equivalent) radon decay product concentration not exceed 0.02 WL.

Results of a measurement for thoron daughters was 0.001 WL. The generic guideline is more restrictive for radon-222 (radon) than for radon-220 (thoron) according to the National

Council on Radiological Protection [see NCRP Report No. 50 (Ref. 11), which was used as the guideline for thoron daughter measurements].

Exterior gamma radiation exposure rate measurements ranged from 4 to 9 μR/h, including background. These results can be found in Table 5-3. The average exterior exposure rate of 6 μR/h does not exceed the average background level of 9 μR/h (Ref. 12). Therefore, no dose in excess of average background would be received as a result of contamination present on the property by employees spending time outside the building.

Indoor exposure rate measurement was 13 μR/h, including background (Table 5-3). For comparison, the DOE guideline for indoor exposure rate is 20 μR/h. Assuming an employee spends 40 hours per week for 50 weeks per year (2,000 hours or 8 hours per day for 5 days per week) inside the building, and assuming the average indoor exposure rate is 13 μR/h, a yearly dose of 8 mrem could be expected (after subtracting average background of 9 μR/h; Ref.12).

Based on the above information, the exposure rates and doses at this property are within DOE guidelines. Further, it should be emphasized that natural background exposure rates vary widely across the United States and are significantly higher than average background for this area.

TABLE 5-1

SURFACE AND SUBSURFACE RADIONUCLIDE CONCENTRATIONS IN SOIL

FOR 80 HANCOCK STREET

Coordinates[a] East	North	Depth (ft)	Concentration (pCi/g ± 2 sigma) Uranium-238	Radium-226	Thorium-232
1953	1785	0.0 - 0.5	< 3.4	< 0.6	< 1.3
1953	1785	0.0 - 2.0	< 3.0	< 0.6	< 1.0
1953	1785	0.5 - 2.0	< 3.7	< 0.9	< 1.4
1953	1785	2.0 - 4.0	< 3.4	< 0.6	< 1.3
1953	1785	6.0 - 7.0	< 3.7	< 0.8	< 1.2
1953	1785	8.0 - 10.0	< 2.0	< 0.5	< 0.7
1953	1785	8.0 - 10.0	< 2.6	< 0.5	< 0.9
1953	1785	10.0 - 11.0	< 3.4	< 0.7	< 1.1
1953	1785	11.0 - 12.0	< 3.6	< 0.8	< 1.5
1980	1986	0.0 - 0.5	< 3.2	< 0.8	< 1.1
1980	1986	0.0 - 2.0	< 2.8	< 0.6	< 0.9
1980	1986	2.0 - 4.0	< 2.7	< 0.6	< 0.9
1980	1986	6.0 - 8.0	< 2.6	< 0.5	< 0.8
1980	1986	8.0 - 9.0	< 4.4	< 1.0	< 1.7
1980	1986	9.0 - 10.0	< 4.9	< 0.9	< 1.5
1980	1986	10.0 - 11.0	< 4.9	< 1.0	< 1.6
1980	1986	11.0 - 12.0	< 5.7	< 1.4	< 2.2
1995	1870	0.5 - 2.0	< 4.3	< 1.1	< 1.6
1995	1870	4.0 - 6.0	< 6.6	< 1.4	< 2.0
1995	1870	9.0 - 10.0	< 5.4	< 1.2	< 1.5
2017	1800	0.0 - 0.5	< 5.1	< 0.9	< 1.6
2017	1800	2.5 - 4.0	< 4.7	< 0.8	2.2 ± 0.2
2017	1800	6.0 - 7.5	< 3.8	< 0.9	< 1.4

TABLE 5-1

(continued)

Coordinates[a] East	North	Depth (ft)	Concentration (pCi/g ± 2 sigma) Uranium-238	Radium-226	Thorium-232
2027	1932	0.0 - 0.5	< 5.8	< 1.0	< 2.3
2027	1932	3.0 - 4.0	< 5.8	< 1.3	< 1.7
2027	1932	4.0 - 6.0	< 7.7	< 1.0	< 3.0
2027	1932	8.0 - 9.0	< 4.7	< 1.0	< 1.6
2027	1932	9.0 - 10.0	< 6.7	< 1.4	< 1.8
2035	1711	1.0 - 1.5	< 2.0	< 1.0	1.0 ± 0.1
2035	1711	1.5 - 2.0	< 2.0	0.8 ± 0.1	0.8 ± 0.5
2035	1711	2.0 - 2.5	< 2.0	< 1.0	< 1.0
2035	1711	2.5 - 3.0	< 2.0	0.4 ± 0.1	0.9 ± 0.5
2035	1711	3.0 - 3.5	< 2.0	0.5 ± 0.2	< 1.0
2035	1711	3.5 - 4.0	< 2.0	< 1.0	< 1.0
2035	1711	4.0 - 4.5	< 1.0	0.5 ± 0.2	1.0 ± 0.1
2035	1711	4.5 - 5.0	< 2.0	0.5 ± 0.2	0.8 ± 0.2
2035	1711	5.0 - 5.5	< 1.0	< 1.0	0.6 ± 0.3
2035	1711	5.5 - 6.0	< 2.0	0.5 ± 0.1	< 1.0
2035	1711	6.0 - 6.5	0.5 ± 0.3	0.3 ± 0.1	0.4 ± 0.1
2035	1711	6.5 - 7.0	< 2.0	0.4 ± 0.2	0.7 ± 0.3
2035	1711	7.0 - 7.5	< 2.0	0.5 ± 0.1	< 1.0
2035	1711	7.5 - 8.0	< 2.0	< 1.0	< 1.0
2035	1711	8.0 - 8.5	< 1.0	0.4 ± 0.1	< 1.0
2035	1711	8.5 - 9.0	< 2.0	0.4 ± 0.2	0.7 ± 0.3
2035	1711	9.0 - 9.5	< 2.0	0.6 ± 0.1	1.1 ± 0.4
2035	1711	9.5 - 10.0	1.5 ± 1.5	0.6 ± 0.1	0.8 ± 0.1

TABLE 5-1

(continued)

Coordinates[a] East	North	Depth (ft)	Concentration (pCi/g ± 2 sigma) Uranium-238	Radium-226	Thorium-232
2067	1988	0.5 - 2.0	< 3.7	< 0.9	< 1.4
2067	1988	2.0 - 4.0	< 3.4	< 0.6	< 1.3
2067	1988	6.0 - 7.0	< 3.7	< 0.8	< 1.2
2067	1988	8.0 - 10.0	< 2.6	< 0.5	< 0.9
2100	1705	0.5 - 1.0	< 2.0	0.6 ± 0.1	< 1.0
2100	1705	1.0 - 1.5	< 2.0	0.9 ± 0.3	< 1.0
2100	1705	1.5 - 2.0	< 2.0	0.6 ± 0.1	0.8 ± 0.4
2100	1705	3.0 - 3.5	< 2.0	< 1.0	< 1.0
2100	1705	3.5 - 4.0	< 2.0	0.5 ± 0.3	1.0 ± 0.2
2100	1705	4.0 - 4.5	< 1.0	< 1.0	< 1.0
2100	1705	4.5 - 5.0	< 2.0	0.5 ± 0.3	0.8 ± 0.2
2100	1705	5.0 - 5.5	< 2.0	0.6 ± 0.2	0.7 ± 0.4
2100	1705	5.5 - 6.0	< 1.0	< 1.0	< 1.0
2100	1705	6.0 - 6.5	< 2.0	0.5 ± 0.2	< 1.0
2100	1705	6.5 - 7.0	< 1.0	0.3 ± 0.1	< 1.0
2100	1705	7.0 - 7.5	< 2.0	< 1.0	< 1.0
2100	1705	7.5 - 8.0	< 1.0	0.5 ± 0.2	0.7 ± 0.4
2100	1705	8.0 - 8.5	< 2.0	< 1.0	< 1.0
2100	1705	8.5 - 9.0	< 2.0	0.7 ± 0.2	1.2 ± 0.8
2100	1705	9.0 - 9.5	< 2.0	< 1.0	< 1.0
2100	1705	9.5 - 10.0	< 2.0	0.5 ± 0.1	0.8 ± 0.5
2172	1991	0.0 - 0.5	< 4.8	< 1.1	< 1.6
2172	1991	4.0 - 5.0	< 5.2	< 1.0	< 1.7
2172	1991	6.0 - 7.0	< 4.9	< 1.0	< 1.2
2172	1991	7.0 - 8.0	< 4.5	< 1.0	< 1.5

TABLE 5-1

(continued)

Coordinates[a] East	Coordinates[a] North	Depth (ft)	Concentration (pCi/g ± 2 sigma) Uranium-238	Radium-226	Thorium-232
2177	1811	0.0 - 0.5	1.9 ± 1.7	0.9 ± 0.3	1.6 ± 0.9
2177	1811	1.0 - 1.5	1.6 ± 1.5	< 1.0	< 1.0
2177	1811	1.5 - 2.0	< 3.0	0.8 ± 0.1	< 1.0
2177	1811	2.0 - 2.5	< 2.0	< 1.0	< 1.0
2177	1811	2.5 - 3.0	< 3.0	0.8 ± 0.1	1.6 ± 0.4
2182	1711	0.5 - 1.0	1.9 ± 1.6	0.9 ± 0.1	1.2 ± 0.2
2182	1711	1.0 - 1.5	2.1 ± 0.4	0.6 ± 0.1	1.0 ± 0.5
2182	1711	1.5 - 2.0	< 2.0	0.8 ± 0.3	1.3 ± 0.2
2182	1711	4.0 - 4.5	< 2.0	0.4 ± 0.2	0.5 ± 0.3
2182	1711	4.5 - 5.0	< 2.0	< 1.0	< 1.0
2182	1711	5.0 - 5.0	< 2.0	0.6 ± 0.3	< 1.0
2182	1711	5.5 - 6.0	< 2.0	0.4 ± 0.1	0.6 ± 0.2
2182	1711	6.0 - 6.5	< 2.0	0.7 ± 0.2	0.8 ± 0.2
2182	1711	6.5 - 7.0	< 2.0	< 1.0	< 1.0
2182	1711	7.0 - 7.5	< 2.0	0.4 ± 0.1	< 1.0
2182	1711	7.5 - 8.0	2.4 ± 1.7	0.7 ± 0.6	< 1.0
2182	1711	8.0 - 8.5	< 2.0	< 1.0	< 1.0
2182	1711	8.5 - 9.0	< 2.0	< 1.0	< 1.0
2182	1711	9.0 - 9.5	< 2.0	0.6 ± 0.2	1.1 ± 0.7
2182	1711	9.5 - 10.0	< 2.0	< 1.0	< 1.0
2186	1933	0.0 - 0.5	< 6.9	< 1.0	8.6 ± 0.8
2186	1933	0.0 - 1.0	< 4.7	< 0.9	< 1.9
2186	1933	3.0 - 4.0	< 4.0	< 0.9	< 1.7
2186	1933	4.0 - 5.0	< 3.7	< 0.7	< 1.5
2186	1933	5.0 - 6.0	< 13.6	4.0 ± 0.3	34.8 ± 1.0
2186	1933	6.0 - 7.0	< 7.7	< 1.0	12.4 ± 0.8
2186	1933	7.0 - 8.0	< 4.5	< 1.0	< 1.4

TABLE 5-1

(continued)

Coordinates[a]		Depth	Concentration (pCi/g ± 2 sigma)		
East	North	(ft)	Uranium-238	Radium-226	Thorium-232
2211	1844	0.0 - 0.5	< 7.7	< 1.4	5.3 ± 0.7
2211	1844	0.5 - 2.0	< 4.3	< 0.8	< 1.6
2211	1844	2.0 - 4.0	< 5.0	< 1.1	< 1.8
2211	1844	4.0 - 6.0	< 3.4	< 0.7	< 1.5
2211	1844	6.0 - 7.0	< 5.8	< 1.4	< 2.0
2211	1844	7.0 - 8.0	< 5.7	< 1.1	< 2.1
2211	1844	8.0 - 9.0	< 3.3	< 0.6	< 1.1
2211	1844	9.0 - 10.0	< 3.3	< 0.7	< 1.2
2250	1763	0.0 - 0.5	< 2.0	< 1.0	< 1.0
2250	1763	0.5 - 1.0	< 3.0	< 1.0	< 1.0
2250	1763	1.0 - 1.5	< 3.0	1.0 ± 0.2	< 1.0
2250	1763	1.5 - 2.0	< 2.0	0.6 ± 0.2	< 1.0
2250	1763	2.0 - 2.5	< 2.0	< 1.0	1.4 ± 0.6
2250	1763	2.5 - 3.0	< 3.0	0.5 ± 0.1	1.1 ± 0.6
2250	1763	4.0 - 4.5	< 2.0	< 1.0	< 1.0
2250	1763	4.5 - 5.0	< 2.0	0.5 ± 0.1	< 1.0
2250	1763	5.0 - 5.5	< 2.0	< 1.0	< 1.0
2250	1763	5.5 - 6.0	< 2.0	< 1.0	< 1.0
2250	1763	6.0 - 6.5	< 2.0	< 1.0	< 1.0
2250	1763	6.5 - 7.0	< 2.0	< 1.0	< 1.0
2250	1763	7.0 - 7.5	< 2.0	0.5 ± 0.2	0.6 ± 0.3
2250	1763	7.5 - 8.0	< 2.0	0.6 ± 0.1	0.8 ± 0.8

TABLE 5-1

(continued)

Coordinates[a] East	Coordinates[a] North	Depth (ft)	Concentration (pCi/g ± 2 sigma) Uranium-238	Radium-226	Thorium-232
2253	1925	0.0 - 0.5	< 7.5	< 1.2	< 2.9
2253	1925	1.0 - 2.0	< 9.3	< 1.5	14.3 ± 2.6
2253	1925	4.0 - 5.0	< 6.9	< 1.3	8.4 ± 1.1
2253	1925	5.0 - 6.0	31.8 ± 5.3	< 2.0	14.3 ± 2.0
2253	1925	6.0 - 7.0	< 9.4	< 2.1	< 3.0
2253	1925	7.0 - 8.0	< 6.6	< 1.6	< 2.2
2253	1925	8.0 - 9.0	< 3.6	< 0.7	< 1.5
2253	1925	9.0 - 10.0	< 4.9	< 1.3	< 1.6

[a]Sampling locations are shown in Figure 4-2.

TABLE 5-2

DOWNHOLE GAMMA LOGGING RESULTS

FOR 80 HANCOCK STREET

Coordinates[a]		Depth[b]	Count Rate[c]
East	North	(ft)	(cpm)
Borehole 1192R[d]			
1953	1785	0.5	8000
1953	1785	1.0	12000
1953	1785	1.5	14000
1953	1785	2.0	14000
1953	1785	2.5	12000
1953	1785	3.0	12000
1953	1785	3.5	12000
1953	1785	4.0	11000
1953	1785	4.5	11000
1953	1785	5.0	9000
1953	1785	5.5	9000
1953	1785	6.0	7000
1953	1785	6.5	7000
1953	1785	7.0	7000
1953	1785	7.5	7000
1953	1785	8.0	7000
1953	1785	8.5	7000
1953	1785	9.0	6000
1953	1785	9.5	7000
Borehole 1189R			
1980	1986	0.5	6000
1980	1986	1.0	6000
1980	1986	1.5	6000
1980	1986	2.0	7000
1980	1986	2.5	9000
1980	1986	3.0	9000
1980	1986	3.5	9000
1980	1986	4.0	8000
1980	1986	4.5	8000
1980	1986	5.0	8000
1980	1986	5.5	8000
1980	1986	6.0	9000
1980	1986	6.5	9000
1980	1986	7.0	10000
1980	1986	7.5	10000
1980	1986	8.0	9000

TABLE 5-2

(continued)

Coordinates[a] East	North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 2026R[d]			
1983	1725	0.5	6000
1983	1725	1.0	8000
1983	1725	1.5	11000
1983	1725	2.0	11000
1983	1725	2.5	11000
1983	1725	3.0	10000
1983	1725	3.5	10000
1983	1725	4.0	10000
1983	1725	4.5	10000
1983	1725	5.0	10000
1983	1725	5.5	10000
1983	1725	6.0	10000
1983	1725	6.5	11000
1983	1725	7.0	11000
1983	1725	7.5	10000
1983	1725	8.0	9000
1983	1725	8.5	8000
1983	1725	9.0	8000
1983	1725	9.5	8000
Borehole 1230R[d]			
1995	1870	0.5	8000
1995	1870	1.0	12000
1995	1870	1.5	15000
1995	1870	2.0	14000
1995	1870	2.5	14000
1995	1870	3.0	14000
1995	1870	3.5	15000
1995	1870	4.0	18000
1995	1870	4.5	35000
1995	1870	5.0	59000
1995	1870	5.5	28000
1995	1870	6.0	13000
1995	1870	6.5	11000
1995	1870	7.0	11000
1995	1870	7.5	10000
1995	1870	8.0	11000

TABLE 5-2

(continued)

Coordinates[a] East	North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 1221R[d]			
2017	1800	0.5	7000
2017	1800	1.0	11000
2017	1800	1.5	12000
2017	1800	2.0	14000
2017	1800	2.5	15000
2017	1800	3.0	18000
2017	1800	3.5	25000
2017	1800	4.0	19000
2017	1800	4.5	15000
2017	1800	5.0	12000
2017	1800	5.5	11000
2017	1800	6.0	11000
2017	1800	6.5	10000
2017	1800	7.0	11000
Borehole 1220R[d]			
2027	1932	0.5	12000
2027	1932	1.0	17000
2027	1932	1.5	19000
2027	1932	2.0	16000
2027	1932	2.5	14000
2027	1932	3.0	22000
2027	1932	3.5	26000
2027	1932	4.0	30000
2027	1932	4.5	47000
2027	1932	5.0	48000
2027	1932	5.5	22000
2027	1932	6.0	13000
2027	1932	6.5	10000
2027	1932	7.0	10000
2027	1932	7.5	11000
2027	1932	8.0	11000
2027	1932	8.5	11000
Borehole 2025R[d]			
2035	1711	0.5	9000
2035	1711	1.0	10000
2035	1711	1.5	10000
2035	1711	2.0	9000

TABLE 5-2

(continued)

Coordinates[a] East	North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 2025R (continued)[d]			
2035	1711	2.5	9000
2035	1711	3.0	9000
2035	1711	3.5	9000
2035	1711	4.0	9000
2035	1711	4.5	8000
2035	1711	5.0	8000
2035	1711	5.5	8000
2035	1711	6.0	7000
2035	1711	6.5	8000
2035	1711	7.0	8000
2035	1711	7.5	8000
2035	1711	8.0	9000
2035	1711	8.5	9000
2035	1711	9.0	9000
2035	1711	9.5	9000
Borehole 1193R			
2067	1988	0.5	7000
2067	1988	1.0	11000
2067	1988	1.5	11000
2067	1988	2.0	10000
2067	1988	2.5	10000
2067	1988	3.0	10000
2067	1988	3.5	11000
2067	1988	4.0	11000
2067	1988	4.5	11000
2067	1988	5.0	10000
2067	1988	5.5	10000
2067	1988	6.0	10000
2067	1988	6.5	9000
2067	1988	7.0	9000
2067	1988	7.5	8000
2067	1988	8.0	8000
2067	1988	8.5	8000
2067	1988	9.0	8000
Borehole 2024R[d]			
2100	1705	0.5	7000
2100	1705	1.0	11000

TABLE 5-2

(continued)

Coordinates[a] East	North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 2024R (continued)[d]			
2100	1705	1.5	12000
2100	1705	2.0	12000
2100	1705	2.5	10000
2100	1705	3.0	9000
2100	1705	3.5	9000
2100	1705	4.0	10000
2100	1705	4.5	10000
2100	1705	5.0	8000
2100	1705	5.5	9000
2100	1705	6.0	8000
2100	1705	6.5	8000
2100	1705	7.0	8000
2100	1705	7.5	8000
2100	1705	8.0	8000
2100	1705	8.5	8000
2100	1705	9.0	8000
2100	1705	9.5	8000
Borehole 1225R			
2172	1991	0.5	6000
2172	1991	1.0	10000
2172	1991	1.5	11000
2172	1991	2.0	11000
2172	1991	2.5	10000
2172	1991	3.0	9000
2172	1991	3.5	9000
2172	1991	4.0	9000
2172	1991	4.5	8000
2172	1991	5.0	8000
2172	1991	5.5	7000
2172	1991	6.0	6000
2172	1991	6.5	5000
2172	1991	7.0	5000
Borehole 2022R[d]			
2182	1711	0.5	7000
2182	1711	1.0	9000
2182	1711	1.5	11000
2182	1711	2.0	11000

TABLE 5-2

(continued)

Coordinates[a] East	North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 2022R (continued)[d]			
2182	1711	2.5	11000
2182	1711	3.0	10000
2182	1711	3.5	9000
2182	1711	4.0	8000
2182	1711	4.5	9000
2182	1711	5.0	9000
2182	1711	5.5	9000
2182	1711	6.0	8000
2182	1711	6.5	8000
2182	1711	7.0	9000
2182	1711	7.5	9000
2182	1711	8.0	9000
2182	1711	8.5	8000
2182	1711	9.0	9000
2182	1711	9.5	9000
Borehole 1222R[d]			
2186	1933	0.5	16000
2186	1933	1.0	18000
2186	1933	1.5	18000
2186	1933	2.0	17000
2186	1933	2.5	15000
2186	1933	3.0	17000
2186	1933	3.5	28000
2186	1933	4.0	47000
2186	1933	4.5	94000
2186	1933	5.0	184000
2186	1933	5.5	159000
2186	1933	6.0	57000
2186	1933	6.5	24000
2186	1933	7.0	15000
2186	1933	7.5	13000
2186	1933	8.0	12000
Borehole 2023R[d]			
2194	1800	0.5	7000
2194	1800	1.0	10000
2194	1800	1.5	11000
2194	1800	2.0	11000

TABLE 5-2

(continued)

Coordinates[a] East	North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 2023R (continued)[d]			
2194	1800	2.5	11000
2194	1800	3.0	11000
2194	1800	3.5	10000
2194	1800	4.0	9000
2194	1800	4.5	9000
2194	1800	5.0	10000
2194	1800	5.5	9000
2194	1800	6.0	9000
2194	1800	6.5	8000
2194	1800	7.0	8000
2194	1800	7.5	9000
2194	1800	8.0	8000
2194	1800	8.5	8000
2194	1800	9.0	8000
2194	1800	9.5	8000
2194	1800	10.0	8000
2194	1800	10.5	8000
2194	1800	11.0	8000
2194	1800	11.5	8000
2194	1800	12.0	8000
2194	1800	12.5	7000
Borehole 1228R[d]			
2211	1844	0.5	23000
2211	1844	1.0	35000
2211	1844	1.5	35000
2211	1844	2.0	29000
2211	1844	2.5	28000
2211	1844	3.0	29000
2211	1844	3.5	32000
2211	1844	4.0	45000
2211	1844	4.5	68000
2211	1844	5.0	35000
2211	1844	5.5	20000
2211	1844	6.0	19000
2211	1844	6.5	18000
2211	1844	7.0	18000
2211	1844	7.5	17000
2211	1844	8.0	17000

TABLE 5-2

(continued)

Page 8 of 9

Coordinates[a] East	North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 2021R[d]			
2250	1763	0.5	11000
2250	1763	1.0	13000
2250	1763	1.5	14000
2250	1763	2.0	14000
2250	1763	2.5	14000
2250	1763	3.0	14000
2250	1763	3.5	14000
2250	1763	4.0	12000
2250	1763	4.5	11000
2250	1763	5.0	11000
2250	1763	5.5	11000
2250	1763	6.0	10000
2250	1763	6.5	9000
2250	1763	7.0	8000
2250	1763	7.5	7000
2250	1763	8.0	6000
2250	1763	8.5	6000
Borehole 1224R[d]			
2253	1925	0.5	17000
2253	1925	1.0	21000
2253	1925	1.5	30000
2253	1925	2.0	56000
2253	1925	2.5	95000
2253	1925	3.0	54000
2253	1925	3.5	27000
2253	1925	4.0	26000
2253	1925	4.5	40000
2253	1925	5.0	76000
2253	1925	5.5	42000

TABLE 5-2

(continued)

Coordinates[a] East	North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 1224R (continued)[d]			
2253	1925	6.0	17000
2253	1925	6.5	12000
2253	1925	7.0	12000
2253	1925	7.5	11000

[a]Borehole locations are shown in Figure 4-1.

[b]The variations in depths of boreholes and corresponding results given in this table are based on the boreholes penetrating the contamination or the drill reaching refusal.

[c]Instrument used was 5.0- by 5.0-cm (2- by 2-in.) thallium-activated sodium iodide gamma scintillation detector.

[d]Bottom of borehole collapsed.

TABLE 5-3

GAMMA RADIATION EXPOSURE RATES

FOR 80 HANCOCK STREET

Coordinates[a] East	North	Rate[b] (μR/h)
2000	1750	5
2000	1950	7
2100	1700	4
2100	1950	9
2175	1825	5
2220	1875	7
2225	1925	6
Interior of Building		13

[a]Measurement locations are shown in Figure 4-3.

[b]Measurements include background.

REFERENCES

1. U.S. Department of Energy. Description of the Formerly Utilized Sites Remedial Action Program, ORO-777, Oak Ridge, Tenn., September 1980 (as modified by DOE in October 1983).

2. Argonne National Laboratory. Action Description Memorandum, Interim Remedial Actions at Maywood, New Jersey, Argonne, Ill., March 1987.

3. Argonne National Laboratory. Action Description Memorandum, Proposed 1984 Remedial Actions at Maywood, New Jersey, Argonne, Ill., June 8, 1984.

4. Bechtel National, Inc. Post-Remedial Action Report for the Lodi Residential Properties, DOE/OR/20722-89, Oak Ridge, Tenn., August 1986.

5. NUS Corporation. Radiological Study of Maywood Chemical, Maywood, New Jersey, November 1983.

6. EG&G Energy Measurements Group. An Aerial Radiologic Survey of the Stepan Chemical Company and Surrounding Area, Maywood, New Jersey, NRC-8109, Oak Ridge, Tenn., September 1981.

7. Oak Ridge National Laboratory. Results of the Mobile Gamma Scanning Activities in Lodi, New Jersey, ORNL/RASA-84/3, Oak Ridge, Tenn., October 1984.

8. Oak Ridge National Laboratory. Results of the Radiological Survey at 80 Hancock Street (LJ059), Lodi, New Jersey, ORNL/RASA-88/16, Oak Ridge, Tenn., March 1989.

9. Thermo Analytical/Eberline. "Technical Review of FUSRAP Instrument Calibrations by Comparison to TMC Calibration Pads," May 1989.

10. U.S. Code of Federal Regulations. 40 CFR 192, "Health and Environmental Protection Standards for Uranium and Thorium Mill Tailings," Washington, D.C., July 1986.

11. National Council on Radiation Protection and Measurements. Environmental Radiation Measurements, NCRP Report No. 50, Washington, D.C., December 27, 1986.

12. Levin, S. G., R. K. Stoms, E. Kuerze, and W. Huskisson. "Summary of Natural Environmental Gamma Radiation Using a Calibrated Portable Scintillation Counter." Radiological Health Data Report 9:679-695 (1968).

APPENDIX A
GEOLOGIC DRILL LOGS FOR 80 HANCOCK STREET

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1192R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
80 Hancock St. (LODI)	N 1,785 E 1,953	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-3-87	12-3-87	E.D.I.	MOBILE B-57	6.5"	12.0		12.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
7.4/70		6			/	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./ 30 in.	NONE	D. Harnish

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH
SS	1.5	1.3	8-10-8					
SS	2.0	1.7	5-7-9-6					
SS	1.0	1.1	3-4					5
SS	2.0	1.1	11-17 19-26					
SS	2.0	0.6	19-22 15-15					
SS	2.0	1.6	11-12 18-14					10

DESCRIPTION AND CLASSIFICATION

0.0 - 6.0 Ft. SILT and GRAVEL FILL (ML, GP-GM).

0.0-0.5 Ft. Gravel, broken basalt.

0.5-1.2 Ft. Silt, reddish brown with pieces of decomposed Brunswick sandstone and soft pebbles of yellow and olive gray silt.

1.2-2.0 Ft. Silt, mixed light gray and dark gray.

2.0-2.7 Ft. Silt, mixed brown and reddish brown.

2.7-3.1 Ft. Silty gravel, broken basalt, pieces 0.5-2 in. in diameter.

3.1-5.0 Ft. Gravelly silt, reddish brown with minor black, grayish green and yellowish brown silt mixed in, some angular gravel.

5.0-6.0 Ft. Rock, basalt?

6.0 - 12.0 Ft. SAND (SP). Brown (7.5YR4/2), very fine-grained, saturated, soft.

10.0-12.0 Ft. Sand and silt, interbedded, beds 3-10 mm thick.

Bottom of borehole at 12.0 Ft.
Borehole backfilled with spoils, 12/3/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-12 Ft. using 6.5 in. o.d. hollow-stem auger. Radiologically sampled and gamma-logged by TMA-Eberline, Inc. 0-0.5 Ft. No sample; roadbed.

5.0 Ft. Rock blocks sampler. Auger to 6.0 Ft.

Description and classification of soils by visual examination.

SS = 3" SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 80 Hancock St. (LODI) HOLE NO. 1192R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1189R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
Hancock St. (LODI)	N 1,986 E 1,980	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-2-87	12-2-87	E.D.I.	MOBILE B-57	6.5"	12.0		12.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
5.4/45		6			/	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./ 30 in.	NONE	D. Harnish

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH
SS	2.0	0.1						
SS	2.0	1.2	11-14 10-11					
SS	2.0	1.5	4-3-9 20					5
SS	2.0	0.0	16-20 22-24					
SS	2.0	1.1	8-12 14-21					
SS	2.0	1.5	8-10 12-8					10

DESCRIPTION AND CLASSIFICATION

0.0 - 5.3 Ft. GRAVEL and SILT FILL (GP, ML).

0.0-2.0 Ft. Gravel, broken basalt, cobbles on top, some silt.

2.0-5.3 Ft. Silt, dark grayish brown (2.5Y4/2) with pieces of yellowish brown, gray, black and grayish green silt, overall green tint.

5.3 - 8.0 Ft. SILT and SAND (ML, SP). Brown (10YR5/3), sand is very fine-grained, finely interbedded, damp.

6.0-8.0 Ft. Saturated, liquefied.

8.0 - 12.0 Ft. SILT (ML). Yellowish brown (10YR5/4), laminated.

10.2-10.8 Ft. Weak red.

10.8-10.9 Ft. Brownish yellow.

10.9-11.1 Ft. Dark brown.

Bottom of borehole at 12.0 Ft.
Borehole backfilled with spoils, 12/2/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-12 Ft. using 6.5 in. o.d. hollow-stem auger. Radiologically sampled and gamma-logged by TMA-Eberline, Inc.

0-2 Ft. Grab sample from auger flights.

6-8 Ft. Grab sample from auger flights. Sampler pushing a rock.

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: Hancock St. (LODI) — HOLE NO. 1189R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	2026R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
80 Hancock St. (LODI)	N 1,725 E 1,983	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
9-27-88	9-27-88	EMPIRE SOILS	CME 45B	12"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
9.5/95		5			8.0/ 9/27/88 /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
300 lbs./ 24 in.	NONE	J. Lord

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.5	1.0	4-5-4						0.0 - 0.5 Ft. ASPHALT & GRAVEL. AIRCO driveway.	Borehole advanced 0-10 Ft. using 12 in. o.d. hollow-stem augers. Radiologically sampled and gamma-logged by TMA-Eberline, Inc.
SS	2.0	2.0	2-2-2-3						0.5 - 3.4 Ft. Silty gravelly SAND. (SM-SG). Moderate brown (5YR3/4) to dusky red (5R3/4) mixed organic flecks, brick, gravel with a sandy silt loam. Dry, soft, crumbles easily. No cohesion. FILL.	
SS	2.0	2.0	4-18 20-15					5	3.4 - 6.5 Ft. Silty SAND (SM). Light gray (N6) to light bluish gray (5B7/1). Wet, loose, adhesive, slightly stiff. Slight fines component, slightly elastic or rubbery.	
SS	2.0	2.0	5-5-6-9						6.5 - 10.0 Ft. Silty SAND (SM). Dark yellowish orange (10YR6/6) medium- to coarse-grained sand. Subangular, poorly sorted with 20% silt. Adhesive due to the moisture. No shear strength. Mixed feldspar and quartz minerals. Compact, no thread, rubbery. 8.2-8.4 Ft. Saturated to 'runny'.	8.0 Ft. Groundwater observed. 6.5 Ft. Top of undisturbed soil.
SS	2.0	2.0	8-10-15 17					10		

Bottom of borehole at 10.0 Ft.
Borehole backfilled with clean spoils, 9/27/88.

Description and classification of soils by visual examination of samples.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE	HOLE NO.
80 Hancock St. (LODI)	2026R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1230R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
80 Hancock St. (LODI)	N 1,870 E 1,995	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-6-87	12-6-87	E.D.I.	MOBILE B-57	6.5"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
5.5/65		5			/	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./ 30 in.	NONE	D. Harnish

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH
SS	1.5	1.2	8-7-16					
SS	1.0	0.9	8-20					
SS	2.0	1.0	5-15-4-4					
								5
SS	2.0	0.9	7-27 22-25					
SS	2.0	1.5	12-24 26-29					
								10

DESCRIPTION AND CLASSIFICATION

0.0 - 4.7 Ft. Silty GRAVEL, SILT, and Gravelly SILT FILL (GM, ML, GM-ML).

0.0-0.5 Ft. Silty GRAVEL, broken basalt gravel.

0.5-2.5 Ft. Silt, dark brown (7.5YR3/4), some gravel

2.5-4.7 Ft. Gravelly silt, dark reddish brown (2.5YR3/4), some Brunswick sandstone gravel, minor granite gravel; silt and sand are decomposed Brunswick formation.

4.7 - 6.0 Ft. Sandy SILT (ML-SM). Greenish gray with minor iron-oxide mottling, very fine-grained, natural undisturbed sediments.

6.0 - 10.0 Ft. SILT (ML). Brown (7.5YR4/2) with olive stain on top.

6.9-8.0 Ft. Yellowish brown (10YR5/4), clayey.

Bottom of borehole at 10.0 Ft.
Borehole backfilled with spoils, 12/6/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-10 Ft. using 6.5 in. o.d. hollow-stem auger.
Gamma-logged by TMA-Eberline, Inc.
3-4 Ft. Grab sample from auger flights.

ENMET reads 100 ppm 6 in. into 10 ft. deep hole.

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE	HOLE NO.
80 Hancock St. (LODI)	1230R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1221R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
80 Hancock St. (LODI)	N 1,800 E 2,017	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-7-87	12-7-87	E.D.I.	MOBILE B-57	6.5"	7.5		7.5

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
5.3/76		4			/	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./ 30 in.	NONE	D. Harnish

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH
SS	2.0	1.5	7-24 15-13					
SS	1.5	1.1	7-7-7					
SS	2.0	2.0	3-24 16-13					5
SS	1.5	0.7	7-21-61 50/2"					

DESCRIPTION AND CLASSIFICATION

0.0 - 4.2 Ft. GRAVEL and Silty GRAVEL (GP, GM).

0.0-0.5 Ft. Gravel, broken basalt gravel.

0.5-4.2 Ft. Silty gravel, dusky red, Brunswick sandstone in a matrix of decomposed Brunsick formation, minor olive gray sandstone gravel.

4.2 - 5.3 Ft. SILT (ML). Very dark gray (7.5YR3/0) with some iron-oxide mottling, clayey, soft.

5.1-5.3 Ft. Clayey sand, gray (7.5YR5/0).

5.3 - 6.7 Ft. SILT (ML). Light brownish gray (2.5Y6/2) becoming grayish brown downward (10YR5/2), dry on top, medium stiff.

6.0-6.6 Ft. Grayish brown, clayey, damp.

6.6-6.7 Ft. Grayish green.

6.7 - 7.5 Ft. SAND (SP). Very fine-grained, clean.

Bottom of borehole at 7.5 ft.
Borehole backfilled with spoils, 12/7/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-7.5 Ft. using 6.5 in. o.d. hollow-stem auger.
Gamma-logged by TMA-Eberline, Inc.

Silt discolored green at contact with moisture.

7.5 Ft. Auger refusal.

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE	HOLE NO.
80 Hancock St. (LODI)	1221R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1220R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
80 Hancock St. (LODI)	N 1,932 E 2,027	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-7-87	12-7-87	E.D.I.	MOBILE B-57	6.5"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
6.3/63		5			/	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./ 30 in.	NONE	D. Harnish

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH
SS	2.0	1.7	1-4-8-7					
SS	2.0	1.8	5-7-5-7					
SS	2.0	0.9	7-7-8-12					5
SS	2.0	1.9	6-30-45 36					
SS	2.0	0.0	16-21 20-21					

DESCRIPTION AND CLASSIFICATION

0.0 - 4.6 Ft. Gravelly SILT and SILT FILL (GM-ML, ML).

0.0-2.5 Ft. Gravelly silt; dusky red and reddish brown. Gravel is Brunswick sandstone.

2.5-4.0 Ft. Silt; dark gray to black, organic, plant fragments, minor gravel of Brunswick sandstone.

4.0-4.3 Ft. Sand; grayish brown (2.5Y5/2) with greenish gray silt pieces, minor gravel.

4.3-4.6 Ft. Silt; interlayered dark reddish brown and greyish green.

4.6 - 6.6 Ft. SILT (ML). Very dark gray (2.5Y3/0), soft.

6.6 - 7.3 Ft. SAND (SP). Greenish gray to gray (10YR5/3) becoming brown downward, very fine-grained.

7.3 - 10.0 Ft. SILT (ML). Brownish yellow (10YR6/6) becoming reddish brown with depth (5YR5/4), dry, stiff, crumbly.

Bottom of borehole at 10.0 ft.
Borehole backfilled with spoils, 12/7/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-10 Ft. using 6.5 in. o.d. hollow-stem auger.
Gamma-logged by TMA-Eberline, Inc.

4.0-6.6 Ft. Radiologically elevated, as detected with hand "pancake" probe.

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	2025R

SITE	COORDINATES	ANGLE FROM HORIZ.	BEARING
80 Hancock St. (LODI)	N 1,711 E 2,035	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
9-23-88	9-23-88	EMPIRE SOILS	CME 45B	12"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
9.0/100		5			8.0/ 9/23/88 /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
300 lbs./ 24 in.	NONE	J. Lord

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY
SS	1.0	1.0	7-5
SS	2.0	2.0	2-2-2-2
SS	2.0	2.0	9-8-11 15
SS	2.0	2.0	6-7-8-12
SS	2.0	2.0	13-13 15-16

WATER PRESSURE TESTS: LOSS IN G.P.M. / PRESS. P.S.I. / TIME IN MIN. — ELEV. — DEPTH — GRAPHICS — SAMPLE

DESCRIPTION AND CLASSIFICATION

0.0 - 1.0 Ft. ASPHALT & GRAVEL. AIRCO driveway.

1.0 - 2.8 Ft. Silty gravelly SAND. (SM-SG). Moderate brown (5YR3/4) to dusky red (5R3/4) mixed organic flecks, brick, gravel with a sandy silt loam. Dry, soft, crumbles easily. No cohesion. FILL.

2.8 - 6.0 Ft. Silty SAND (SM). Greenish gray (5G6/1). Moist, loose, adhesive, slightly stiff. Slight fines component. No thread.

6.0 - 9.0 Ft. Silty SAND (SM). Moderate yellowish brown (10YR5/4) medium- to coarse-grained silty sand. Subangular, poorly sorted with 20% silt. Adhesive due to the moisture. No shear strength. Mixed feldspar and quartz minerals. Compact, no thread, rubbery. Crumbles easily.

8.0-8.2 Ft. A 'runny' saturated interval.

9.0 - 10.0 Ft. Sandy SILT (ML). Light brown (5YR5/6). Very slightly moist. Stiff, well sorted, slightly cohesive, but crumbles easily. Dense.

Bottom of borehole at 10.0 Ft.
Borehole backfilled with clean spoils, 9/23/88.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-10 Ft. using 12 in. o.d. hollow-stem augers. Radiologically sampled and gamma-logged by TMA-Eberline, Inc.

8.0 Ft. Groundwater observed.
6.0 Ft. Top of undisturbed soil.

Description and classification of soils by visual examination of samples.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 80 Hancock St. (LODI) — HOLE NO. 2025R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1193R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
Hancock St. (LODI)	N 1,988 E 2,067	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-3-87	12-3-87	E.D.I.	MOBILE B-57	6.5"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
5.7/57		5			/ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./ 30 in.	NONE	D. Harnish

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH
SS	1.5	1.0	12-20-15					
SS	2.0	0.2	5-7-8 11					
SS	2.0	1.4	7-12-16 20					5
SS	2.0	1.8	8-6-10 10					
SS	2.0	1.3	6-8-10 10					

DESCRIPTION AND CLASSIFICATION

0.0 - 4.0 Ft. GRAVEL, Gravelly SILT and SILT FILL (GP, GM-ML, OL).

0.0-0.5 Ft. Gravel, broken basalt.

0.5-2.3 Ft. Gravelly silt, gray and brown. Gravel of decomposed and broken Brunswick sandstone.

2.3-4.0 Ft. Silt, dark grayish brown (2.5Y4/2).

4.0 - 6.3 Ft. SILT (ML). Light gray (2.56/0) with abundant yellowish brown iron-oxide mottling.

6.3 - 10.0 Ft. SILT and SAND (ML, SP). Dark yellowish brown (10YR4/4), very fine-grained, interbedded on scale of 1 cm.

8-10 Ft. Sand, very fine-grained.

Bottom of borehole at 10.0 Ft.
Borehole backfilled with spoils, 12/3/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-10 Ft. using 6.5 in. o.d. hollow-stem auger. Radiologically sampled and gamma-logged by TMA-Eberline, Inc. 0-0.5 Ft. No sample; roadbed.

2-4 Ft. Supplimentary grab sample from auger.

Hole caved in to 9.0 Ft.

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: Hancock St. (LODI) HOLE NO. 1193R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	2024R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
80 Hancock St. (LODI)	N 1,705 E 2,100	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
9-23-88	9-23-88	EMPIRE SOILS	CME 45B	12"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
8.4/88		5			▽ 8.4/ 9/23/88 /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
300 lbs./ 24 in.	NONE	J. Lord

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH
SS	1.5	1.2	10-10-8					
SS	2.0	1.2	3-2-2-5					
SS	2.0	2.0	11-7-12 17					5
SS	2.0	2.0	8-10 14-20					
SS	2.0	2.0	5-8-9-13					▽ 10

DESCRIPTION AND CLASSIFICATION

0.0 - 0.5 Ft. ASPHALT & GRAVEL. AIRCO driveway.

0.5 - 3.0 Ft. Silty gravelly SAND. (SM-SG). Moderate brown (5YR3/4) to dusky red (5R3/4) mixed organic flecks, brick, gravel with a sandy silt loam. Dry, soft, crumbles easily. No cohesion. FILL.

3.0 - 6.4 Ft. Silty SAND (SM). Dark yellowish orange (10YR6/6) then grading to light gray (N6) or light bluish gray (5B7/1). Wet, loose, adhesive, slightly stiff. Slight fines component, slightly elastic or rubbery.

6.4 - 9.0 Ft. Silty SAND (SM). Moderate yellowish brown (10YR5/4) coarse silty sand. Subangular, poorly sorted with 20% silt. Adhesive due to the moisture. No shear strength. Mixed feldspar and quartz minerals. Compact, no thread, rubbery. Crumbles easily.

9.0 - 10.0 Ft. Sandy SILT (ML). Light brown (5YR5/6). Very slightly moist. Stiff, well sorted, slightly cohesive, but crumbles easily. Dense.

Bottom of borehole at 10.0 Ft.
Borehole backfilled with clean spoils, 9/23/88.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-10 Ft. using 12 in. o.d. hollow-stem augers. Radiologically sampled and gamma-logged by TMA-Eberline, Inc.

8.4 Ft. Groundwater observed.
6.4 Ft. Top of undisturbed soil.

Description and classification of soils by visual examination of samples.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 80 Hancock St. (LODI) HOLE NO. 2024R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1225R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
Hancock St. (LODI)	N 1,991 E 2,172	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-8-87	12-8-87	E.D.I.	MOBILE B-57	6.5"	8.0		8.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
5.1/64		4			/	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs/ 30 in.	NONE	D. Harnish

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY
SS	1.5	1.3	7-14-20
SS	2.0	0.2	20-10 9-7
SS	2.0	1.8	14-22 30-41
SS	2.0	1.8	15-15 25-25

WATER PRESSURE TESTS: LOSS IN G.P.M. / PRESS. P.S.I. / TIME IN MIN. — ELEV. — DEPTH — GRAPHICS — SAMPLE

DESCRIPTION AND CLASSIFICATION

0.0 - 2.8 Ft. GRAVEL and Silty GRAVEL FILL (GP, GM).

0.0-0.7 Ft. Gravel, asphalt and broken basalt gravel.

0.7-2.8 Ft. Silty gravel. Dusky red Brunswick sandstone with dusky red silt.

2.8 - 5.1 Ft. Silty SAND and Gravelly SILT FILL (?) (SM, ML-GM).

2.8-4.0 Ft. Silty sand. Dark gray (5Y4/1) with greenish tint, soft, damp.

4.0-4.9 Ft. Gravelly silt. Greenish gray with round Brunswick sandstone gravel.

4.9-5.1 Ft. Silty sand. Greenish gray.

5.1 - 5.4 Ft. SILT (ML). Reddish brown (5YR5/2), olive stain on top.

5.4 - 8.0 Ft. SAND (SP). Fine- to medium-grained, some silt, minor gravel, subangular grains.

5.4-6.0 Ft. Weak red (2.5YR4/2).

6.0-8.0 Ft. Reddish brown (5YR4/3). Minor gravel, wet.

Bottom of borehole at 8.0 Ft.
Borehole backfilled with spoils, 12/8/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-8 Ft. using 6.5 in. o.d. hollow-stem auger. Radiologically sampled and gamma-logged by TMA-Eberline, Inc. 2-4 Ft. Grab sample from auger flights.

0-0.5 Ft. No sample; roadbed.

ENMET reads 100 ppm at top of 6 Ft. hole.

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: Hancock St. (LODI) — HOLE NO. 1225R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	2022R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
80 Hancock St. (LODI)	N 1,711 E 2,182	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
9-22-88	9-22-88	EMPIRE SOILS	CME 45 B	12"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
7.3/77		5			9.0/ 9/22/88	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
300 lbs./ 24 in.	NONE	J. Lord

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.5	1.5	10-15-22						0.0 - 0.5 Ft. ASPHALT & GRAVEL. AIRCO Driveway.	0-10 Ft. advanced using 6 1/4 in. i.d. hollow stem augers. Sampled and gamma-logged to 10' by TMA-Eberline, Inc.
SS	2.0	0.0	5-6-6-7						0.5 - 4.0 Ft. Sandy SILT FILL. Moderate brown (5YR3/4) to dusky red (5R3/4). Mixed organic flecks, brick, gravel with a sandy silt loam. Dry, soft, crumbles easily. No cohesion.	
SS	2.0	2.0	3-6-8-12					5	4.0 - 7.7 Ft. Silty SAND (SM). Light gray (N6) to olive brown (5Y4/4). Wet, loose, adhesive, slightly stiff. Slight fines component. 6.0-7.7 Ft. Wet to saturated; stiffer with depth.	
SS	2.0	1.8	10-10 16-12						7.7 - 10.0 Ft. Silty SAND (SM). Moderate yellowish brown (10YR5/4) medium- to coarse-grained sand. Wet, subangular, poorly sorted with 20% silt. Adhesive due to the moisture. No shear strength. Mixed feldspar and quartz minerals. Compact, no thread, rubbery.	9.0 Ft. Groundwater observed. 7.7 Ft. Top of undisturbed soil.
SS	2.0	2.0	10-12 10-5					10		
									Bottom of borehole at 10.0 Ft. Borehole backfilled with clean spoils, 9/25/88.	Description and classification of soils by visual examination of samples.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 80 Hancock St. (LODI)

HOLE NO. 2022R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1222R

SITE	COORDINATES	ANGLE FROM HORIZ.	BEARING
80 Hancock St. (LODI)	N 1,933 E 2,186	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-7-87	12-7-87	E.D.I.	MOBILE B-57	6.5"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
6.3/63		5			/	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./ 30 in.	NONE	D. Harnish

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M.	PRESS. P.S.I.	TIME IN MIN.	ELEV.
SS	2.0	1.0	1-1-6-14				
SS	2.0	1.7	15-14 14-15				
SS	2.0	2.0	7-2-2-5				
SS	2.0	1.6	3-21-20 19				
SS	2.0		6-9-11--				

DEPTH: 5, 10

DESCRIPTION AND CLASSIFICATION

0.0 - 4.6 Ft. Gravelly SILT, GRAVEL, and SILT FILL (GM-ML, GP, ML).

0.0-2.4 Ft. Gravelly silt, dark reddish brown (5YR3/3) mixed with dark brown topsoil and Brunswick sandstone gravel; glass at base.

2.4-3.0 Ft. Gravel, dusky red, Brunswick sandstone.

3.0-3.3 Ft. Silt, mixed dark gray, dark reddish brown, brownish yellow, some black silt.

3.3-4.6 Ft. Gravel, dusky red, Brunswick sandstone; dead plants and grass at base, (pre-fill surface?).

4.6 - 6.9 Ft. SILT (ML).

4.6-4.9 Ft. Reddish gray, organic.

4.9-5.4 Ft. Sandy, gray (10YR5/1).

5.4-6.8 Ft. Very dark gray (7.5YR3/0).

6.8-6.9 Ft. Sand, very dark gray.

6.8 - 10.0 Ft. SILT (ML). Light brown (7.5YR6/4) and dry becoming brown (7.5YR5/4) and damp downward.

Bottom of borehole at 10.0 Ft.
Borehole backfilled with spoils, 12/7/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-10 Ft. using 6.5 in. o.d. hollow-stem auger.
Gamma-logged by TMA-Eberline, Inc.
1-2 Ft. Grab sample from auger flights.
3.5-4.0 Ft. Brunswick SS erratic.

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 80 Hancock St. (LODI) — HOLE NO. 1222R

GEOLOGIC DRILL LOG

PROJECT: FUSRAP	JOB NO.: 14501-138	SHEET NO.: 1 OF 1	HOLE NO.: 2023R	
SITE: 80 Hancock St. (LODI)	COORDINATES: N 1,800 E 2,194	ANGLE FROM HORIZ: Vertical	BEARING: ------	
BEGUN: 9-25-88	COMPLETED: 9-25-88	DRILLER: EMPIRE SOILS	DRILL MAKE AND MODEL: CME 45B	SIZE: 12"
OVERBURDEN: 14.0	ROCK (FT.):	TOTAL DEPTH: 14.0	CORE RECOVERY (FT./%): 11.9/88	CORE BOXES:
SAMPLES: 7	EL. TOP CASING:	GROUND EL.:	DEPTH/EL. GROUND WATER: 8.2/ 9/25/88	DEPTH/EL. TOP OF ROCK: /
SAMPLE HAMMER WEIGHT/FALL: 300 lbs./ 24 in.	CASING LEFT IN HOLE: DIA./LENGTH: NONE	LOGGED BY: J. Lord		

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY
SS	1.5	1.0	9-11-13
SS	2.0	2.0	10-8-6-5
SS	2.0	1.1	2-2-2-6
SS	2.0	1.8	9-10-10 10
SS	2.0	2.0	10-8-11 12
SS	2.0	2.0	5-5-8-7
SS	2.0	2.0	7-10-11 9

WATER PRESSURE TESTS: LOSS IN G.P.M | PRESS. P.S.I. | TIME IN MIN. — ELEV. — DEPTH (5, 10) — GRAPHICS — SAMPLE

DESCRIPTION AND CLASSIFICATION

0.0 - 0.5 Ft. ASPHALT & GRAVEL. AIRCO Driveway.

0.5 - 4.3 Ft. Silty gravelly SAND. Moderate brown (5YR3/4) to dusky red (5R3/4) mixed organic flecks, brick, gravel with a sandy silt loam. Dry, soft, crumbles easily. No cohesion. Strong petroleum odor. Borehole next to underground diesel storage tank. FILL.

4.3 - 6.8 Ft. Silty SAND (SM). Light gray (N6) to light bluish gray (5B7/1). Wet, loose, adhesive, slightly stiff. Slight fines component, slightly elastic or rubbery.

6.8 - 13.5 Ft. Silty SAND (SM). Dark yellowish orange (10YR6/6) medium- to coarse-grained sand. Subangular, poorly sorted with 20% silt. Adhesive due to the moisture. No shear strength. Mixed feldspar and quartz minerals. Compact, no thread, rubbery.

13.2-13.3 Ft. Saturated to runny, then stiff to 13.5 Ft.

13.5 -14.0 Ft. SAND (SG). Moderate brown (5YR3/4) coarse-grained sand with some fines. Saturated, slightly adhesive, loose. Mixed mineralogy.

Bottom of borehole at 14.0 Ft.
Borehole backfilled with clean spoils, 9/25/88.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-13 Ft. using 12" o.d. hollow-stem augers. Split-spoons sampled to 14.0 Ft.

Sampled and gamma-logged by TMA-Eberline, Inc.

8.2 Ft. Groundwater observed.

1-3 Ft. High ENMET readings; off scale. Seal 1-3 Ft. interval with auger. No more high readings.

Description and classification of soils by visual examination of samples.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 80 Hancock St. (LODI) HOLE NO.: 2023R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1228R

SITE	COORDINATES	ANGLE FROM HORIZ.	BEARING
80 Hancock St. (LODI)	N 1,844 E 2,211	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-8-87	12-8-87	E.D.I.	MOBILE B-57	6.5"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
5.7/60		5			/ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./ 30 in.	NONE	D. Harnish

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH
SS	1.5	1.3	6-10-21					
SS	2.0	1.2	11-20 12-12					
SS	2.0	0.2	12-3-3 21					5
SS	2.0	1.5	14-24 22-27					
SS	2.0	1.5	19-35 31-33					10

DESCRIPTION AND CLASSIFICATION

0.0 - 4.0 Ft. GRAVEL and SILT FILL (GP, ML).

0.0-0.5 Ft. Gravel; broken basalt.

0.5-1.2 Ft. Silt; very dark gray and light gray, interlayered.

1.2-4.0 Ft. Gravel; dusky red Brunswick formation.

1.5-1.6 Ft. Dark brown silt with basalt gravel.

4.0 - 6.1 Ft. SAND (SP). Gray (5YR5/1), fine-grained, damp.

6.1 - 8.3 Ft. SILT (ML). Brown (7.5YR3/4), crumbly, slightly damp, massive.

8.3 - 8.7 Ft. Silty SAND (SM). Strong brown (7.5YR3/4).

8.7 - 10.0 Ft. SILT and Silty SAND (ML, SM). Grayish brown (10Y5/2), silt becomes silty sand downward, very fine- to fine-grained.

Bottom of borehole at 10.0 ft.
Borehole backfilled with spoils, 12/8/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-10 Ft. using 6.5 in. o.d. hollow-stem auger.
Gamma-logged by TMA-Eberline, Inc.
0-0.5 Ft. No sample. Road bed.

ENMET reads 110 ppm 6 in. into 10 ft. deep hole.

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 80 Hancock St. (LODI) — HOLE NO. 1228R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	2021R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
80 Hancock St. (LODI)	N 1,763 E 2,250	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
9-25-88	9-25-88	EMPIRE SOILS	CME 45B	12"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
6.5/81		4			8.0/ 9/25/88 /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
300 lbs./ 24 in.	NONE	J. Lord

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	2.0	1.8	5-5-6-17								0.0 - 0.2 Ft. ASPHALT & GRAVEL. AIRCO Driveway.	Borehole advanced 0-10 Ft. using 12 in. o.d. hollow-stem augers. Sampled to 8' and gamma-logged to 10' by TMA-Eberline, Inc.
SS	2.0	1.0	5-3-4-3								0.2 - 5.0 Ft. Silty gravelly SAND. (SM-SG). Moderate brown (5YR3/4) to dusky red (5R3/4). Mixed organic flecks, brick, gravel with a sandy silt loam. Dry, soft, crumbles easily. No cohesion. Strong petroleum odor. Borehole next to underground diesel storage tank.	
SS	2.0	1.7	2-2-6-11					5			5.0 - 6.8 Ft. Silty SAND (SM). Light gray (N6) to light bluish gray (5B7/1). Wet, loose, adhesive, slightly stiff. Slight fines component, slightly elastic or rubbery.	
SS	2.0	2.0	12-12 11-15								6.8 - 7.6 Ft. Silty SAND (SM). Moderate yellowish brown (10YR5/4) medium- to coarse-grained sand. Wet, subangular, poorly sorted with 20% silt. Adhesive due to the moisture. No shear strength. Mixed feldspar and quartz minerals. Compact, no thread, rubbery.	8.0 ft. Groundwater observed. 6.8 Ft. Top of undisturbed soil.
								10			7.6 - 10.0 Ft. SAND (SW). Moderate brown (5YR3/4) coarse-grained sand with some fines. Saturated, slightly adhesive, loose. Mixed mineralogy.	
											Bottom of borehole at 10.0 Ft. Borehole backfilled with clean spoils, 9/25/88.	Description and classification of soils by visual examination of samples.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 80 Hancock St. (LODI) — HOLE NO. 2021R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1224R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
80 Hancock St. (LODI)	N 1,925 E 2,253	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-8-87	12-8-87	E.D.I.	MOBILE B-57	6.5"	10.0		10.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
6.5/65		5			/	

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./ 30 in.	NONE	D. Harnish

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	PRESS. P.S.I.	TIME IN MIN.	ELEV.	DEPTH
SS	2.0	1.7	7-10-17 20					
SS	2.0	0.4	12-9 5-6					
SS	2.0	1.2	3-5-5-5					5
SS	2.0	1.6	12-26 30-45					
SS	2.0	1.6	6-16 17-15					10

DESCRIPTION AND CLASSIFICATION

0.0 - 4.6 Ft. Gravelly SILT and SILT FILL (GM-ML, ML).

0.0-0.7 Ft. Gravelly silt, dark grayish brown (10YR4/2), crushed Brunswick sandstone gravel.

0.7-1.2 Ft. Gravelly silt, dusky red (2.5YR3/2), crushed Brunswick sandstone gravel.

1.2-4.0 Ft. Gravelly silt, very dark gray (10YR3/1), abundant plant material, crushed Brunswick sandstone gravel.
4.0-4.6 Ft. Silt, weak red (5YR4/2), disturbed (?).

4.6 - 6.5 Ft. SILT (FILL?) (MH). Very dark gray (10YR4/1), organic.

6.5 - 10.0 Ft. SILT (ML). Weak red (2.5YR5/2), stiff, crumbly and dry, downward becomes dark reddish gray (5YR4/2) and wet.

8.0-8.2 Ft. Clay, same color.

8.2-10.0 Ft. Dark reddish gray, wet.

Bottom of borehole at 10.0 ft.
Borehole backfilled with spoils, 12/8/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-10 Ft. using 6.5 in. o.d. hollow-stem auger.
Gamma-logged by TMA-Eberline, Inc.
2-4 Ft. Grab sample from auger flights.

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE	HOLE NO.
80 Hancock St. (LODI)	1224R