Formerly Utilized Sites Remedial Action Program (FUSRAP)

Maywood Chemical Company Superfund Site

ADMINISTRATIVE RECORD

Document Number

MISS-023.



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CHARACTERIZATION REPORT FOR THE NEW JERSEY VEHICLE INSPECTION STATION PROPERTY LODI, NEW JERSEY

JUNE 1987

Prepared for

UNITED STATES DEPARTMENT OF ENERGY OAK RIDGE OPERATIONS OFFICE Under Contract No. DE-AC05-810R20722

Ву

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Bechtel Job No. 14501

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CM	centimeter
cm^2	square centimeter
cpm	counts per minute
đpm	disintegrations per minute
ft	foot
h	hour
in.	inch
1	liter
l/min	liters per minute
m	meter
m ²	square meter
µR/h	microroentgens per hour
mi	mile
mi ²	square mile
mrad/h	millirad per hour
mrem	millirem
mrem/yr	millirem per year
min	minute
pCi/g	picocuries per gram
pCi/l	picocuries per liter
WL	working level

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1.0 INTRODUCTION AND SUMMARY

1.1 INTRODUCTION

The 1984 Energy and Water Appropriations Act authorized the U.S. Department of Energy (DOE) to conduct a decontamination research and development project at four sites, including the site of the former Maywood Chemical Works (now owned by the Stepan Company) and its vicinity properties. The act was reauthorized in 1985. DOE has constructed the Maywood Interim Storage Site (MISS) on 11.7 acres of land west of the Stepan Company property. The New Jersey Vehicle Inspection Station property is included as one of the Maywood vicinity properties (Figure 1-1). The work is being administered by the Formerly Utilized Sites Remedial Action Program (FUSRAP), one of two remedial action programs under the direction of the DOE Division of Facility and Site Decommissioning Projects.

The U.S. Government initiated FUSRAP in 1974 to identify, clean up, or otherwise control sites where low-activity radioactive contamination (exceeding current guidelines) remains from the early years of the nation's atomic energy program or from commercial operations that resulted in conditions Congress has mandated DOE to remedy (Ref. 1).

FUSRAP is currently being managed by the DOE Oak Ridge Operations Office (ORO). As the Project Management Contractor (PMC) for FUSRAP, Bechtel National, Inc. (BNI) is responsible to DOE for planning, managing, and implementing FUSRAP.

1.2 PURPOSE AND OBJECTIVES

A radiological characterization of the New Jersey Vehicle Inspection Station (NJVIS) property has been conducted to establish the horizontal and vertical limits of radioactive contamination and to determine ranges of radionuclide concentrations. The information obtained from this characterization work will be used in planning

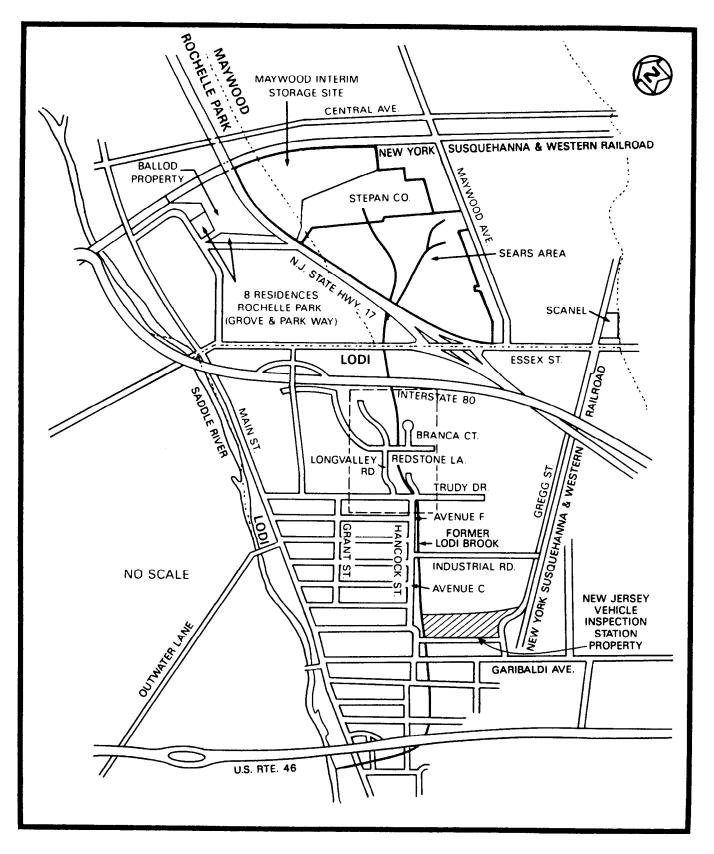


FIGURE 1-1 LOCATION OF THE MAYWOOD INTERIM STORAGE SITE, THE FORMER LODI BROOK, AND THE NEW JERSEY VEHICLE INSPECTION STATION any required remedial action. The results will also be used to satisfy an important secondary objective, which is to provide data to aid in the identification and evaluation of pathways by which contamination might have migrated from the property.

1.3 SUMMARY

This report summarizes the procedures and results of the radiological characterization of the NJVIS property conducted in July and December 1986 and the additional characterization work performed in February 1987.

The radiological characterization confirmed that thorium-232 is the primary radioactive contaminant. The surface soil sample results showed the maximum concentration of thorium-232 to be 12.5 pCi/g, which is in excess of the DOE guideline of 5.0 pCi/g plus background of 1.0 pCi/g for surface soils. The maximum concentration for radium-226 was 1.6 pCi/g above background, which does not exceed the guideline. The maximum uranium-238 concentration was less than 14.3 pCi/g above background, but no site-specific DOE guidelines for uranium have been established.

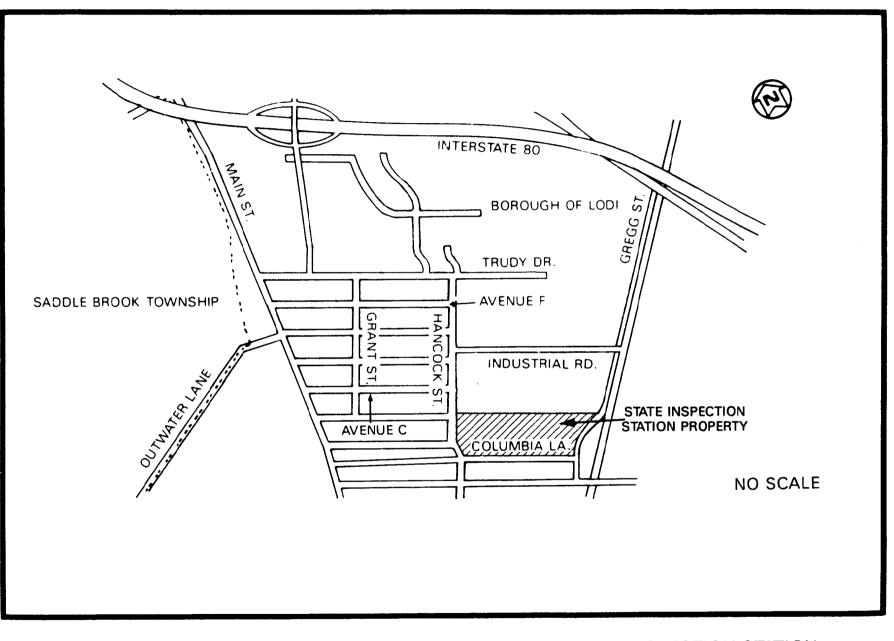
The results of downhole gamma logging indicate subsurface contamination at depths ranging from 1 to 7 ft.

2.0 SITE DESCRIPTION AND BACKGROUND

The New Jersey Vehicle Inspection Station (NJVIS) is located in a highly developed area of the Borough of Lodi, County of Bergen, New Jersey. The population density of the area is approximately 10,000 people per square mile. It is located approximately 12 mi north-northwest of downtown Manhattan (New York City) and 13 mi northeast of Newark, New Jersey. The property (14.3 acres) is bordered on the north by Hancock Street, the south by Gregg Street, the east by another commercial property, and the west by Columbia Lane (Figure 2-1).

The NJVIS property was shown to be radioactively contaminated during a radiological survey conducted in August 1984 by the Oak Ridge National Laboratory (ORNL) at the request of DOE (Ref. 2). The available data indicates that the contamination originated from the processing of monazite sand (thorium ore) by the Maywood Chemical Works from 1916 through 1956. During this time, slurry containing process wastes from the thorium operations was pumped to diked areas west of the plant. The area west of the plant was generally low and swampy at that time. In 1932, New Jersey Route 17 was built through this disposal area. Some of these process wastes were removed from the Maywood Chemical Works for use as mulch and fill on nearby properties, thereby contaminating them with radioactive thorium (Ref. 3). Additional waste apparently migrated off-site via the natural drainage provided by the former Lodi Brook.

In 1954, the Atomic Energy Commission (AEC) issued License R-103 to the Maywood Chemical Works allowing it to continue to ship, receive, possess, and process radioactive materials under the authority of the Atomic Energy Act of 1954. The Maywood Chemical Works stopped processing thorium in 1956 after approximately 40 years of production. The Maywood Chemical Works was sold to the Stepan Company in 1959 (Ref. 3).



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FIGURE 2-1 LOCATION OF THE NEW JERSEY STATE VEHICLE INSPECTION STATION PROPERTY

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3.0 RADIOLOGICAL CHARACTERIZATION

To provide sufficiently detailed information regarding the limits of radioactive contamination and to provide data for the development of cost-effective measures for any potential remedial action, both surface and subsurface investigations were performed.

To facilitate the collection of data in a systematic manner, a 50-ft grid was established over the area to be characterized. This grid was correlated with the New Jersey state grid system to ensure that it could be reestablished if remedial action is undertaken. All data correspond to coordinates on the characterization grid.

3.1 REMEDIAL ACTION GUIDELINES

Information collected during the radiological survey conducted by ORNL (Ref. 2) indicated that the radioactive contamination at the NJVIS property consists primarily of thorium-232, with typically much lower levels of radium-226 and uranium-238. Thorium is also known to be the primary contaminant at the MISS (Ref. 3). Table 3-1 lists the DOE residual contamination guidelines governing the release of formerly contaminated property for unrestricted use (Ref. 4).

3.2 SURFACE CHARACTERIZATION

Surface characterization was conducted with a shielded gamma scintillation detector. Near-surface gamma radiation measurements were taken 12 in. from the ground at the grid line intersections spaced 10 ft apart. The shielded detector was used to ensure that radiation detected by the probe originated from the ground directly beneath the unit. By shielding against lateral gamma flux, the shielded detector minimizes possible sources of error in the measurements. Furthermore, this detector was calibrated at the Technical Measurements Center (TMC) in Grand Junction, Colorado, to provide a correlation of counts per minute (cpm) to picocuries per gram (pCi/g). Based on this relationship, locations with

measurements of more than 11,000 cpm were noted as exceeding the DOE guideline of 5 pCi/g for thorium-232 in surface soils. To better define the limits of contamination, soil sampling locations were chosen by evaluating locations with measurements of more than 11,000 cpm, locations with measurements at or near 11,000 cpm, and the potential for lateral gamma flux. The sampling locations are shown in Figure 3-1. It should be noted that not all surface soil samples indicated contamination because some samples were taken from locations where the gamma measurement was at or near the guideline. The data in Table 3-2 show the maximum concentration of thorium-232 to be 12.5 pCi/g, which exceeds the DOE guideline for surface soils. Use of the "less than" (<) notation indicates that the radionuclide was not present in measurable concentrations. The value following the less than notation is the minimum detectable amount (MDA). The MDA is based on various factors, including the volume, size, and weight of the sample; the type of detector used; the counting time, and the background count rate. In addition, since radioactive decay is a random process, a correlation between the rate of disintegration and a given radionuclide concentration cannot be precisely established; therefore, the exact concentration of the radionuclide cannot be determined. As such, each value that is equal to or greater than the MDA has an associated uncertainty term (+), which represents the maximum amount by which the actual value can be expected to differ from the value given in the table. The uncertainty term has an associated confidence level of 95 percent.

The maximum concentration of radium-226 was 1.6 pCi/g, which is within the guideline. The maximum concentration of uranium-238 was less than 14.3 pCi/g, but no site-specific DOE guideline for uranium in soil has been established.

Although the concentrations for uranium-238 have higher values than thorium-232 concentrations, thorium-232 is considered the primary contaminant. As shown in Table 3-1, the guidelines for thorium-232 are 5 pCi/g for surface soil and 15 pCi/g for subsurface soil. Although no specific guidelines have been determined for

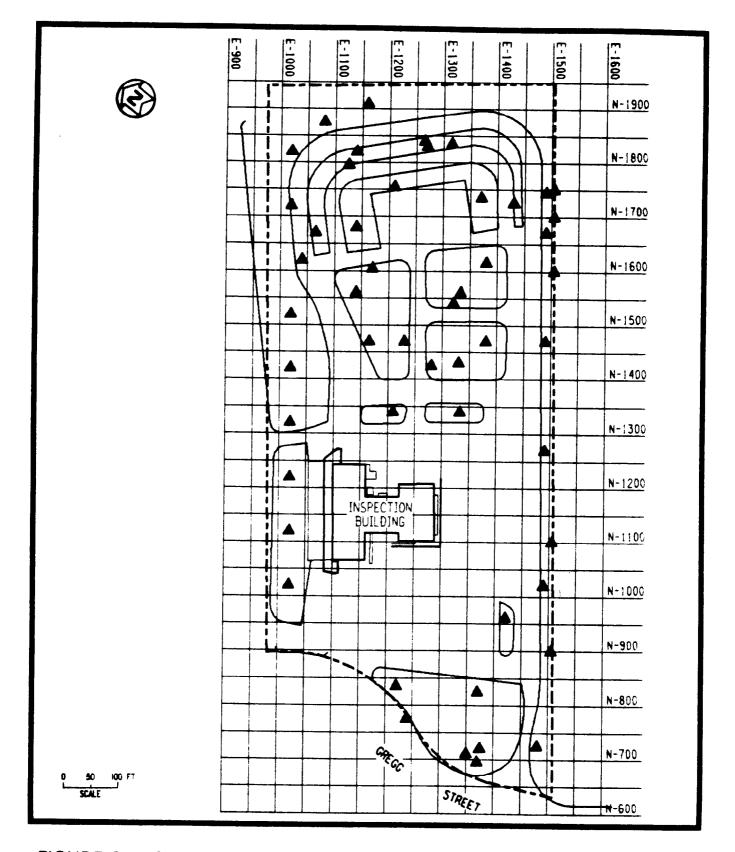


FIGURE 3-1 SURFACE SOIL SAMPLING LOCATIONS AT THE NEW JERSEY VEHICLE INSPECTION STATION PROPERTY

uranium-238, using a typical (as opposed to a site-specific) value to calculate the guideline would result in a guideline of approximately 75 pCi/g. Because the measured concentrations of thorium-232 exceed its guidelines by a greater percentage than uranium-238, thorium-232 is considered the primary contaminant.

Analysis of the surface soil sample taken at Coordinates El210, N1340 indicated the presence of cesium-137 at a concentration of 12 pCi/g. This appears to be an isolated occurrence as no evidence of cesium was found in other radiological samples. No explanation for the presence of this radionuclide has been determined.

The largest area of surface contamination exists north and east of the NJVIS building beginning at the property boundaries (north, east, and west) and extending southward to within approximately 150 ft of the building (Figure 3-2).

Additional small areas of surface contamination exist near the southeastern corner of the property near Gregg Street and near the northeastern corner of the NJVIS building. Areas of surface contamination are shown in Figure 3-2.

3.3 SUBSURFACE CHARACTERIZATION

After surface characterization was completed, a subsurface investigation was conducted to determine the depth of previously identified surface contamination and to locate subsurface contamination with no surface manifestation. The subsurface investigation was conducted using downhole gamma logging of the drill holes. This technique is significantly more cost effective than soil sampling, because the procedure can be completed more quickly and eliminates the need for laboratory analysis.

A 2-in. by 2-in. sodium iodide gamma scintillation detector was used to perform the downhole logging. The instrument was calibrated at TMC, where it was determined that a count rate of approximately 40,000 cpm corresponds to the 15-pCi/g guideline for thorium-232 in

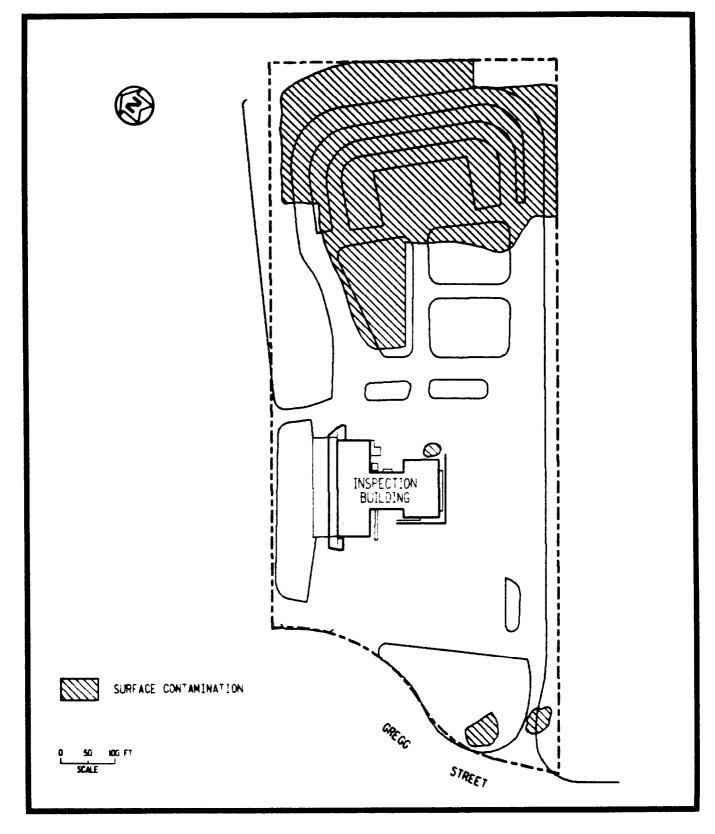


FIGURE 3-2 AREAS OF SURFACE CONTAMINATION AT THE NEW JERSEY VEHICLE INSPECTION STATION PROPERTY

subsurface soils. This relationship has been corroborated in results from previous characterizations where thorium-232 was found (Ref. 5). However, analysis of trends and marginal readings is necessary to predict the contamination boundaries.

During the course of the subsurface investigation, 113 radiological boreholes were drilled (Figure 3-3) and gamma logged to determine the depth of radioactive contamination. Detailed gamma logging data are presented in Table 3-3.

As shown in Figure 3-4, the largest area of subsurface contamination exists in the same location as surface contamination (north and east of the NJVIS building). The depths of this contamination range from 1 to 7 ft. Contamination is believed to have resulted primarily from stream sediment deposition and possibly from fill This belief is based on information obtained during emplacement. additional drilling activities conducted to better define the location of the original Lodi Brook streambed. It was determined that the streambed flowed through the northern section of the property. Radiological and geological data can be used to infer the streambed location on the basis of the presence of stream sediments and their degree of contamination. A logical assumption would be that the original streambed was probably located where the deepest and most contaminated stream sediments are found. Lodi Brook currently flows through a buried conduit in the northern section of the property. The conduit is parallel to Hancock Street (Figure 3-5).

Geological information regarding the location of the former Lodi Brook streambed also indicates that the exposed relic channel (Coordinates E1500, N1800, approximately) was not incised but rather was a broad, open channel, and contamination is not evenly distributed (Figure 3-6). This offers further explanation as to why some gamma logs from boreholes in or near the channel indicate concentrations below guidelines. It also explains why so little fill was needed to bring the concave channel up to its present grade. Fill depths in the former streambed vary from 0 to 6 ft.

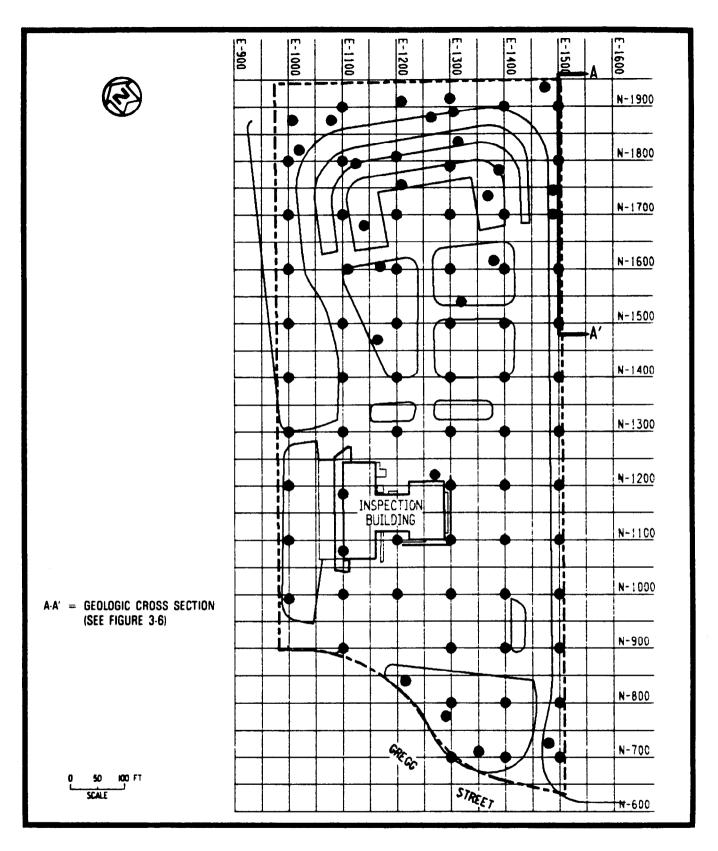
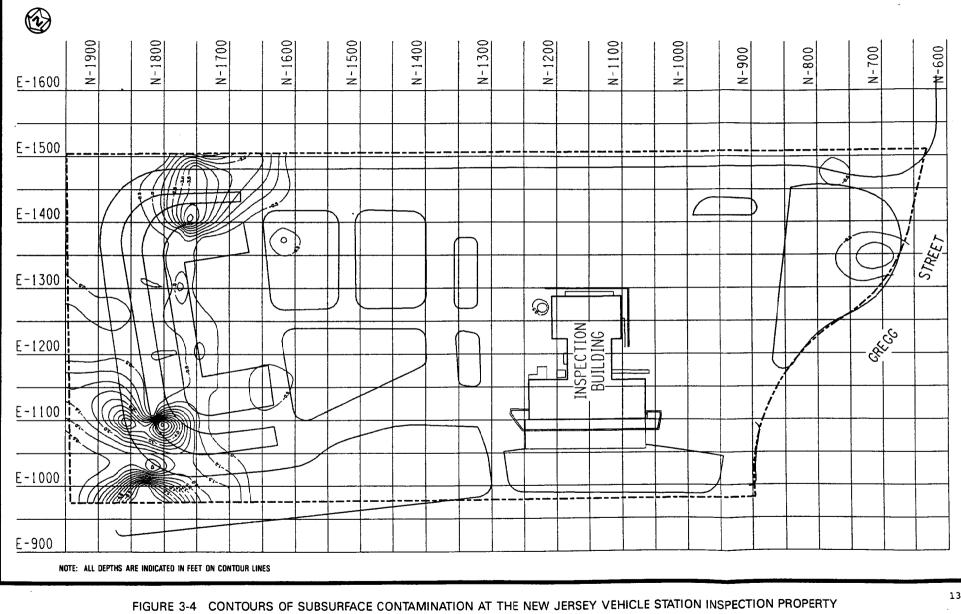


FIGURE 3-3 BOREHOLE LOCATIONS AT THE NEW JERSEY VEHICLE INSPECTION STATION PROPERTY

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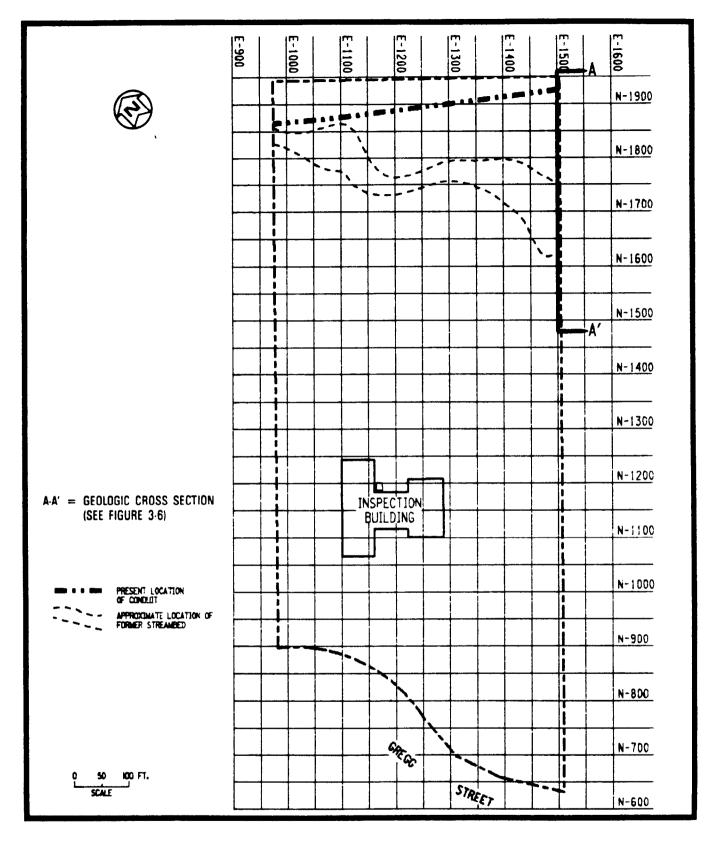
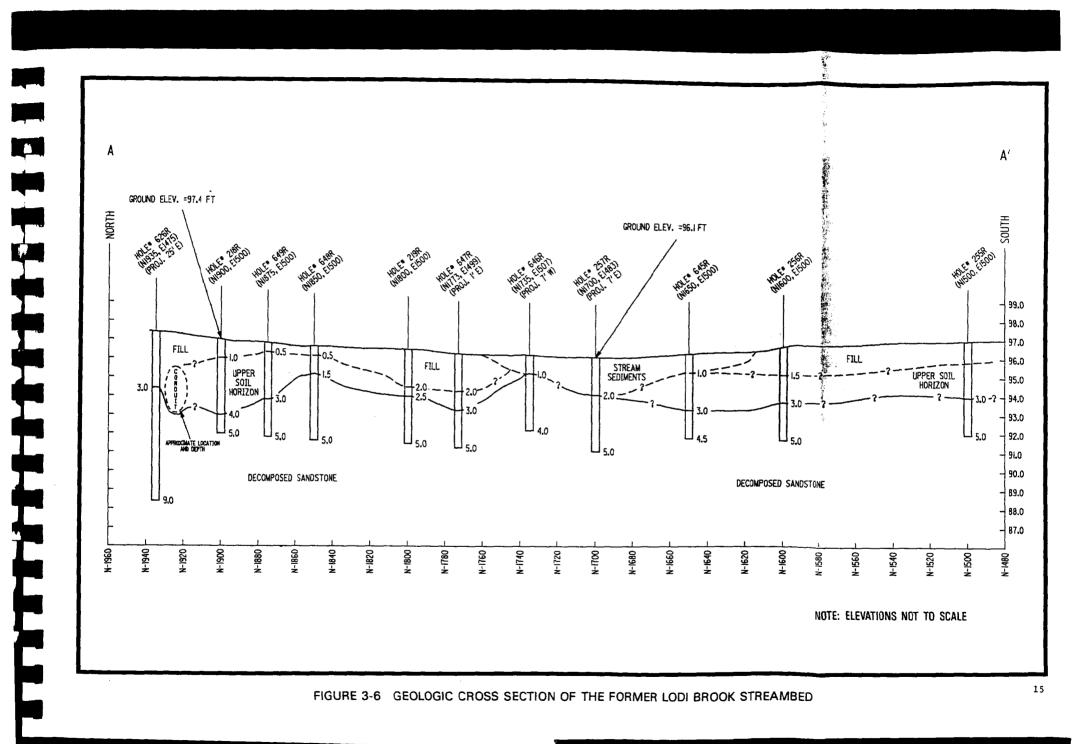


FIGURE 3-5 LOCATIONS OF THE PRESENT LODI BROOK (CONDUIT) AND THE ORIGINAL STREAMBED

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These fill depths conform to the natural 1-percent grade of the former streambed. The shallowness of fill (moved indigenous soil) also explains why the fill is so thoroughly contaminated with underlying black, thorium-bearing stream sediments. The former streambed and the present conduit converge in the northwestern corner of the property with contamination indicated above the conduit. Although drilling data in this area suggest that this contamination is mostly surficial, it may extend around the conduit in the northwestern corner of the property. Contamination appears to trend off the property to the north under Hancock Street as well as to the east and west toward properties contiguous with the NJVIS property.

Subsurface contamination (0.5 to 1.0 ft) found in a small area near the northeastern corner of the NJVIS building (Figure 3-3) is thought to result from fill emplacement. Contamination is not thought to exist beneath the building itself for four reasons: (1) no other areas of subsurface contamination were found either adjacent to or in close proximity to the building; (2) no subsurface contamination was indicated by any of the near-surface measurements taken close to the building; (3) the building may be founded on bedrock; no contamination has been found in any of the boreholes that have penetrated bedrock in this area (depth of bedrock is approximately 6 ft in this area), and the bedrock in this area has an extremely low primary hydraulic conductivity; and (4) interior exposure rate measurements were all within background levels. On the basis of this information, drilling inside the building was considered unnecessary and therefore was not performed.

The presence of subsurface contamination (0.5 to 1.5 ft) was also indicated in the southeastern corner of the property near Gregg Street (Figure 3-4) in an area where surface contamination is also present.

On the basis of geological information gained as a result of the borehole drilling during this characterization, it was determined that the property is relatively flat (total measured relief of

6.7 ft) and is underlain in most areas by at least two types of soil, fill, and naturally occurring sediments over the red, consolidated sandstone of the Brunswick Formation. There are competent sandstone outcrops in the southeastern section of the property. The sandstone layer extends beneath the surface of the property from depths of as much as 6 ft facing northwest toward the NJVIS building to depths greater than 20 ft below the surface in the central and northwestern areas of the property.

Unconsolidated materials of dark yellowish brown sandstone covered by a moderately brown, residual sandy soil are present in the slightly higher areas of the property. Three soil sequences are present in the low-lying areas of the property. The property south of the NJVIS building has a soil sequence of decomposed sandstone covered by a thin lens (1 to 2 ft) of black silty organic soil. These materials are buried by 1 to 3 ft of fill. In the area north of the NJVIS building, exposed black organic silt overlying decomposed Brunswick sandstone delineates the original Lodi Brook channel and its floodplain. Black silt is also present under the surrounding lawn, suggesting that stream sediment was taken from the channel and used as topsoil. The third type of soil sequence appears in many areas throughout the property and is represented by fill placed on top of indigenous brown soil.

In addition to the building, the property is presently covered with asphalt parking lots, roadways, and a grass lawn. A 3-ft-high berm exists in the northern section (drivers education area) of the property (along Coordinate N1775 and between Coordinates El150 and El350). The fill used on the property is primarily residual soil transported from higher elevations on the property. Areas with thick accumulations of fill include the berm in the drivers education area (6 ft), the original Lodi Brook channel (6 ft), the conduit through which the brook presently flows (5 to 7 ft), and locations of the property's drainage pipes (approximately 5 ft).

North of the NJVIS access road, surface water drains through three evenly spaced grates directly into the Lodi Brook conduit. The

remainder of the site is drained to the south by a series of surface drains and a buried pipeline. Immediately south of the berm in the drivers education area, this drainage system is ineffective; surface soil in this area is nearly saturated. Groundwater levels are shallowest (6 to 8 ft) in the northern and eastern sections of the property with mid-property levels at depths greater than 10 ft, suggesting a northeast to southwest gradient.

Along the eastern property boundary, a linear 10-ft-wide drainage sump is the only nonburied portion of the former Lodi Brook channel between the Saddle River and Interstate 80. Fill has been placed on both sides of this drainage sump, and this lowland now serves as a collection area for runoff from the neighboring property to the east.

3.4 BUILDING SURVEY PROCEDURES

Two indoor radon measurements were taken using the Tedlar bag technique. Using this method, radon measurements are obtained by pumping air into a Tedlar bag at a rate of approximately 2 1/min and transferring the air sample directly into a scintillation cell with an interior coating of zinc sulfide and an end window for viewing the scintillations. Analysis of the sample was simplified by allowing the radon decay products to build up over time. This method allows all the radon decay products to come into secular equilibrium with the radon. The scintillation cell was placed in contact with a photomultiplier tube, and the scintillations were counted using standard nuclear counting instrumentation. Indoor radon measurement results, using this method, ranged from less than 0.2 to 0.8 pCi/l. These concentrations fall within the range typical of those from background indoor radon measurements.

Four indoor air samples were collected to determine working levels (WL) of radon and thoron daughters. Measurement of radon daughters was done by collecting an air sample for exactly 5 min through a 0.45-micron membrane filter at a rate of 11 liters/min for a total sample volume of 55 liters. Alpha-particle activity on the filter paper was counted 40 to 90 min after sampling using an alpha

scintillation detector coupled to a count-rate meter or a digital scaler. Results of measurements for radon daughters ranged from 0.0006 to 0.001 WL and were substantially less than the applicable generic guideline (40 CFR 192) (Ref. 6) of an annual average (or equivalent) radon decay product concentration not to exceed 0.02 WL (Table 3-1). Measurements for thoron daughters were conducted using the same method as for radon daughters with the exception of the time delay between collection of the air sample and counting of the alpha-particle activity. In the case of thoron daughters, the sample is allowed to age for at least 5 hours after sampling before it is counted. This elapsed time allows radon daughters, which may be present with the thoron daughters, to decay sufficiently so as not to interfere with computation of the working levels for thoron daughters. Results of measurements for thoron daughters ranged from less than the lower limit of detection to 0.003 WL. The generic guideline is more restrictive for radon-222 (radon) than for radon-220 (thoron) according to NCRP Report No. 50 (Ref. 7), which was used as the guideline for thoron daughter measurements.

In addition, exposure rate measurements were taken inside the NJVIS building to determine the potential health risk for employees in the event that contamination might be present beneath the building. These measurements are taken 3 ft above the floor using either a SPA-3 or a pressurized ionization chamber (PIC). The latter instrument has a response to gamma radiation that is proportional to exposure in roentgens. A conversion factor for SPA-3 measurements was established through a correlation of measurements taken at four locations in the vicinity of the NJVIS property with these two instruments. The unshielded SPA-3 readings were then used to estimate gamma exposure rates for each location. Locations of these measurements (Figure 3-7) were determined to be representative of the entire building interior. Gamma radiation exposure rate measurements ranged from 4 $\mu\,R/h$ to 5 $\mu\,R/h$, giving an average of 4 uR/h, including background. These measurements are considered within the normal variation of background radiation. These results can be found in Table 3-4.

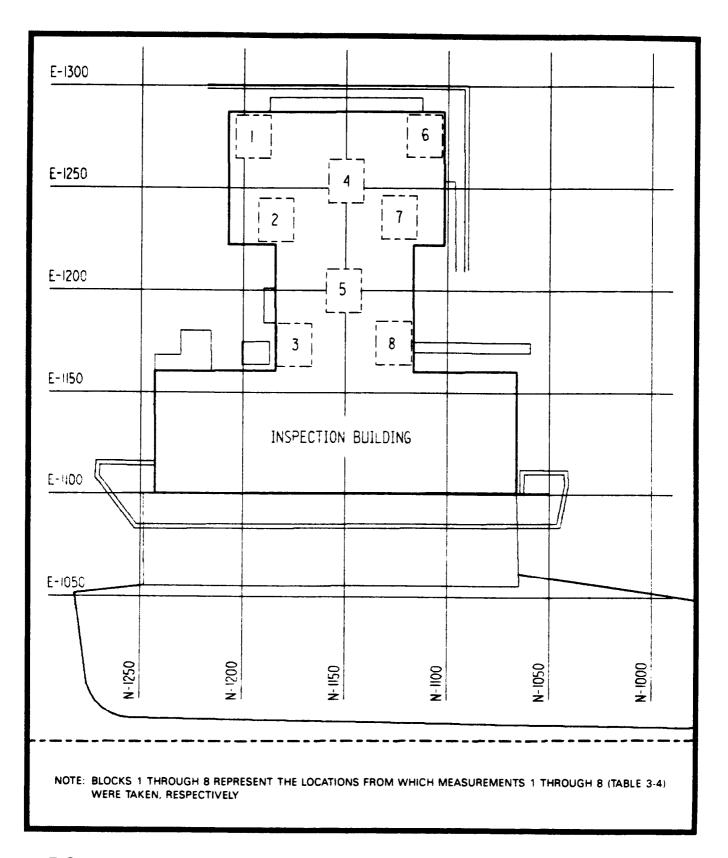


FIGURE 3-7 EXPOSURE RATE MEASUREMENT LOCATIONS AT THE NEW JERSEY VEHICLE INSPECTION STATION PROPERTY

SUMMARY OF RESIDUAL CONTAMINATION GUIDELINES FOR THE MAYWOOD SITE

Page 1 of 2

BASIC DOSE LIMITS

The basic limit for the annual radiation dose received by an individual member of the general public is 100 mrem/yr.

SOIL (LAND) GUIDELINES (MAXIMUM LIMITS FOR UNRESTRICTED USE)

Radionuclide	Soil Concentration (pCi/g) above background ^{a,b,c}
Radium-226 Radium-228 Thorium-230 Thorium-232	5 pCi/g, averaged over the first 15 cm of soil below the surface; 15 pCi/g when averaged over any 15-cm- thick soil layer below the surface layer.
Other radionuclides	Soil guidelines will be calculated on a site-specific basis using the DOE manual developed for this use.

STRUCTURE GUIDELINES (MAXIMUM LIMITS FOR UNRESTRICTED USE)

Airborne Radon Decay Products

Generic guidelines for concentrations of airborne radon decay products shall apply to existing occupied or habitable structures on private property that are intended for unrestricted use; structures that will be demolished or buried are excluded. The applicable generic guideline (40 CFR 192) is: In any occupied or habitable building, the objective of remedial action shall be, and reasonable effort shall be made to achieve, an annual average (or equivalent) radon decay product concentration (including background) not to exceed 0.02 WL.^d In any case, the radon decay product concentration (including background) shall not exceed 0.03 WL. Remedial actions are not required in order to comply with this guideline when there is reasonable assurance that residual radioactive materials are not the cause.

External Gamma Radiation

The average level of gamma radiation inside a building or habitable structure on a site to be released for unrestricted use shall not exceed the background level by more than 20 μ R/h.

Indoor/Outdoor Structure Surface Contamination

	Allowable Residual Surface Contamination ^e (dpm/100 cm ²)		ntamination ^e
Radionuclidef	<u>Average</u> g,h	<u>Maximum</u> h,i	<u>Removable</u> h,j
Transuranics, Ra-226, Ra-228, Th-230, Th-228 Pa-231, Ac-227, I-125, I-129	100	300	20
Th -Natural, Th-232, Sr-90, Ra-223, Ra-224 U-232, I-126, I-131, I-133	1,000	3,000	200

Page 2 of 2

Indoor/Outdoor Structure Surface Contamination (continued)

		idual Surface Cont (dpm/100 cm ²)	amination ^e
<u>Radionuclide</u> ^f	Average ^{g, h}	<u>Maximum</u> h,i	<u>Removable^{h,j}</u>
U-Natural, U-235, U-238, and associated decay products	5,000 a	15,000 œ	1,000 a
Beta-gamma emitters (radionuclides with decay modes other than alpha emission or spontaneous fission) except Sr-90 and others noted above	5,000 β - γ	15,000 β - γ	1 ,000 β-γ

^aThese guidelines take into account ingrowth of radium-226 from thorium-230 and of radium-228 from thorium-232, and assume secular equilibrium. If either thorium-230 and radium-226 or thorium-232 and radium-228 are both present, not in secular equilibrium, the guidelines apply to the higher concentration. If other mixtures of radionuclides occur, the concentrations of individual radionuclides shall be reduced so that the dose for the mixtures will not exceed the basic dose limit.

^bThese guidelines represent unrestricted-use residual concentrations above background averaged across any 15-cm-thick layer to any depth and over any contiguous 100-m² surface area.

^CLocalized concentrations in excess of these limits are allowable provided that the average concentration over a $100-m^2$ area does not exceed these limits.

^dA working level (WL) is any combination of short-lived radon decay products in 1 liter of air that will result in the ultimate emission of 1.3×10^5 MeV of potential alpha energy.

^eAs used in this table, dpm (disintegrations per minute) means the rate of emission by radioactive material as determined by correcting the counts per minute observed by an appropriate detector for background, efficiency, and geometric factors associated with the instrumentation.

[†]Where surface contamination by both alpha- and beta-gamma-emitting radionuclides exists, the limits established for alpha- and beta-gamma-emitting radionuclides should apply independently.

⁹Measurements of average contamination should not be averaged over more than 1 m^2 . For objects of less surface area, the average shall be derived for each such object.

^hThe average and maximum radiation levels associated with surface contamination resulting from beta-gamma emitters should not exceed 0.2 mrad/h and 1.0 mrad/h, respectively, at 1 cm.

¹The maximum contamination level applies to an area of not more than 100 cm^2 .

^jThe amount of removable radioactive material per 100 cm² of surface area should be determined by wiping that area with dry filter or soft absorbent paper, applying moderate pressure, and measuring the amount of radioactive material on the wipe with an appropriate instrument of known efficiency. When removable contamination on objects of surface area less than 100 cm² is determined, the activity per unit area should be based on the actual area and the entire surface should be wiped. The numbers in this column are maximum amounts.

SURFACE SOIL SAMPLING RESULTS

FOR THE NEW JERSEY VEHICLE INSPECTION STATION PROPERTY

Page 1 of 2

Bio20Ni020 $\langle 6.0$ $\langle 0.7$ 1.7 ± 0.4 Bi020Ni220 $\langle 5.6$ $\langle 1.2$ $\langle 2.9$ Bi020Ni220 $\langle 5.6$ $\langle 1.0$ $\langle 3.0$ Bi020Ni220 $\langle 5.6$ 0.8 ± 0.2 $\langle 2.3$ Bi020Ni520 $\langle 6.4$ 0.6 ± 0.4 2.8 ± 0.6 Bi020Ni520 $\langle 6.4$ 0.6 ± 0.4 2.8 ± 0.6 Bi020Ni520 $\langle 6.4$ 0.6 ± 0.4 2.8 ± 0.6 Bi020Ni520 $\langle 6.4$ 0.6 ± 0.4 2.8 ± 0.6 Bi020Ni820 $\langle 9.6$ $\langle 1.2$ 9.2 ± 1.7 Bi020Ni820 $\langle 7.3$ 0.5 ± 0.1 4.4 ± 0.6 Bi040Ni620 $\langle 6.9$ $\langle 1.8$ $\langle 3.1$ Bi065Ni670 $\langle 6.9$ 1.0 ± 0.6 2.1 ± 0.2 Bi1080Ni875 $\langle 6.9$ 0.6 ± 0.4 4.9 ± 0.4 Bi125Ni795 $\langle 8.0$ 0.7 ± 0.1 6.2 ± 1.1 Bi140Ni660 $\langle 8.1$ 0.9 ± 0.4 4.6 ± 1.2 Bi140Ni680 $\langle 9.2$ 1.0 ± 0.2 12.5 ± 2.3 Bi160Ni910 $\langle 8.3$ $\langle 1.5$ 7.6 ± 1.3 Bi165Ni470 $\langle 9.3$ $\langle 1.1$ 1.2 ± 0.5 Bi120Ni340 $\langle 5.1$ $\langle 1.1$ $\langle 2.4$ Bi1210Ni755 $\langle 8.7$ 1.2 ± 0.1 11.2 ± 2.5 Bi220No835 $\langle 9.4$ 0.7 ± 0.1 10.2 ± 4.5 Bi230Ni400 $\langle 5.5$ $\langle 1.6$ $\langle 2.9$ Bi330Ni400 $\langle 5.5$ <th colspan="2"><u>Grid Coordinates</u></th> <th></th> <th colspan="3">Concentrations (pCi/g +/-</th>	<u>Grid Coordinates</u>			Concentrations (pCi/g +/-		
B1020N1120 $\langle 5.1$ 1.0 ± 0.4 1.6 ± 0.5 B1020N1220 $\langle 5.6$ $\langle 1.2$ $\langle 2.9$ B1020N1320 $\langle 4.9$ $\langle 1.0$ $\langle 3.0$ B1020N1420 $\langle 5.6$ 0.8 ± 0.2 $\langle 2.3$ B1020N1520 $\langle 6.4$ 0.6 ± 0.4 2.8 ± 0.6 B1020N1820 $\langle 9.6$ $\langle 1.2$ 9.2 1.1 ± 1.1 B1020N1820 $\langle 9.6$ $\langle 1.2$ 9.2 ± 1.7 B1020N1820 $\langle 9.6$ $\langle 1.2$ 9.2 ± 1.7 B1020N1820 $\langle 7.3$ 0.5 ± 0.1 4.4 ± 0.6 B1045N1670 $\langle 6.9$ 1.0 ± 0.6 2.1 ± 0.2 B1080N1875 $\langle 6.9$ 0.6 ± 0.4 4.9 ± 0.4 B1140N1560 $\langle 8.1$ 0.9 ± 0.4 4.6 ± 1.2 B1140N1560 $\langle 8.1$ 0.9 ± 0.4 4.6 ± 1.2 B1140N1820 $\langle 8.2$ 0.6 ± 0.5 5.4 ± 3.3 B1160N1910 $\langle 8.3$ $\langle 1.5$ 7.6 ± 1.3 B1160N1910 $\langle 8.3$ $\langle 1.2$ 3.3 ± 0.6 B1170N1605 $\langle 13.8$ 1.5 ± 0.3 11.5 ± 0.5 B1210N1470 $\langle 7.6$ $\langle 1.2$ 4.1 ± 1.1 B1240N1755 $\langle 8.7$ 1.2 4.1 ± 1.1 B1240N1755 $\langle 8.1$ $\langle 1.1$ 1.4 ± 7.2 B1333N140 $\langle 9.3$ $\langle 1.1$ 1.4 ± 7.2 B1330N1430 $\langle 5.5$ $\langle 1.6$ $\langle 2.9$ B1330N1430 $\langle 5.5$	E, W	N,S	Uranium-238	Radium-226	Thorium-232	
B1020N1220 < 5.6 < 1.2 < 2.9 B1020N1320 < 4.9 < 1.0 < 3.0 B1020N1320 < 4.9 < 1.0 < 3.0 B1020N1520 < 6.4 0.6 ± 0.4 2.8 ± 0.5 B1020N1520 < 6.4 0.6 ± 0.4 2.8 ± 0.5 B1020N1820 < 7.3 0.5 ± 0.1 4.4 ± 0.6 B1020N1820 < 7.3 0.5 ± 0.1 4.4 ± 0.5 B1020N1820 < 7.3 0.5 ± 0.1 4.4 ± 0.5 B1040N1620 < 6.9 1.0 ± 0.6 2.1 ± 0.2 B1080N1875 < 6.9 0.6 ± 0.4 4.9 ± 0.4 B1125N1795 < 8.0 0.7 ± 0.1 6.2 ± 1.1 B1140N1660 < 8.1 0.9 ± 0.4 4.6 ± 1.2 B1140N1680 < 9.2 1.0 ± 0.2 12.5 ± 2.2 B1140N1680 < 9.2 1.0 ± 0.2 12.5 ± 2.2 B1140N1680 < 9.2 1.0 ± 0.3 11.5 ± 0.5 B1165N1470 < 9.3 < 1.2 3.3 ± 0.6 B1210N1755 < 8.7 1.2 ± 0.1 11.2 ± 2.9 B1220N0835 < 9.4 0.7 ± 0.1 11.2 ± 2.9 B1230N1470 < 7.6 < 1.2 4.1 ± 1.1 B1240N0775 < 4.5 0.5 ± 0.1 0.8 ± 0.6 B1315N1830 < 10.0 1.0 ± 0.1 $9.4 < 2.1$ B1333N1560 < 5.5 $< 1.6 \pm 0.4$ < 2.9 B1333<		N1020	<6.0	<0.7	1.7 + 0.4	
B1020N1320 $\langle 4.9 \rangle$ $\langle 1.0 \rangle$ $\langle 3.0 \rangle$ B1020N1420 $\langle 5.6 \rangle$ $0.8 \pm 0.2 \rangle$ $\langle 2.3 \rangle$ B1020N1520 $\langle 6.4 \rangle$ $0.6 \pm 0.4 \rangle$ $2.8 \pm 0.5 \rangle$ B1020N1720 $\langle 10.2 \rangle$ $0.9 \pm 0.3 \rangle$ $7.1 \pm 1.1 \rangle$ B1020N1820 $\langle 9.6 \rangle$ $\langle 1.2 \rangle$ $9.2 \pm 1.7 \rangle$ B1020N1820 $\langle 7.3 \rangle$ $0.5 \pm 0.1 \rangle$ $4.4 \pm 0.6 \rangle$ B1040N1620 $\langle 6.9 \rangle$ $\langle 1.8 \rangle$ $\langle 3.1 \rangle$ B1065N1670 $\langle 6.9 \rangle$ $1.0 \pm 0.6 \rangle$ $2.1 \pm 0.2 \rangle$ B1080N1875 $\langle 6.9 \rangle$ $0.6 \pm 0.4 \rangle$ $4.9 \pm 0.4 \rangle$ B1125N1795 $\langle 8.0 \rangle$ $0.7 \pm 0.1 \rangle$ $6.2 \pm 1.1 \rangle$ B1140N1660 $\langle 8.1 \rangle$ $0.9 \pm 0.4 \rangle$ $4.6 \pm 1.2 \rangle$ B1140N1680 $\langle 9.2 \rangle$ $1.0 \pm 0.2 \rangle$ $12.5 \pm 2.3 \rangle$ B1160N1910 $\langle 8.3 \rangle$ $\langle 1.5 \rangle$ $7.6 \pm 1.3 \rangle$ B1160N1910 $\langle 8.3 \rangle$ $\langle 1.2 \rangle$ $3.3 \pm 0.6 \rangle$ B1210N1755 $\langle 8.7 \rangle$ $1.2 \pm 0.1 \rangle$ $11.2 \pm 2.9 \rangle$ B1210N1755 $\langle 8.7 \rangle$ $1.2 \pm 0.1 \rangle$ $11.2 \pm 2.9 \rangle$ B1220N0835 $\langle 9.4 \rangle$ $0.7 \pm 0.1 \rangle$ $8.9 \wedge 0.3 \rangle$ B1220N0835 $\langle 9.4 \rangle$ $0.7 \pm 0.1 \rangle$ $0.9 \pm 0.4 \rangle$ B1230N1470 $\langle 7.6 \rangle$ $\langle 1.2 \rangle$ $4.1 \pm 1.1 \rangle$ B1240N0775 $\langle 4.5 \rangle$ $0.5 \pm 0.1 \rangle$ $0.8 \pm 0.3 \rangle$ B1333N1340 $\langle 4.9 \rangle$ $1.6 \pm 0.4 \rangle$ $\langle 2.9 \rangle$ <td></td> <td></td> <td></td> <td></td> <td>1.6 ± 0.5</td>					1.6 ± 0.5	
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B1020N1820 $\langle 7.3 \\ 6.9 \end{pmatrix}$ (0.5 ± 0.1) $4.4 \pm 0.6 \\ 3.1 \end{pmatrix}$ B1065N1670 $\langle 6.9 \end{pmatrix}$ $(1.8 \\ 0.6 \end{pmatrix}$ $\langle 3.1 \\ 1.8 \end{pmatrix}$ B1080N1875 $\langle 6.9 \end{pmatrix}$ $1.0 \pm 0.6 \\ 2.1 \pm 0.2 \\ 1.9 \end{bmatrix}$ B1125N1795 $\langle 8.0 \end{pmatrix}$ $0.7 \pm 0.1 \\ 6.2 \pm 1.1 \end{bmatrix}$ B1140N1560 $\langle 8.1 \rangle$ $0.9 \pm 0.4 \\ 4.6 \pm 1.2 \\ 1.140 \end{pmatrix}$ B1140N1680 $\langle 9.2 \rangle$ $1.0 \pm 0.2 \\ 1.2 5 \pm 2.3 \\ 1.140 \end{pmatrix}$ B1160N1910 $\langle 8.3 \rangle$ $\langle 1.5 \rangle$ B1165N1470 $\langle 9.3 \rangle$ $\langle 1.2 \rangle$ B1165N1470 $\langle 9.3 \rangle$ $\langle 1.2 \rangle$ B1210N1755 $\langle 8.7 \rangle$ $1.2 \pm 0.1 \rangle$ B1220N0835 $\langle 9.4 \rangle$ $0.7 \pm 0.1 \rangle$ B1220N0835 $\langle 9.4 \rangle$ $0.7 \pm 0.1 \rangle$ B1220N0835 $\langle 9.4 \rangle$ $0.7 \pm 0.1 \rangle$ B1220N1470 $\langle 7.6 \rangle$ $\langle 1.1 \rangle$ B1240N0775 $\langle 4.5 \rangle$ $0.5 \pm 0.1 \rangle$ B1280N1470 $\langle 7.6 \rangle$ $\langle 1.1 \rangle$ B1315N1830 $\langle 10.0 \rangle$ $1.0 \pm 0.1 \rangle$ B1315N1830 $\langle 10.0 \rangle$ $1.0 \pm 0.1 \rangle$ B1333N1340 $\langle 4.9 \rangle$ $1.6 \pm 0.4 \rangle$ B1333N1430 $\langle 5.5 \rangle$ $0.6 \pm 0.3 \rangle$ B1350N0710 $\langle 7.7 \rangle$ $0.7 \pm 0.5 \rangle$ B1370N0695 $\langle 5.6 \rangle$ $0.9 \pm 0.2 \rangle$ B1380N1470 $\langle 6.3 \rangle$ $0.8 \pm 0.1 \rangle$ B1380N1470 $\langle 6.3 \rangle$ $0.8 \pm 0.4 \rangle$ B1380N1615 <						
B1040N1620 $\langle 6.9 \rangle$ $\langle 1.8 \rangle$ $\langle 3.1 \rangle$ B1065N1670 $\langle 6.9 \rangle$ $1.0 \pm 0.6 \rangle$ $2.1 \pm 0.2 \rangle$ B1080N1875 $\langle 6.9 \rangle$ $0.6 \pm 0.4 \rangle$ $4.9 \pm 0.4 \rangle$ B1125N1795 $\langle 8.0 \rangle$ $0.7 \pm 0.1 \rangle$ $6.2 \pm 1.1 \rangle$ B1140N1560 $\langle 8.1 \rangle$ $0.9 \pm 0.4 \rangle$ $4.6 \pm 1.2 \rangle$ B1140N1680 $\langle 9.2 \rangle$ $1.0 \pm 0.2 \rangle$ $12.5 \pm 2.3 \rangle$ B1140N1820 $\langle 8.3 \rangle$ $\langle 1.5 \rangle$ $7.6 \pm 1.3 \rangle$ B1160N1910 $\langle 8.3 \rangle$ $\langle 1.5 \rangle$ $7.6 \pm 1.3 \rangle$ B1165N1470 $\langle 9.3 \rangle$ $\langle 1.1 \rangle$ $2.3 3 \pm 0.6 \rangle$ B1210N1605 $\langle 13.8 \rangle$ $1.5 \pm 0.3 \rangle$ $11.5 \pm 0.5 \rangle$ B1210N1340 $\langle 5.1 \rangle$ $\langle 1.1 \rangle$ $\langle 2.4 \rangle$ B1220N0835 $\langle 9.4 \rangle$ $0.7 \pm 0.1 \rangle$ $11.2 \pm 2.9 \rangle$ B1230N1470 $\langle 7.6 \rangle$ $\langle 1.2 \rangle$ $4.1 \pm 1.1 \rangle$ B1240N0775 $\langle 4.5 \rangle$ $0.5 \pm 0.1 \rangle$ $0.8 \pm 0.6 \rangle$ B1315N1830 $\langle 10.0 \rangle$ $1.0 \pm 0.1 \rangle$ $9.0 \pm 0.6 \rangle$ B1330N1425 $\langle 8.1 \rangle$ $\langle 1.1 \rangle$ $4.7 \pm 0.5 \rangle$ B1333N1560 $\langle 5.9 \rangle$ $0.6 \pm 0.4 \rangle$ $\langle 2.1 \rangle$ B1370N0695 $\langle 5.6 \rangle$ $0.9 \pm 0.2 \rangle$ $1.2 \pm 0.7 \rangle$ B1370N0695 $\langle 5.7 \rangle$ $0.8 \pm 0.1 \rangle$ $1.5 \pm 1.7 \rangle$ B1380N1470 $\langle 6.3 \rangle$ $0.8 \pm 0.4 \rangle$ $1.1 \pm 0.6 \rangle$ B1380N1615 $\langle 12.3 \rangle$ $0.7 \pm 0.1 \rangle$ $1.9 \pm 0.7 \rangle$						
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E1230N1470 <7.6 <1.2 4.1 ± 1.1 E1240N0775 <4.5 0.5 ± 0.1 0.8 ± 0.6 E1265N1840 <9.3 <1.1 11.4 ± 2.2 E1270N1830 <10.0 1.0 ± 0.1 9.0 ± 0.8 E1280N1425 <8.1 <1.1 4.7 ± 0.8 E1315N1835 <6.3 0.8 ± 0.5 2.5 ± 0.4 E1330N1430 <5.5 <1.6 <2.9 E1333N1340 <4.9 1.6 ± 0.4 <2.1 E1333N1560 <5.9 0.6 ± 0.3 <3.3 E1365N0710 <7.7 0.7 ± 0.1 5.0 ± 1.3 E1365N0730 <14.3 1.7 ± 0.5 10.1 ± 2.2 E1370N0695 <5.6 0.9 ± 0.2 1.2 ± 0.7 E1370N0825 <4.9 1.0 ± 0.6 1.1 ± 0.4 E1380N1470 <6.3 0.8 ± 0.1 7.5 ± 1.7 E1380N1470 <6.3 0.8 ± 0.4 1.1 ± 0.6 E1380N1615 <12.3 0.7 ± 0.1 7.0 ± 0.5 E1420N0960 <7.0 1.0 ± 0.1 1.9 ± 0.7 E1430N1725 <9.2 <1.4 8.0 ± 1.2						
E1240N0775 $\langle 4.5$ 0.5 ± 0.1 0.8 ± 0.6 E1265N1840 $\langle 9.3$ $\langle 1.1$ 11.4 ± 2.2 E1270N1830 $\langle 10.0$ 1.0 ± 0.1 9.0 ± 0.8 E1280N1425 $\langle 8.1$ $\langle 1.1$ 4.7 ± 0.8 E1315N1835 $\langle 6.3$ 0.8 ± 0.5 2.5 ± 0.4 E1330N1430 $\langle 5.5$ $\langle 1.6$ $\langle 2.9$ E1333N1340 $\langle 4.9$ 1.6 ± 0.4 $\langle 2.1$ E1333N1560 $\langle 5.9$ 0.6 ± 0.3 $\langle 3.3$ E1365N0710 $\langle 7.7$ 0.7 ± 0.1 5.0 ± 1.3 E1365N0730 $\langle 14.3$ 1.7 ± 0.5 10.1 ± 2.2 E1370N0695 $\langle 5.6$ 0.9 ± 0.2 1.2 ± 0.7 E1370N0825 $\langle 4.9$ 1.0 ± 0.6 1.1 ± 0.4 E1370N0720 $\langle 9.9$ 1.4 ± 0.4 7.5 ± 1.7 E1380N1470 $\langle 6.3$ 0.8 ± 0.4 1.1 ± 0.6 E1380N1615 $\langle 12.3$ 0.7 ± 0.1 7.0 ± 0.5 E1420N0960 $\langle 7.0$ 1.0 ± 0.1 1.9 ± 0.7 E1430N1725 $\langle 9.2$ $\langle 1.4$ 8.0 ± 1.2				0.7 ± 0.1	3.5 ± 0.3	
B1265N1840 $\langle 9.3$ $\langle 1.1$ 11.4 ± 2.2 B1270N1830 $\langle 10.0$ 1.0 ± 0.1 9.0 ± 0.8 B1280N1425 $\langle 8.1$ $\langle 1.1$ 4.7 ± 0.8 B1315N1835 $\langle 6.3$ 0.8 ± 0.5 2.5 ± 0.4 B1330N1430 $\langle 5.5$ $\langle 1.6$ $\langle 2.9$ B1333N1340 $\langle 4.9$ 1.6 ± 0.4 $\langle 2.1$ B1333N1560 $\langle 5.9$ 0.6 ± 0.3 $\langle 3.3$ B1350N0710 $\langle 7.7$ 0.7 ± 0.1 5.0 ± 1.3 B1365N0730 $\langle 14.3$ 1.7 ± 0.5 10.1 ± 2.2 B1370N0825 $\langle 4.9$ 1.0 ± 0.6 1.1 ± 0.4 B1370N1735 $\langle 6.3$ 0.8 ± 0.1 7.5 ± 1.7 B1370N1735 $\langle 6.3$ 0.8 ± 0.3 1.8 ± 0.1 B1380N1470 $\langle 6.3$ 0.8 ± 0.4 1.1 ± 0.6 B1380N1540 $\langle 5.7$ 0.8 ± 0.4 1.1 ± 0.6 B1380N1615 $\langle 12.3$ 0.7 ± 0.1 7.0 ± 0.5 B1420N0960 $\langle 7.0$ 1.0 ± 0.1 1.9 ± 0.7 B1430N1725 $\langle 9.2$ $\langle 1.4$ 8.0 ± 1.2					4.1 ± 1.1	
E1270N1830 < 10.0 1.0 ± 0.1 9.0 ± 0.8 E1280N1425 < 8.1 < 1.1 4.7 ± 0.8 E1315N1835 < 6.3 0.8 ± 0.5 2.5 ± 0.4 E1330N1430 < 5.5 < 1.6 < 2.9 E1333N1340 < 4.9 1.6 ± 0.4 < 2.1 E1333N1560 < 5.9 0.6 ± 0.3 < 3.3 E1350N0710 < 7.7 0.7 ± 0.1 5.0 ± 1.3 E1365N0730 < 14.3 1.7 ± 0.5 10.1 ± 2.2 E1370N0695 < 5.6 0.9 ± 0.2 1.2 ± 0.7 E1370N0825 < 4.9 1.0 ± 0.6 1.1 ± 0.4 E1370N1735 < 6.3 0.8 ± 0.1 7.5 ± 1.7 E1370N1735 < 6.3 0.8 ± 0.1 7.5 ± 0.8 E1380N1470 < 6.3 0.8 ± 0.4 1.1 ± 0.6 E1380N1540 < 5.7 0.8 ± 0.4 1.1 ± 0.6 E1380N1615 < 12.3 0.7 ± 0.1 7.0 ± 0.5 E1420N0960 < 7.0 1.0 ± 0.1 1.9 ± 0.7 E1430N1725 < 9.2 < 1.4 8.0 ± 1.2					0.0 ± 0.0	
E1280N1425 $\langle 8.1$ $\langle 1.1$ 4.7 ± 0.8 E1315N1835 $\langle 6.3$ 0.8 ± 0.5 2.5 ± 0.4 E1330N1430 $\langle 5.5$ $\langle 1.6$ $\langle 2.9$ E1333N1340 $\langle 4.9$ 1.6 ± 0.4 $\langle 2.1$ E1333N1560 $\langle 5.9$ 0.6 ± 0.3 $\langle 3.3$ E1365N0710 $\langle 7.7$ 0.7 ± 0.1 5.0 ± 1.3 E1365N0730 $\langle 14.3$ 1.7 ± 0.5 10.1 ± 2.2 E1370N0695 $\langle 5.6$ 0.9 ± 0.2 1.2 ± 0.7 E1370N0825 $\langle 4.9$ 1.0 ± 0.6 1.1 ± 0.4 E1370N0720 $\langle 9.9$ 1.4 ± 0.4 7.5 ± 1.7 E1375N0720 $\langle 9.9$ 1.4 ± 0.4 7.5 ± 0.8 E1380N1470 $\langle 6.3$ 0.8 ± 0.3 1.8 ± 0.1 E1380N1615 $\langle 12.3$ 0.7 ± 0.1 7.0 ± 0.5 E1420N0960 $\langle 7.0$ 1.0 ± 0.1 1.9 ± 0.7 E1430N1725 $\langle 9.2$ $\langle 1.4$ 8.0 ± 1.2						
E1315N1835 $\langle 6.3$ 0.8 ± 0.5 2.5 ± 0.4 E1330N1430 $\langle 5.5$ $\langle 1.6$ $\langle 2.9$ E1333N1340 $\langle 4.9$ 1.6 ± 0.4 $\langle 2.1$ E1333N1560 $\langle 5.9$ 0.6 ± 0.3 $\langle 3.3$ E1350N0710 $\langle 7.7$ 0.7 ± 0.1 5.0 ± 1.3 E1365N0730 $\langle 14.3$ 1.7 ± 0.5 10.1 ± 2.2 E1370N0695 $\langle 5.6$ 0.9 ± 0.2 1.2 ± 0.7 E1370N0825 $\langle 4.9$ 1.0 ± 0.6 1.1 ± 0.4 E1370N0720 $\langle 9.9$ 1.4 ± 0.4 7.5 ± 1.7 E1375N0720 $\langle 9.9$ 1.4 ± 0.4 7.5 ± 0.8 E1380N1540 $\langle 5.7$ 0.8 ± 0.4 1.1 ± 0.6 E1380N1615 $\langle 12.3$ 0.7 ± 0.1 7.0 ± 0.5 E1420N0960 $\langle 7.0$ 1.0 ± 0.1 1.9 ± 0.7 E1430N1725 $\langle 9.2$ $\langle 1.4$ 8.0 ± 1.2						
E1330N1430 < 5.5 < 1.6 < 2.9 E1333N1340 < 4.9 1.6 ± 0.4 < 2.1 E1333N1560 < 5.9 0.6 ± 0.3 < 3.3 E1350N0710 < 7.7 0.7 ± 0.1 5.0 ± 1.3 E1365N0730 < 14.3 1.7 ± 0.5 10.1 ± 2.2 E1370N0695 < 5.6 0.9 ± 0.2 1.2 ± 0.7 E1370N0825 < 4.9 1.0 ± 0.6 1.1 ± 0.4 E1370N0720 < 9.9 1.4 ± 0.4 7.5 ± 1.7 E1375N0720 < 9.9 1.4 ± 0.4 7.5 ± 0.8 E1380N1470 < 6.3 0.8 ± 0.4 1.1 ± 0.6 E1380N1615 < 12.3 0.7 ± 0.1 7.0 ± 0.5 E1420N0960 < 7.0 1.0 ± 0.1 1.9 ± 0.7 E1430N1725 < 9.2 < 1.4 8.0 ± 1.2						
E1333N1340 $\langle 4.9$ 1.6 ± 0.4 $\langle 2.1$ E1333N1560 $\langle 5.9$ 0.6 ± 0.3 $\langle 3.3$ E1350N0710 $\langle 7.7$ 0.7 ± 0.1 5.0 ± 1.3 E1365N0730 $\langle 14.3$ 1.7 ± 0.5 10.1 ± 2.2 E1370N0695 $\langle 5.6$ 0.9 ± 0.2 1.2 ± 0.7 E1370N0825 $\langle 4.9$ 1.0 ± 0.6 1.1 ± 0.4 E1370N1735 $\langle 6.3$ 0.8 ± 0.1 7.5 ± 1.7 E1375N0720 $\langle 9.9$ 1.4 ± 0.4 7.5 ± 0.8 E1380N1470 $\langle 6.3$ 0.8 ± 0.3 1.8 ± 0.1 E1380N1615 $\langle 12.3$ 0.7 ± 0.1 7.0 ± 0.5 E1420N0960 $\langle 7.0$ 1.0 ± 0.1 1.9 ± 0.7 E1430N1725 $\langle 9.2$ $\langle 1.4$ 8.0 ± 1.2						
E1333N1560 $\langle 5.9 \rangle$ 0.6 ± 0.3 $\langle 3.3 \rangle$ E1350N0710 $\langle 7.7 \rangle$ 0.7 ± 0.1 $5.0 \pm 1.3 \rangle$ E1365N0730 $\langle 14.3 \rangle$ $1.7 \pm 0.5 \rangle$ $10.1 \pm 2.2 \rangle$ E1370N0695 $\langle 5.6 \rangle$ $0.9 \pm 0.2 \rangle$ $1.2 \pm 0.7 \rangle$ E1370N0825 $\langle 4.9 \rangle$ $1.0 \pm 0.6 \rangle$ $1.1 \pm 0.4 \rangle$ E1370N1735 $\langle 6.3 \rangle$ $0.8 \pm 0.1 \rangle$ $7.5 \pm 1.7 \rangle$ E1375N0720 $\langle 9.9 \rangle$ $1.4 \pm 0.4 \rangle$ $7.5 \pm 0.8 \rangle$ E1380N1470 $\langle 6.3 \rangle$ $0.8 \pm 0.3 \rangle$ $1.8 \pm 0.1 \rangle$ E1380N1540 $\langle 5.7 \rangle$ $0.8 \pm 0.4 \rangle$ $1.1 \pm 0.6 \rangle$ E1380N1615 $\langle 12.3 \rangle$ $0.7 \pm 0.1 \rangle$ $7.0 \pm 0.5 \rangle$ E1420N0960 $\langle 7.0 \rangle$ $1.0 \pm 0.1 \rangle$ $1.9 \pm 0.7 \rangle$ E1430N1725 $\langle 9.2 \rangle$ $\langle 1.4 \rangle$ $8.0 \pm 1.2 \rangle$						
E 1350N0710 $\langle 7.7 \rangle$ $0.7 \pm 0.1 \rangle$ $5.0 \pm 1.3 \rangle$ E 1365N0730 $\langle 14.3 \rangle$ $1.7 \pm 0.5 \rangle$ $10.1 \pm 2.2 \rangle$ E 1370N0695 $\langle 5.6 \rangle$ $0.9 \pm 0.2 \rangle$ $1.2 \pm 0.7 \rangle$ E 1370N0825 $\langle 4.9 \rangle$ $1.0 \pm 0.6 \rangle$ $1.1 \pm 0.4 \rangle$ E 1370N0735 $\langle 6.3 \rangle$ $0.8 \pm 0.1 \rangle$ $7.5 \pm 1.7 \rangle$ E 1370N1735 $\langle 6.3 \rangle$ $0.8 \pm 0.1 \rangle$ $7.5 \pm 0.8 \rangle$ E 1380N1470 $\langle 6.3 \rangle$ $0.8 \pm 0.4 \rangle$ $1.1 \pm 0.6 \rangle$ E 1380N1615 $\langle 12.3 \rangle$ $0.7 \pm 0.1 \rangle$ $7.0 \pm 0.5 \rangle$ E 1420N0960 $\langle 7.0 \rangle$ $1.0 \pm 0.1 \rangle$ $1.9 \pm 0.7 \rangle$ E 1430N1725 $\langle 9.2 \rangle$ $\langle 1.4 \rangle$ $8.0 \pm 1.2 \rangle$				1.0 + 0.4		
E1365N0730 < 14.3 1.7 ± 0.5 10.1 ± 2.2 E1370N0695 < 5.6 0.9 ± 0.2 1.2 ± 0.7 E1370N0825 < 4.9 1.0 ± 0.6 1.1 ± 0.4 E1370N1735 < 6.3 0.8 ± 0.1 7.5 ± 1.7 E1375N0720 < 9.9 1.4 ± 0.4 7.5 ± 0.8 E1380N1470 < 6.3 0.8 ± 0.4 1.1 ± 0.6 E1380N1615 < 12.3 0.7 ± 0.1 7.0 ± 0.5 E1420N0960 < 7.0 1.0 ± 0.1 1.9 ± 0.7 E1430N1725 < 9.2 < 1.4 8.0 ± 1.2						
B1370N0695 < 5.6 0.9 ± 0.2 1.2 ± 0.7 B1370N0825 < 4.9 1.0 ± 0.6 1.1 ± 0.4 B1370N1735 < 6.3 0.8 ± 0.1 7.5 ± 1.7 B1375N0720 < 9.9 1.4 ± 0.4 7.5 ± 0.8 B1380N1470 < 6.3 0.8 ± 0.3 1.8 ± 0.1 B1380N1540 < 5.7 0.8 ± 0.4 1.1 ± 0.6 B1380N1615 < 12.3 0.7 ± 0.1 7.0 ± 0.5 B1420N0960 < 7.0 1.0 ± 0.1 1.9 ± 0.7 B1430N1725 < 9.2 < 1.4 8.0 ± 1.2						
E1370N0825 $\langle 4.9$ 1.0 ± 0.6 1.1 ± 0.4 B1370N1735 $\langle 6.3$ 0.8 ± 0.1 7.5 ± 1.7 B1375N0720 $\langle 9.9$ 1.4 ± 0.4 7.5 ± 0.8 B1380N1470 $\langle 6.3$ 0.8 ± 0.3 1.8 ± 0.1 B1380N1540 $\langle 5.7$ 0.8 ± 0.4 1.1 ± 0.6 B1380N1615 $\langle 12.3$ 0.7 ± 0.1 7.0 ± 0.5 B1420N0960 $\langle 7.0$ 1.0 ± 0.1 1.9 ± 0.7 B1430N1725 $\langle 9.2$ $\langle 1.4$ 8.0 ± 1.2				1.7 + 0.3	10.1 + 2.2	
B1370N1735 < 6.3 0.8 ± 0.1 7.5 ± 1.7 B1375N0720 < 9.9 1.4 ± 0.4 7.5 ± 0.8 B1380N1470 < 6.3 0.8 ± 0.3 1.8 ± 0.1 B1380N1540 < 5.7 0.8 ± 0.4 1.1 ± 0.6 B1380N1615 < 12.3 0.7 ± 0.1 7.0 ± 0.5 B1420N0960 < 7.0 1.0 ± 0.1 1.9 ± 0.7 B1430N1725 < 9.2 < 1.4 8.0 ± 1.2					1.2 + 0.7	
E1375N0720 $\langle 9.9$ 1.4 ± 0.4 7.5 ± 0.8 E1380N1470 $\langle 6.3$ 0.8 ± 0.3 1.8 ± 0.1 E1380N1540 $\langle 5.7$ 0.8 ± 0.4 1.1 ± 0.6 E1380N1615 $\langle 12.3$ 0.7 ± 0.1 7.0 ± 0.5 E1420N0960 $\langle 7.0$ 1.0 ± 0.1 1.9 ± 0.7 E1430N1725 $\langle 9.2$ $\langle 1.4$ 8.0 ± 1.2					1.1 + 0.4 7 5 + 1 7	
B1380N1470 < 6.3 0.8 ± 0.3 1.8 ± 0.1 B1380N1540 < 5.7 0.8 ± 0.4 1.1 ± 0.6 B1380N1615 < 12.3 0.7 ± 0.1 7.0 ± 0.5 B1420N0960 < 7.0 1.0 ± 0.1 1.9 ± 0.7 B1430N1725 < 9.2 < 1.4 8.0 ± 1.2				1.4 + 0.4		
E1380 N1540 $\langle 5.7 \rangle$ 0.8 ± 0.4 1.1 ± 0.6 E1380 N1615 $\langle 12.3 \rangle$ 0.7 ± 0.1 7.0 ± 0.5 E1420 N0960 $\langle 7.0 \rangle$ 1.0 ± 0.1 1.9 ± 0.7 E1430 N1725 $\langle 9.2 \rangle$ $\langle 1.4 \rangle$ 8.0 ± 1.2				0.8 + 0.3		
E1380N1615<12.3 0.7 ± 0.1 7.0 ± 0.5 E1420N0960<7.0 1.0 ± 0.1 1.9 ± 0.7 E1430N1725<9.2<1.4 8.0 ± 1.2				0.8 + 0.4		
E1420N0960 <7.0 1.0 ± 0.1 1.9 ± 0.7 E1430N1725 <9.2 <1.4 8.0 ± 1.2						
E1430 N1725 $\langle 9.2 \rangle$ $\langle 1.4 \rangle$ 8.0 \pm 1.2					1.9 + 0.7	
1.0 + 0.2 + 0.4 + 0.2	E1480	N0725	<12.1	1.0 ± 0.2	5.9 ± 2.7	

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Grid Coordinates		Concentrations (pCi/g +/- 2 sigma)			
B,W	N,S	Uranium-238	Radiu∎-226	Thorium-232	
E1490	N1020	<4.9	0.8 + 0.1	1.7 <u>+</u> 0.1	
E1490	N1270	<4.6	0.6 + 0.2	<2.4	
E1490	N1470	<5.4	0.7 + 0.4	2.3 ± 0.5	
E1490	N1670	<7.0	0.8 + 0.3	3.5 ± 0.6	
B1490	N1745	<9.4	1.3 + 0.4	7.8 + 0.9	
B1505	N0900	<6.6	1.1 + 0.4	3.1 + 1.4	
E1505	N1100	<9.1	<1.8	<4.9	
E1505	N1600	<4.3	1.2 + 0.2	1.4 + 0.4	
E1505	N1700	<7.1	0.7 + 0.1	4.1 + 1.7	
E1505	N1750	<8.2	1.7 ± 0.3	5.9 ± 0.5	

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DOWNHOLE GAMMA LOGGING RESULTS*

FOR THE NEW JERSEY VEHICLE INSPECTION STATION PROPERTY

	rdinates	Depth	Counts
B , W	N , S	(ft)	per Minute
E1000	N0992	0.5	10,000
B1000	N0992	1.0	12,000
B1000	N0992	1.5	12,000
E1000	N0992	2.0	13,000
E1000	N1100	0.5	8,000
B1000	N1100	1.0	10,000
B1000	N1100	1.5	10,000
B1000	N1100	2.0	11,000
B1000	N1100	2.5	10,000
B100 0	N1100	3.0	10,000
E1000	N1100	3.5	9,000
B1000	N1100	4.0	9,000
E1000	N1100	4.5	8,000
B100 0	N1200	0.5	8,000
E1000	N1200	1.0	10,000
B10 00	N1200	1.5	10,000
B100 0	N1200	2.0	11,000
B1000	N1200	2.5	11,000
E1000	N1200	3.0	10,000
B1000	N1200	3.5	11,000
E1000	N1200	4.0	9,000
B1000	N1200	4.5	9,000
E1000	N1200	5.0	9,000
B1000	N1300	0.5	10,000
E1000	N1300	1.0	11,000
B1000	N1300	1.5	11,000
E1000	N1300	2.0	10,000
B1000	N1300	2.5	10,000
E1000	N1300	3.0	11,000
B1000	N1300	3.5	10,000
E1000	N1300	4.0	10,000
E1000	N1300	4.5	10,000
E1000	N1300	5.0	8,000
B1000	N1300	5.5	8,000
E1000	N1300	6.0	8,000
B100 0	N1300	6.5	8,000
B1000	N1300	7.0	8,000
B1000	N1300	7.5	8,000
E1000	N1300	8.0	8,000
B1000	N1300	8.5	8,000

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Pa	ge	2	of	30

Grid Coordinates		Depth	Counts
E,W	N,S	(ft)	per Minute
E1000	N1300	9.0	8,000
E1000	N1300	9.5	8,000
E1000	N1300	10.0	8,000
B1000	N1300	10.5	8,000
E1000	N1300	11.0	8,000
B1000	N1300	11.5	8,000
B1000	N1300	12.0	9,000
E1000	N1300	12.5	9,000
E1000	N1300	13.0	9,000
B1000	N1300	13.5	9,000
E1000	N1300	14.0	9,000
B1000	N1400	0.5	9,000
B1000	N1400	1.0	9,000
B10 00	N1400	1.5	9,000
B10 00	N1400	2.0	10,000
E1000	N1400	2.5	9,000
E1000	N1400	3.0	9,000
B1000	N1400	3.5	8,000
B1000	N1400	4.0	8,000
E1000	N1400	4.5	8,000
E1000	N1500	0.5	9,000
B10 00	N1500	1.0	10,000
B1000	N1500	1.5	11,000
B1000	N1500	2.0	11,000
B1000	N1500	2.5	11,000
B100 0	N1500	3.0	11,000
B1000	N1500	3.5	10,000
E1000	N1500	4.0	9,000
E1000	N1500	4.5	9,000
B 1000	N1600	0.5	13,000
B1000	N1600	1.0	12,000
B1000	N1600	1.5	10,000
B1000	N1600	2.0	10,000
B1000	N1600	2.5	9,000
B1000	N1600	3.0	9,000
E1000	N1600	3.5	9,000
B1000	N1600	4.0	8,000
B1000	N1600	4.5	7,000
E1000	N1600	5.0	6,000
B1000	N1600	5.5	7,000

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<u>Grid Coor</u>	dinates	Depth	Counts
Ε,₩	N,S	(ft)	per Minute
B1000	N1600	6.0	6,000
E1000	N1600	6.5	9,000
E1000	N1650	0.5	15,000
B1000	N1650	1.0	15,000
E1000	N1650	1.5	12,000
E1000	N1650	2.0	12,000
E1000	N1650	2.5	11,000
B1000	N1650	3.0	12,000
B100 0	N1650	3.5	11,000
B1000	N1650	4.0	10,000
E1000	N1700	0.5	34,000
E1000	N1700	1.0	41,000
B1000	N1700	1.5	32,000
B1000	N1700	2.0	17,000
B1000	N1700	2.5	11,000
B1000	N1700	3.0	9,000
E1000	N1700	3.5	9,000
B 1000	N1700	4.0	9,000
B1000	N1700	4.5	8,000
B1000	N1700	5.0	8,000
B1000	N1700	5.5	7,000
B1000	N1700	6.0	7,000
E1000	N1700	6.5	8,000
B1000	N1700	7.0	12,000
E1000	N1700	7.5	12,000
E1000	N1700	8.0	13,000
B1000	N1700	8.5	13,000
B1000	N1700	9.0	11,000
E1000	N1700	9.5	11,000
B1000	N1750	0.5	50,000
B1000	N1750	1.0	52,000
B100 0	N1750	1.5	38, 000
B1000	N1750	2.0	60,000
B1000	N1750	2.5	13,000
B1000	N1750	3.0	11,000
B1000	N1750	3.5	10,000
E1000	N1800	0.5	39,000
B1000	N1800	1.0	47,000
E1000	N1800	1.5	36,000

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	<u>ordinates</u>	Depth	Counts
B,W	N,S	(ft)	per Minute
B1000	N1800	2.0	30,000
B1000	N1800	2.5	38,000
B1000	N1800	3.0	33,000
B100 0	N1800	3.5	32,000
B1000	N1800	4.0	61,000
B1000	N1800	4.5	57,000
B1000	N1800	5.0	25,000
B1000	N1800	5.5	12,000
B1000	N1800	6.0	9,000
B1000	N1800	6.5	9,000
E1000	N1800	7.0	9,000
B1000	N1800	7.5	11,000
B1000	N1800	8.0	12,000
B1000	N1800	8.5	10,000
B1000	N1800	9.0	11,000
B1000	N1800	9.5	10,000
B1000	N1800	10.0	11,000
B1004	N1831	0.5	41,000
B1004	N1831	1.0	48,000
B1004	N1831	1.5	52,000
B1004	N1831	2.0	68,000
B1004	N1831	2.5	80,000
B1004	N1831	3.0	63,000
B1004	N1831	3.5	42,000
B1004	N1831	4.0	31,000
B1004	N1831	4.5	40,000
B1004	N1831	5.0	63,000
B1004	N1831	5.5	72,000
B1004	N1831	6.0	90,000
B1004	N1831	6.5	82,000
B1004	N1831	7.0	40,000
E1004	N1831	7.5	19,000
B1004	N1831	8.0	15,000
B1004	N1831	8.5	14,000
E1008	N1875	0.5	43,000
E1008	N1875	1.0	48,000
B1008	N1875	1.5	47,000
B1008	N1875	2.0	25,000
E1008	N1875	2.5	13,000
B1008	N1875	3.0	10,000
B1008	N1875	3.5	11,000

(continued)

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	rdinates	Depth	Counts
E,W	N, S	(ft)	per Minute
B1008	N1875	4.0	13,000
B1008	N1875	4.5	13,000
E1008	N1875	5.0	13,000
B1008	N1875	5.5	13,000
B1008	N1875	6.0	12,000
E1008	N1875	6.5	10,000
E1008	N1875	7.0	10,000
E1008	N1875	7.5	9,000
E1008	N1875	8.0	9,000
E1008	N1875	8.5	9,000
E1008	N1875	9.0	9,000
E1020	N1820	0.5	38,000
E1020	N1820	1.0	33,000
B1020	N1820	1.5	23,000
E1020	N1820	2.0	19,000
B1020	N1820	2.5	17,000
E1080	N1875	0.5	27,000
B1080	N1875	1.0	30,000
E1080	N1875	1.5	30,000
E1080	N1875	2.0	31,000
E1080	N1875	2.5	23,000
E1080	N1875	3.0	16,000
E1085	N1747	0.5	28,000
B1085	N1747	1.0	35,000
B1085	N1747	1.5	21,000
B1085	N1747	2.0	15,000
E108 5	N1747	2.5	16,000
E1085	N1747	3.0	15,000
B1085	N1747	3.5	16,000
E1085	N1747	4.0	14,000
E1085	N1747	4.5	14,000
B1085	N1747	5.0	11,000
E1085	N1747	5.5	12,000
B1085	N1747	6.0	13,000
E1085	N1747	6.5	12,000
B1085	N1747	7.0	11,000
E1085	N1747	7.5	10,000
E1085	N1747	8.0	10,000
E1100	N0900	0.5	8,000
E1085	N1747	8.0	10,00

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	<u>rdinates</u>	Depth	Counts
B,W	N,S	(ft)	per Minute
E1100	N0900	1.0	12,000
B1100	N0900	1.5	13,000
B1100	N0900	2.0	14,000
E 1100	N0900	2.5	13,000
B1100	N0900	3.0	15,000
B1100	N0900	3.5	15,000
B1100	N0900	4.0	15,000
E1100	N0900	4.5	16,000
E1100	N1000	0.5	6,000
B1100	N1000	1.0	7,000
B1100	N1000	1.5	9,000
E1100	N1000	2.0	12,000
E1100	N1000	2.5	14,000
E1100	N1000	3.0	15,000
B1100	N1000	3.5	15,000
E1100	N1000	4.0	14,000
B1100	N1080	0.5	11,000
E1100	N1080	1.0	11,000
B1100	N1080	1.5	11 ,0 00
E1100	N1080	2.0	11,000
B1100	N1080	2.5	11,000
B1100	N1080	3.0	11,000
B1100	N1080	3.5	10,000
B1100	N1080	4.0	9,000
B1100	N1080	4.5	10,000
B1100	N1080	5.0	10,000
B1100	N1185	0.5	11,000
B1100	N1185	1.0	12,000
B1100	N1185	1.5	13,000
E1100	N1185	2.0	13,000
B1100	N1185	2.5	12,000
B1100	N1185	3.0	12,000
B1100	N1185	3.5	10,000
E1100	N1185	4.0	9,000
B1100	N1185	4.5	9,000
E1100	N1185	5.0	9,000
B1100	N1185	5.5	10,000
E1100	N1185	6.0	10,000
B1100	N1185	6.5	9,000
E1100	N1185	7.0	9,000

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- · · .		D	Counta
	<u>rdinates</u>	Depth	Counts
E,W	N, S	(ft)	per Minute
B1100	N1185	7.5	8,000
E1100		8.0	8,000
E1100	N1185		÷
B1100	N1185	8.5	8,000
B1100	N1300	0.5	6,000
B1100	N1300	1.0	6,000
B1100	N1300	1.5	8,000
B1100	N1300	2.0	9,000
B1100	N1300	2.5	9,000
B1100	N1300	3.0	10,000
B1100	N1300	3.5	9,000
B1100	N1300	4.0	9,000
E1100	N1300	4.5	9,000
B1100	N1400	0.5	20,000
B1100	N1400	1.0	19,000
B1100	N1400	1.5	14,000
B1100	N1400	2.0	12,000
B1100	N1400	2.5	9,000
B1100	N1400	3.0	10,000
B1100	N1400	3.5	9,000
E1100	N1400	4.0	8,000
E1100	N1400	4.5	8,000
B1100	N1500	0.5	9,000
B1100	N1500	1.0	9,000
E1100	N1500	1.5	11,000
B1100	N1500	2.0	10,000
B1100	N1500	2.5	9,000
E1100	N1500	3.0	9,000
E1100	N1500	3.5	9,000
B1100	N1500	4.0	8,000
		4.0	•
E1100	N1500		8,000
B1100	N1500	5.0	9,000
B1100	N1700	0.5	23,000
B1100	N1700	1.0	13,000
E1100	N1700	1.5	10,000
B1100	N1700	2.0	12,000
B1100	N1700	2.5	12,000
11100	N1700	3.0	14,000
B1100			•
E1100 E1100 E1100	N1700 N1700	3.5	10,000 9,000

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crid Coc	rdinates	Depth	Counts
	N,S	(ft)	per Minute
E,W	N, 5	(10)	per minute
B1100	N1700	4.5	8,000
			·
E1100	N1800	0.5	21,000
E1100	N1800	1.0	28,000 18,000
B1100	N1800	1.5	13,000
B1100	N1800	2.0 2.5	14,000
B1100	N1800		•
B1100	N1800	3.0	19,000
B1100	N1800	3.5	31,000
E1100	N1800	4.0	71,000
B1100	N1800	4.5	20,000
E1100	N1800	5.0 5.5	43,000
E1100	N1800		165,000 162,000
E1100	N1800	6.0 6.5	46,000
B1100	N1800	7.0	16,000
E1100	N1800	7.5	11,000
B1100	N1800	8.0	11,000
B1100	N1800 N1800	8.5	10,000
B1100		9.0	9,000
E1100 E1100	N1800 N1800	9.5	9,000
B1100	N1800	10.0	10,000
E1100	N1855	0.5	35,000
B 1100	N1855	1.0	35,000
B1100	N1855	1.5	40,000
E1100	N1855	2.0	44,000
B1100	N1855	2.5	39,000
B1100 B1100	N1855	3.0	33,000
B1100	N1855	3.5	54,000
E1100	N1855	4.0	124,000
B1100	N1855	4.5	122,000
B1100	N1855	5.0	45,000
B1100	N1855	5.5	21,000
B1100	N1855	6.0	16,000
B1100	N1855	6.5	15,000
B1100	N1855	7.0	14,000
E1100	N1855	7.5	13,000
B1100	N1855	8.0	13,000
B1100	N1855	8.5	12,000
E 1100	N1900	0.5	34,000
E1100	N1900	1.0	54,000

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	rdinates	Depth	Counts
E,W	N, S	(ft)	per Minute
E1100	N1900	1.5	68,000
B1100	N1900	2.0	35,000
B1100	N1900	2.5	16,000
B1100	N1900	3.0	11,000
E 1100	N1900	3.5	9,000
B1100	N1900	4.0	8,000
B1100	N1900	4.5	9,000
B1100	N1900	5.0	10,000
B1100	N1900	5.5	13,000
B1100	N1900	6.0	13,000
E1106	N1818	0.5	11,000
E1106	N18 18	1.0	9,000
B1106	N1818	1.5	9,000
B1106	N1818	2.0	9,000
E1106	N1818	2.5	10,000
B1106	N1818	3.0	12,000
B1106	N1818	3.5	14,000
B1106	N1818	4.0	14,000
B1106	N1818	4.5	16,000
B1106	N1818	5.0	19,000
B1106	N1818	5.5	20,000
B1106	N1818	6.0	16,000
E1106	N1818	6.5	15,000
B1110	N1600	0.5	11,000
B1110	N1600	1.0	11,000
B1110	N1600	1.5	12,000
B1110	N1600	2.0	12,000
B1110	N1600	2.5	13,000
B1110	N1600	3.0	11,000
B1110	N1600	3.5	9,000
E1110	N1600	4.0	9,000
B1110	N1600	4.5	9,000
E1125	N1795	0.5	19,000
B1125	N1795	1.0	27,000
B1125	N1795	1.5	23,000
B1125	N1795	2.0	14,000
E1140	N1680	0.5	20,000
B1140	N1680	1.0	19,000
B1140	N1680	1.5	11,000

(continued)

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Grid Coo	rdinates	Depth	Counts
E,W	N,S	(ft)	per Minute
····			
B1140	N1680	2.0	11,000
B1140	N1680	2.5	9,000
B1140	N1680	3.0	10,000
B1150	N1660	0.5	34,000
B1150	N1660	1.0	17,000
E1150	N1660	1.5	12,000
B1150	N1660	2.0	11,000
E1150	N1660	2.5	10,000
B1150	N1660	3.0	10,000
7115 0	N1700	0 5	39 000
B1150 B1150	N1700 N1700	0.5	38,000
E1150 E1150	N1700	1.0	26,000
		1.5	22,000
E1150 E1150	N1700	2.0	18,000
E1150 E1150	N1700	2.5 3.0	17,000
	N1700		15,000
B1150	N1700	3.5	10,000
B1165	N1470	0.5	13,000
E1165	N1470	1.0	15,000
B1165	N1470	1.5	15,000
E1165	N1470	2.0	13,000
B1165	N1470	2.5	11,000
B1170	N1605	0.5	38,000
B1170	N1605	1.0	22,000
E1170	N1605	1.5	18,000
B1170	N1605	2.0	11,000
E1170	N1605	2.5	11,000
B1190	N1820	0.5	22,000
B1190	N1820	1.0	14,000
B1190	N1820	1.5	12,000
E1190	N1820	2.0	10,000
B1190	N1820	2.5	11,000
B1190	N1820	3.0	11,000
E1190	N1820	3.5	11,000
B 1192	N1749	0.5	43,000
B1192	N1749	1.0	33,000
B1192	N1749	1.5	18,000
B1192	N1749	2.0	16,000
	MI I TU		10,000

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rid Coo	rdinates	Depth	Counts
B,W	N, S	(ft)	per Minute
B 1192	N1749	2.5	18,000
B1192	N1749	3.0	17,000
B 1192	N1749	3.5	17,000
B1192	N1749	4.0	17,000
B1192	N1749	4.5	12,000
B1192	N1749	5.0	10,000
E1192	N1749	5.5	9,000
B1192	N1749	6.0	9,000
B1192	N1749	6.5	8,000
B1192	N1749	7.0	8,000
B1192	N1749	7.5	8,000
E1192	N1749	8.0	7,000
E1200	N1000	0.5	14,000
E1200	N1000	1.0	11,000
B1200	N1000	1.5	13,000
B1200	N1000	2.0	13,000
B1200	N1000	2.5	13,000
B1200	N1000	3.0	14,000
E1200	N1000	3.5	14,000
B1200	N1000	4.0	13,000
E1200	N1100	0.5	10,000
B1200	N1100	1.0	11,000
B 1200	N1100	1.5	11,000
B1200	N1100	2.0	12,000
E1200	N1100	2.5	11,000
B1200	N1100	3.0	12,000
B1200	N1100	3.5	13,000
E1200	N1100	4.0	13,000
E1200	N1100	4.5	14,000
B1200	N1100	5.0	12,000
E1200	N1100	5.5	13,000
B1200	N1100	6.0	14,000
B1200	N1300	0.5	8,000
B1200	N1300	1.0	10,000
E1200	N1300	1.5	10,000
B1200	N1300	2.0	9,000
B1200	N1300	2.5	9,000
B1200	N1300	3.0	9,000
B1200 B1200	N1300	3.5	9,000
DIGAA	MT300	5.0	0,000

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Grid Coor	<u>rdinates</u>	Depth	Counts
E,W	N, S	(ft)	per Minute
E1200	N1400	0.5	8,000
B1200	N1400	1.0	10,000
B1200	N1400	1.5	11,000
B1200	N1400	2.0	11,000
B1200	N1400	2.5	10,000
B1200	N1400	3.0	9,000
B1200	N1400	3.5	9,000
B1200	N1400	4.0	9,000
E1200	N1400	4.5	9,000
E1200	N1400	5.0	8,000
E1200	N1400	5.5	9,000
B1200	N1400	6.0	10,000
B1200	N1400	6.5	8,000
B1200	N1400	7.0	8,000
B1200	N1400	7.5	7,000
B1200	N1400	8.0	7,000
B1200	N1400	8.5	9,000
B 1200	N1400	9.0	9,000
E1200	N1500	0.5	17,000
B1200	N1500	1.0	14,000
B1200	N1500	1.5	11,000
B1200	N1500	2.0	10,000
B1200	N1500	2.5	10,000
B1200	N1500	3.0	10,000
B1200	N1500	3.5	9,000
B1200	N1500	4.0	9,000
B1200	N1500	4.5	10,000
B1200	N1600	0.5	15,000
E1200	N1600	1.0	14,000
B1200	N1600	1.5	9,000
B1200	N1600	2.0	8,000
B1200	N1600	2.5	8,000
E1200	N1600	3.0	7,000
B1200	N1600	3.5	6,000
B1200	N1600	4.0	6,000
B1200	N1600	4.5	6,000
B1200	N1700	0.5	9,000
B1200	N1700	1.0	10,000
B1200	N1700	1.5	12,000
B1200	N1700	2.0	11,000

(continued)

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	<u>ordinates</u>	Depth	Counts
E,W	N,S	(ft)	per Minute
E1200	N1700	2.5	11,000
B1200	N1700	3.0	16,000
B 1200	N1700	3.5	17,000
B1200	N1700	4.0	16,000
E1200	N1700	4.5	17,000
B1200	N1700	5.0	18,000
E1200	N1808	0.5	22,000
B1200	N1808	1.0	14,000
B 1200	N1808	1.5	11,000
B1200	N1808	2.0	10,000
B120 0	N1808	2.5	12,000
B1200	N1808	3.0	11,000
B1200	N1808	3.5	10,000
B1200	N1808	4.0	11,000
B1200	N1808	4.5	9,000
B1200	N1808	5.0	9,000
B1200	N1808	5.5	11,000
B1200	N1808	6.0	11,000
B1200	N1808	6.5	10,000
B 1200	N1808	7.0	9,000
B1203	N1776	0.5	11,000
B1203	N1776	1.0	10,000
E1203	N1776	1.5	12,000
E1203	N1776	2.0	14,000
E1203	N1776	2.5	13,000
B1203	N1776	3.0	13,000
E1203	N1776	3.5	14,000
B1203	N1776	4.0	13,000
B120 3	N1776	4.5	12,000
B1203	N1776	5.0	11,000
B1203	N1776	5.5	13,000
B120 3	N1776	6.0	14,000
B1203	N1776	6.5	14,000
B1203	N1776	7.0	11,000
E1203	N1776	7.5	11,000
B1203	N1776	8.0	15,000
E1203	N1776	8.5	17,000
B 1203	N1776	9.0	15,000
B1203	N1776	9.5	11,000
B1210	N1755	0.5	56,000

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	rdinates	Depth	Counts
B,W	N,S	(ft)	per Minute
B1210	N1755	1.0	33,000
B1210	N1755	1.5	16,000
B1210	N1755	2.0	12,000
B1210	N1755	2.5	11,000
E1210	N1910	0.5	16,000
B1210	N1910	1.0	19,000
E1210	N1910	1.5	12,000
B1210	N1910	2.0	9,000
E1210	N1910	2.5	9,000
E1210	N1910	3.0	9,000
B1210	N1910	3.5	8,000
B1210	N1910	4.0	7,000
B1210	N1910	4.5	7,000
B1210	N1910	5.0	7,000
B1210	N1910	5.5	6,000
E1210	N1910	6.0	6,000
E1215	N0840	0.5	18,000
E1215	N0840	1.0	18,000
E1215	N0840	1.5	16,000
B1215	N0840	2.0	16,000
B1215	N0840	2.5	16,000
B1215	N0840	3.0	16,000
B1215	N0840	3.5	14,000
B1215	N0840	4.0	14,000
B1215	N0840	4.5	14,000
B1265	N1880	0.5	36,000
E1265	N1880	1.0	27,000
E1265	N1880	1.5	14,000
E1265	N1880	2.0	12,000
E1265	N1880	2.5	11,000
E1265	N1880	3.0	10,000
B1270	N1220	0.5	27,000
E1270	N1220	1.0	28,000
B1270	N1220	1.5	14,000
B1270	N1220	2.0	11,000
B1270	N1220	2.5	10,000
B1270	N1220	3.0	10,000
B1270	N1220	3.5	9,000
E1270	N1220	4.0	10,000

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rid Coc B,W	rdinates	Depth (ft)	Counts
љ, п	N , S	(11)	per Minute
B1270	N1220	4.5	10,000
B1290	N0775	0.5	11,000
E1290	N0775	1.0	11,000
B1290	N0775	1.5	11,000
B1290	N0775	2.0	11,000
E1290	N0775	2.5	9,000
B1300	N0700	0.5	14,000
E1300	N0700	1.0	12,000
E1300	N0700	1.5	10,000
B1300	N0700	2.0	12,000
B1300	N0700	2.5	14,000
E1300	N0700	3.0	12,000
E1300	N0700	3.5	12,000
B1300	N0700	4.0	13,000
B1300	N0700	4.5	13,000
B1300	N0800	0.5	6,000
B1300	N0800	1.0	8,000
E1300	N0800	1.5	11,000
B1300	N0800	2.0	10,000
B 1300	N0800	2.5	10,000
B1300	N0800	3.0	9,000
E1300	N0800	3.5	10,000
E1300	N0800	4.0	11,000
E1300	N0800	4.5	12,000
B1300	N0800	5.0	11,000
E1300	N0900	0.5	13,000
B1300	N0900	1.0	11,000
B1300	N0900	1.5	10,000
B1300	N0900	2.0	11,000
B1300	N0900	2.5	11,000
B1300	N0900	3.0	10,000
E1300	N0900	3.5	11,000
B1300	N0900	4.0	11,000
B1300	N0900	4.5	11,000
B1300	N0900	5.0	11,000
B1300	N0900	5.5	10,000
B130 0	N0900	6.0	11,000
B1300	N0900	6.5	11,000
B1300	N0900	7.0	11,000

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	rdinates	Depth	Counts
Β,₩	N,S	(ft)	per Minute
B1300	N0900	7.5	11,000
B1300	N0900	8.0	12,000
E1300	N0900	8.5	12,000
E1300	N0900	9.0	12,000
E1300	N0900	9.5	12,000
E1300	N1000	0.5	11,000
B1300	N1000	1.0	11,000
B1300	N1000	1.5	11,000
E1300	N1000	2.0	11,000
B1300	N1000	2.5	12,000
B1300	N1000	3.0	13,000
B1300	N1000	3.5	12,000
B1300	N1000	4.0	13,000
E1300	N1100	0.5	15,000
E1300	N1100	1.0	12,000
B1300	N1100	1.5	12,000
B1300	N1100	2.0	13,000
E1300	N1100	2.5	14,000
B1300	N1100	3.0	13,000
E1300	N1100	3.5	14,000
B1300	N1100	4.0	13,000
E1300	N1200	0.5	18,000
B1300	N1200	1.0	17,000
B1300	N1200	1.5	13,000
E1300	N1200	2.0	12,000
B1300	N1200	2.5	12,000
B1300	N1200	3.0	11,000
B1300	N1200	3.5	10,000
E1300	N1200	4.0	11,000
B1300	N1200	4.5	10,000
B1300	N1200	5.0	11,000
B1300	N1200	5.5	9,000
B1300	N1200	6.0	9,000
E1300	N1200	6.5	8,000
E1300	N1200	7.0	8,000
E1300	N1200	7.5	9,000
B1300	N1200	8.0	7,000
B1300	N1300	0.5	6,000
E1300	N1300	1.0	8,000

(continued)

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Frid Coo B,W	ordinates N,S	Depth (ft)	Count s per Minute
B1300	N1300	1.5	8,000
B1300	N1300	2.0	9,000
B1300	N1300	2.5	9,000
E1300	N1300	3.0	8,000
B1300	N1300	3.5	9,000
B1300	N1300	4.0	9,000
B1300	N1300	4.5	10,000
B1300	N1300	5.0	10,000
B1300	N1400	0.5	8,000
E1300	N1400	1.0	10,000
E1300	N1400	1.5	11,000
E1300	N1400	2.0	13,000
B1300	N1400	2.5	11,000
E1300	N1400	3.0	9,000
E1300	N1400	3.5	9,000
E1300	N1400	4.0	9,000
B1300	N1400	4.5	9,000
E1300	N1400	5.0	9,000
E1300	N1400	5.5	9,000
E1300	N1500	0.5	7,000
E1300	N1500	1.0	8,000
E1300	N1500	1.5	8,000
E1300	N1500	2.0	8,000
B1300	N1500	2.5	8,000
B1300	N1500	3.0	8,000
E1300	N1500	3.5	8,000
B1300	N1500	4.0	8,000
E1300	N1500	4.5	7,000
B1300	N1500	5.0	7,000
E1300	N1500	5.5	7,000
E1300	N1600	0.5	15,000
E1300	N1600	1.0	14,000
B1300	N1600	1.5	9,000
E1300	N1600	2.0	8,000
E1300	N1600	2.5	9,000
E1300	N1600	3.0	8,000
B1300	N1600	3.5	7,000
B1300	N1600	4.0	7,000
E1300	N1600	4.5	6,000
E1300	N1700	0.5	9,000

(continued)

Pag	e	18	of	30

B,W	N . N	(ft)	per Minute
	N , S	(10)	per minute
B1300	N1700	1.0	9,000
B1300	N1700	1.5	10,000
E1300	N1700	2.0	13,000
B1300	N1700	2.5	10,000
B1300	N1700	3.0	10,000
B1300	N1700	3.5	10,000
E1300	N1700	4.0	14,000
B1300	N1700	4.5	16,000
B1300	N1700	5.0	10,000
E1300	N1700	5.5	8,000
B1300	N1700	6.0	8,000
B1300	N1700	6.5	8,000
B1300	N1700	7.0	9,000
B1300	N1700	7.5	9,000
B1300	N1700	8.0	10,000
B1300	N1700	8.5	11,000
81000	NI / UU	0.5	11,000
B1300	N1750	0.5	10,000
B1300	N1750	1.0	11,000
E1300	N1750	1.5	13,000
B1300	N1750	2.0	14,000
B1300	N1750	2.5	13,000
B1300	N1750	3.0	13,000
B1300	N1750	3.5	13,000
B1300	N1750	4.0	18,000
B1300	N1750	4.5	19,000
E1300	N1750	5.0	15,000
B1300	N1750	5.5	11,000
E1300	N1750	6.0	
E1300	N1750		9,000
B1300	N1750	6.5	8,000
E1300	N1775	0.5	41,000
B1300	N1775	1.0	66,000
B1300	N1775	1.5	64,000
B1300 B1300	N1775	2.0	26,000
E1300	N1775	2.5	
B1300	N1775	2.5 3.0	15,000
E1300	N1775	3.5	11,000
E1300 E1300	N1775	3.5 4.0	10,000 10,000
E1300	N1775	4.0	-
B1300 B1300	N1775		10,000
		5.0	10,000
E1300	N1775	5.5	10,000

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Grid Coor B,W B1300	N,S	Depth (ft)	Counts per Minute
B 1300	N, S	(ft)	ner Minute
			Per MINUCE
	N1790	1.0	17,000
B1300	N1790	1.5	18,000
B130 0	N1790	2.0	14,000
E1300	N1790	2.5	14,000
B1300	N1790	3.0	21,000
B1300	N1790	3.5	18,000
B1300	N1790	4.0	15,000
B1300	N1790	4.5	11,000
B 1300	N1790	5.0	9,000
B1300	N1790	5.5	9,000
E1300	N1790	6.0	9,000
B1300	N1790	6.5	9,000
E1300	N1790	7.0	9,000
B1300	N1790	7.5	7,000
E1300	N1790	8.0	7,000
B1300	N1822	0.5	11,000
E1300	N1822	1.0	9,000
E1300	N1822	1.5	9,000
B1300	N1822	2.0	10,000
B1300	N1822	2.5	9,000
E1300	N1822	3.0	11,000
E1300	N1822	3.5	14,000
E1300	N1822	4.0	14,000
B1300	N1822	4.5	15,000
B1300	N1822	5.0	12,000
E1300	N1822	5.5	10,000
B1300	N1822	6.0	10,000
B1300	N1822	6.5	9,000
E1300	N1822	7.0	9,000
B1300	N1822	7.5	9,000
E1300	N1822	8.0	9,000
B1300	N1915	0.5	33,000
E1300	N1915	1.0	19,000
B1300	N1915	1.5	12,000
E1300	N1915	2.0	11,000
B130 0	N1915	2.5	10,000
B1300	N1915	3.0	9,000
B1300	N1915	3.5	9,000
B1300	N1915	4.0	8,000
B1300	N1915	4.5	7,000
B1300	N1915	5.0	8,000

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	ordinates	Depth	Counts
B, W	N,S	(ft)	per Minute
E1307	N1890	0.5	17,000
E1307	N1890	1.0	11,000
B1307	N1890	1.5	11,000
E1307	N1890	2.0	11,000
B1307	N1890	2.5	10,000
B1307	N1890	3.0	10,000
B1307	N1890	3.5	9,000
B1307	N1890	4.0	8,000
B1307	N1890	4.5	7,000
B1307	N1890	5.0	7,000
B1307	N1890	5.5	7,000
E1307	N1890	6.0	7,000
B1307	N1890	6.5	7,000
B1307	N1890	7.0 .	8,000
B1307	N1890	7.5	8,000
BIOVI	N1030	1.5	8,000
B1315	N1835	0.5	19,000
B1315	N1835	1.0	18,000
B1315	N1835	1.5	15,000
B1315	N1835	2.0	10,000
B1315	N1835	2.5	10,000
B1315	N1835	3.0	9,000
E1320	N1540	0.5	7,000
B1320	N1540	1.0	8,000
E1320	N1540	1.5	8,000
E1320	N1540	2.0	8,000
B1320	N1540	2.5	9,000
B13 50	N0710	0.5	32,000
B1350	N0710	1.0	33,000
B1350	N0710	1.5	31,000
B1350	N0710	2.0	24,000
B1350	N0710	2.5	20,000
E1370	N1735	0.5	16,000
B1370	N1735	1.0	12,000
B137 0	N1735	1.5	11,000
B 1370	N1735	2.0	11,000
B1370	N1735	2.5	11,000
B1380	N1615	0.5	35,000
E1380	N1615	1.0	00,000

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Pa	ge	21	of	30
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<u>Grid Coc</u>	ordinates	Depth	Counts
B,W	N,S	(ft)	per Minute
E1380	N1615	1.5	16,000
B1380	N1615	2.0	10,000
B1380	N1615	2.5	8,000
E1390	N1783	0.5	31,000
B1390	N1783	1.0	47,000
B1390	N1783	1.5	24,000
B1390	N1783	2.0	14,000
E1390	N1783	2.5	12,000
B 1390	N1783	3.0	11,000
B1390	N1783	3.5	8,000
B1390	N1783	4.0	8,000
E1390	N1783	4.5	7,000
B1395	N1763	0.5	49,000
E1395	N1763	1.0	57,000
E1395	N1763	1.5	33,000
E1395	N1763	2.0	24,000
E1395	N1763	2.5	37,000
B1395	N1763	3.0	77,000
B1395	N1763	3.5	106,000
E1395	N1763	4.0	55,000
B1395	N1763	4.5	24,000
E1395	N1763	5.0	14,000
B1395	N1763	5.5	14,000
E1395	N1763	6.0	12,000
E1395	N1763	6.5	11,000
B1395	N1763	7.0	11,000
B1396	N1892	0.5	8,000
B1396	N1892	1.0	10,000
B1396	N1892	1.5	11,000
B1396	N1892	2.0	11,000
B1396	N1892	2.5	11,000
E 1396	N1892	3.0	11,000
B1396	N1892	3.5	10,000
B1396	N1892	4.0	11,000
B1396	N1892	4.5	9,000
B1396	N1892	5.0	9,000
B1396	N1892	5.5	8,000
B1396	N1892	6.0	7,000
B1396	N1892	6.5	7,000
E1396	N1892	7.0	7,000

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Grid Coc	ordinates	Depth	Counts
B,W	N,S	(ft)	per Minute
B 1396	N1892	7.5	7,000
B1396	N1892	8.0	7,000
B1396	N1892	8.5	7,000
B1400	N0700	0.5	19,000
B1400	N0700	1.0	22,000
E1400	N0700	1.5	25,000
B1400	N0700	2.0	18,000
B1400	N0700	2.5	15,000
B1400	N0700	3.0	17,000
B1400	N0700	3.5	16,000
B1400	N0700	4.0	14,000
B1400	N0700	4.5	14,000
B1400	N0700	5.0	14,000
B1400	N0800	0.5	10,000
B1400	N0800	1.0	11,000
B140 0	N0800	1.5	12,000
B1400	N0800	2.0	11,000
B1400	N08 00	2.5	12,000
B1400	N0800	3.0	11,000
E1400	N0800	3.5	11,000
B1400	N0800	4.0	12,000
E1400	N0800	4.5	11,000
B1400	N0800	5.0	11,000
E1400	N0900	0.5	11,000
B1400	N0900	1.0	10,000
B1400	N0900	1.5	11,000
B14 00	N0900	2.0	11,000
B1400	N0900	2.5	11,000
B1400	N0900	3.0	10,000
B1400	N0900	3.5	11,000
B1400	N0900	4.0	11,000
E1400	N0900	4.5	11,000
E1400	N0900	5.0	11,000
E1400	N0900	5.5	12,000
B1400	N0900	6.0	12,000
E1400	N0900	6.5	13,000
E1400	N1000	0.5	13,000
B1400	N1000	1.0	13,000
B1400	N1000	1.5	13,000

Grid Coordinates		Depth	Counts
E, W	N,S	(ft)	per Minute
B1400	N1000	2.0	13,000
B1400	N1000	2.5	14,000
B1400	N1000	3.0	13,000
B1400	N1000	3.5	13,000
B1400	N1100	0.5	10,000
E1400	N1100	1.0	12,000
E1400	N1200	0.5	10,000
E1400	N1200	1.0	11,000
E1400	N1200	1.5	13,000
B1400	N1200	2.0	13,000
E1400	N1200	2.5	13,000
B1400	N1200	3.0	13,000
E1400	N1200	3.5	13,000
E1400	N1200	4.0	13,000
E1400	N1300	0.5	5,000
B1400	N1300	1.0	7,000
E1400	N1300	1.5	8,000
E1400	N1300	2.0	8,000
E1400	N1300	2.5	9,000
E1400	N1300	3.0	9,000
E1400	N1300	3.5	9,000
B1400	N1300	4.0	8,000
E1400	N1300	4.5	8,000
B1400	N1400	0.5	10,000
B1400	N1400	1.0	12,000
B1400	N1400	1.5	11,000
E1400	N1400	2.0	10,000
E1400	N1400	2.5	9,000
E1400	N1400	3.0	9,000
E1400	N1400	3.5	9,000
E1400	N1400	4.0	8,000
B1400	N1400	4.5	8,000
E1400	N1500	0.5	8,000
E1400	N1500	1.0	11,000
E1400	N1500	1.5	8,000
E1400	N1500	2.0	9,000
E1400	N1500	2.5	9,000
E1400	N1500	3.0	9,000

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rid Coo	<u>rdinates</u>	Depth	Counts
E,W	N, S	(ft)	per Minute
E1400	N1500	3.5	8,000
B1400	N1500	4.0	8,000
E1400	N1500	4.5	8,000
B1400	N1500	5.0	9,000
E1400	N1500	5.5	9,000
E1400	N1600	0.5	22,000
B1400	N1600	1.0	20,000
B1400	N1600	1.5	11,000
B14 00	N1600	2.0	9,000
B1400	N1600	2.5	9,000
E1400	N1600	3.0	7,000
B1400	N1600	3.5	6,000
B1400	N1600	4.0	6,000
B1400	N1600	4.5	7,000
B1400	N1600	5.0	9,000
E1400	N1600	5.5	9,000
E1400	N1600	6.0	9,000
E1400	N1600	6.5	9,000
E1400	N1600	7.0	9,000
B1400	N1600	7.5	10,000
E1400	N1600	8.0	10,000
B1400	N1600	8.5	10,000
E1400	N1600	9.0	10,000
E1400	N1640	0.5	20,000
E1400	N1640	1.0	20,000
E1400	N1640	1.5	13,000
E1400	N1640	2.0	11,000
E1400	N1640	2.5	10,000
E1400	N1640	3.0	9,000
B1400	N1640	3.5	10,000
E1400	N1640	4.0	10,000
B1400	N1640	4.5	10,000
B1400	N1700	0.5	25,000
B1400	N1700	1.0	26,000
E1400	N1700	1.5	21,000
B1400	N1700	2.0	14,000
E1400	N1700	2.5	13,000
B1400	N1700	3.0	12,000
E1400	N1700	3.5	10,000
B1400	N1700	4.0	8,000

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Grid Coo B,W	rdinates N,S	Depth (ft)	Count s per Minute
<u>ь</u> , н	N , 5		per minute
B140 0	N1700	4.5	8,000
B1400	N1730	0.5	17,000
B1400	N1730	1.0	31,000
B1400	N1730	1.5	53,000
B1400	N1730	2.0	70,000
B1400	N1730	2.5	44,000
B1400	N1730	3.0	18,000
B1400	N1730	3.5	13,000
B1400	N1730	4.0	12,000
B1400	N1730	4.5	13,000
B1400	N1730	5.0	12,000
E1400	N1850	0.5	16,000
B14 00	N1850	1.0	12,000
E1400	N1850	1.5	10,000
B1400	N1850	2.0	10,000
B1400	N1850	2.5	8,000
E1400	N1850	3.0	8,000
B1400	N1850	3.5	7,000
E1400	N1850	4.0	8,000
E1400	N1900	0.5	11,000
B1400	N1900	1.0	10,000
B1400	N1900	1.5	10,000
E1400	N1900	2.0	9,000
B1400	N1900	2.5	9,000
E1400	N1900	3.0	9,000
B1400	N1900	3.5	9,000
B1400	N1900	4.0	9,000
E1400	N1900	4.5	8,000
E147 5	N1935	0.5	11,000
B1475	N1935	1.0	11,000
E1475	N1935	1.5	11,000
B1475	N1935	2.0	12,000
B1475	N1935	2.5	10,000
B1475	N1935	3.0	10,000
B1475	N1935	3.5	9,000
B1475	N1935	4.0	9,000
B1475	N1935	4.5	8,000
B1475	N1935	5.0	7,000
B1475	N1935	5.5	8,000

(continued)

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Grid Cod	ordinates	Depth	Counts
B,W	N,S	(ft)	per Minute
B147 5	N1935	6.0	8,000
B147 5	N1935	6.5	7,000
B1475	N1935	7.0	7,000
E1480	N0725	0.5	26,000
B1480	N0725	1.0	23,000
B1480	N0725	1.5	16,000
B1480	N0725	2.0	15,000
B1480	N0725	2.5	13,000
E1480	N0725	3.0	13,000
E1490	N1700	0.5	25,000
B1490	N1700	1.0	30,000
E1490	N1700	1.5	36,000
B1490	N1700	2.0	34,000
E1490	N1700	2.5	20,000
E1490	N1700	3.0	15,000
E1490	N1700	3.5	13,000
E1490	N1700	4.0	13,000
E1490	N1700	4.5	12,000
E1490	N1700	5.0	11,000
E1490	N1745	0.5	46,000
B1490	N1745	1.0	51,000
E1490	N1745	1.5	82,000
E1490	N1745	2.0	98,000
E1490	N1745	2.5	85,000
B1490	N1745	3.0	53,000
B1490	N1745	3.5	20,000
B1490	N1745	4.0	15,000
E1490	N1745	4.5	9,000
B1490	N1745	5.0	9,000
E1499	N1773	0.5	39,000
B1499	N1773	1.0	57,000
E1499	N1773	1.5	26,000
E1499	N1773	2.0	15,000
E1499	N1773	2.5	12,000
B1499	N1773	3.0	11,000
E1499	N1773	3.5	10,000
B1499	N1773	4.0	10,000
E1500	N0700	0.5	20,000

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rage 21	01 30		
Grid Coo	rdinates	Depth	Counts
B,W	N,S	(ft)	per Minute
B1500	N0700	1.0	14,000
B1500	N0700	1.5	13,000
B1500	N0700	2.0	12,000
E1500	N0700	2.5	13,000
B1500	N0700	3.0	13,000
B1500	N0700	3.5	12,000
B1500	N0700	4.0	11,000
E1500	N0700	4.5	11,000
B1500 B1500	N0700	5.0	9,000
E1500	N0700	5.5	8,000
B1500	N0700	6.0	7,000
B1300	NOTOO	0.0	7,000
B1500	N0800	0.5	12,000
B1500	N0800	1.0	12,000
B1500	N0800	1.5	12,000
B1500	N0800	2.0	13,000
E1500	N0800	2.5	17,000
B1500	N0800	3.0	15,000
E1500	N0800	3.5	13,000
B1500	N0800	4.0	13,000
E1500	N0800	4.5	12,000
B1500	N0800	5.0	12,000
E1500	N0800	5.5	11,000
B1500	N0800	6.0	12,000
E1500	N0800	6.5	12,000
B1500	N0900	0.5	12,000
E1500	N0900	1.0	13,000
B1500	N0900	1.5	14,000
B1500	N0900	2.0	14,000
B1500	N0900	2.5	14,000
B 1500	N0900	3.0	13,000
E1500	N0900	3.5	14,000
B1500	N0900	4.0	14,000
B1500	N0900	4.5	13,000
E1500	N0900	5.0	13,000
E1500	N1000	0.5	11,000
E1500	N1000	1.0	14,000
B1500	N1000	1.5	13,000
BIOOU	MICOO	1.0	10,000
E1500	N1100	0.5	11,000
E1500	N1200	0.5	8,000
			-

(continued)

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	ordinates	Depth	Counts
E,W	N,S	(ft)	per Minute
B1500	N1200	1.0	9,000
B1500	N1200	1.5	12,000
E1500	N1300	0.5	10,000
E1500	N1300	1.0	11,000
E1500	N1300	1.5	11,000
B1500	N1300	2.0	9,000
E1500	N1300	2.5	9,000
E1500	N1300	3.0	10,000
B1500	N1300	3.5	10,000
B1500	N1300	4.0	9,000
E1500	N1300	4.5	9,000
B1500	N1300	5.0	8,000
E1500	N1300	5.5	8,000
B1500	N1300	6.0	8,000
E1500	N1300	6.5	8,000 8,000
B1500	N1300	7.0	
E1500	N1300	7.5 8.0	9,000 11,000
E1500	N1300	8.5	12,000
B1500 B1500	N1300 N1300	9.0	11,000
E1500	N1400	0.5	10,000
E1500	N1400	1.0	12,000
E1500 E1500	N1400	1.5	11,000
E1500	N1400 N1400	2.0	10,000
E1500	N1400	2.5	9,000
E1500	N1400	3.0	9,000
B1500	N1400	3.5	9,000
B1500	N1400	4.0	8,000
E1500	N1400	4.5	8,000
B1500	N1400	5.0	9,000
E1500	N1400	5.5	8,000
B1500	N1500	0.5	9,000
E1500	N1500	1.0	10,000
B1500	N1500	1.5	10,000
B1500	N1500	2.0	10,000
B1500	N1500	2.5	10,000
E1500	N1500	3.0	8,000
B1500	N1500	3.5	8,000
B1500	N1500	4.0	7,000
B1500	N1500	4.5	8,000

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Page 29	of 30		······
Grid <u>Coo</u>	<u>rdinates</u>	Depth	Counts
E,W	N,S	(ft)	per Minute
E1500	N1500	5.0	8,000
B1500	N1600	0.5	13,000
B 1500	N1600	1.0	11,000
B1500	N1600	1.5	10,000
B1500	N1600	2.0	9,000
B 1500	N1600	2.5	8,000
B1500	N1600	3.0	8,000
B 1500	N1600	3.5	7,000
E1500	N1600	4.0	8,000
B1500	N1600	4.5	8,000
E1500	N1650	0.5	36,000
B150 0	N1650	1.0	37,000
E1500	N1650	1.5	49,000
B1500	N1650	2.0	31,000
B1500	N1650	2.5	19,000
E1500	N1650	3.0	18,000
E1500	N1650	3.5	14,000
B 1500	N1650	4.0	15,000
E1500	N1800	0.5	22,000
B1500	N1800	1.0	15,000
E1500	N1800	1.5	11,000
B1500	N1800	2.0	10,000
B 1500	N1800	2.5	9,000
B1500	N1800	3.0	9,000
B 1500	N1800	3.5	8,000
B1500	N1800	4.0	8,000
E1500	N1800	4.5	8,000
E1500	N1850	0.5	25,000
E1500	N1850	1.0	18,000
B1500	N1850	1.5	15,000
B1500	N1850	2.0	13,000
B 1500	N1850	2.5	13,000
E1500	N1850	3.0	12,000
B1500	N1850	3.5	12,000
B1500	N1850	4.0	10,000
B1500	N1850	4.5	10,000
B1500	N1850	5.0	9,000
B1500	N1875	0.5	13,000

(continued)

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<u> </u>		
rdinates	Depth	Counts
N,S	(ft)	per Minute
N1875	1.0	12,000
N1875	1.5	13,000
N1875	2.0	13,000
N1875	2.5	12,000
N1875	3.0	13,000
N1875	3.5	12,000
N1875	4.0	11,000
N1900	0.5	9,000
N1900	1.0	11,000
N1900	1.5	11,000
N1900	2.0	11,000
N1900	2.5	9,000
N1900	3.0	10,000
N1900	3.5	10,000
N1900	4.0	9,000
N1900	4.5	10,000
N1735	0.5	18,000
N1735	1.0	16,000
N1735	1.5	14,000
N1735	2.0	10,000
N1735	2.5	9,000
N1735	3.0	9,000
N1735	3.5	9,000
N1735	4.0	10,000
	N1875 N1875 N1875 N1875 N1875 N1875 N1875 N1875 N1875 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1900 N1935 N1735 N1735 N1735 N1735 N1735	N,S (ft) N1875 1.0 N1875 1.5 N1875 2.0 N1875 2.5 N1875 3.0 N1875 3.0 N1875 3.5 N1875 3.5 N1875 3.5 N1875 3.5 N1875 3.5 N1875 3.5 N1900 0.5 N1900 1.0 N1900 1.5 N1900 2.0 N1900 2.0 N1900 3.0 N1900 3.0 N1900 3.5 N1900 4.0 N1900 4.5 N1735 1.5 N1735 1.5 N1735 2.5 N1735 3.0 N1735 3.5

^aThe results given in this table are based on penetrating the contamination or the drill reaching refusal. Any other circumstances are noted for the hole to which they apply.

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GAMMA RADIATION EXPOSURE RATE MEASUREMENTS

FOR THE NEW JERSEY VEHICLE INSPECTION STATION PROPERTY

Location	<u>Grid Coo</u>	rdinates	Exposure Rate
Number	E,W	N, S	(µR/h)
1	E1275	N1190	5
2	B1280	N1180	4
3	E1160	N1175	4
4	E1250	N1150	4
5	E1200	N1150	4
6	E1275	N1110	4
7	E1280	N1125	4
8	E1160	N1130	4

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- 6. <u>U.S. Code of Federal Regulations</u>. 40 CFR 192, "Health and Environmental Protection Standards for Uranium and Thorium Mill Tailings," Washington, DC, July 1986.
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APPENDIX A GEOLOGIC DRILL LOGS FOR THE MAYWOOD INTERIM STORAGE SITE - NEW JERSEY VEHICLE INSPECTION STATION



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	G	EOL	OGK		DRI		OG		PRESECT		F	USRAP			4501	-138	SHEET I		MELE MA. MISS-213R
ute j			NTERIN	I ST	TORAC			COMPONAT	COMPONATES AND BT5, E 1008 90°							i.	BEARDE N/A		
KAUN 7/21			/21/86]		HORE	RENCH AL SERVI			NE N	E 8-33		HOLE SEE	OVERLAND		MCX /	נד ו. 0'	TETAL SEPTE
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			NTERIN NJVI	\$		E-	COMPANYES N1900, E1100							Film H 90 ⁴)	BEARDE N/A				
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	2 CEVATRON 2 3		* VANTUR AETLAN, CRADACTER OF STELLAN, ETC.											
NUCER, 6', THROUCHOUT.		1 0555005 88 511 DEO ESTOTO 11	SITE CHECKED FOR RADIDACTIVE CONTAMINATION BY EBERLINE ANALYTICAL CORPORATION EBERLINE ANALYTICAL											
	90.6 5 99.6	5.0-6.0': SANDY SLT OL-CLE PALE GREEN GG772A SOFT, DENSE N PLAN MOST. 6.0-10.0': SLTY SAND SAN DAWN YELLOWISH ORANEZ DOVIS/6N FINE 1 MEDIAN GRANED SOFT: DENSE N PL MOST TO SATURATED AT BUD FT.	CORPORATION PERFORMED GAMMA LOGGING.											
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SS-SPLE SPOON ST-SELEY TUBE		ERIN STORAGE SITE - NJVIS	HILE HL. HISS-229R											



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GEOLOGIC DRIL	L LOG	FILEET	USRAP		OF 1 MISS-2428
SHE MAYNOOD INTERIN STORAGE NJVIS	SITE - CONTENSIT	3	N992,E1000	ANDLE FROM	MIRE BEADS 0° N/A
16.000 CONFLETED 100110 7/25/86 7/25/86 E	NORETRENCH	CES HOBIL	B UTBL. HELE SHE (N LE 8-33 6°	2.0" Note	I OTJ TETAL REPTE
CARE RECOVERING 1.70 CARE I		N/A S	B.L. ISPINEL STAND BITTER 5.5' HONE OBSE		TARL THE OF MACK 2.0'/97.5'
Safel mark short the	CARDE LETT IN HELLS BOA		LONG IN D. HCG	RANE	
		RP'IL Runc Let	DESCRIPTION AND CLASSIFIC		NUTES CON UNITER LEVELS, UNITER RETURN, CONCASTER OF DELLOS, FTC.
		0	CO-LO': SAMOY SET BLE DAY TELLORISH BROWN BOTHLY SOFTE GRAMED, SOFTFCOR, Y SOFTE CONSOLDATED LOOSE, DAW YELLOWSH URAME DOTHLY SOFT CONSOLDATED SOFTFSLIMMELY LOOSAL CAMED, SOFTFSLIMMELY ACTURES FOUND SOFTFSLIMMELY BEDLA GRAMED, SOFTFSLIMMELY CONSOLDATED SAMOSTOR BUTTONI OF HELL AT 30 FF. AUGER SPOILS WERE MAREDATEN N THE HOLE.	A POCHLY FINE TO TED: POORLY MOIST. DIF: FINE TO OTALLY HERED: SOFT HUND PIECES HOIST.	ELEVATIONS ESTABLISHED ANI AMALYTICAL CONFORATION BY EXCIDENTIAL CORRECT CONFORMATION BY EXCIDENTIAL AND CONFORATION. -DESCRIPTION AND CLASSIFICATION BY YESIAL EXAMINATION OF CUTTINGS. ALIGER REFUSAL AT 3.0 FT.
SI-SPLIT SPeak ST-SHELSY TUBL PHENISHIN PHYTICHEN G-OTHER		35 -	I STORAGE SITE - VIS		NILE III. NI 55-2428



	C	EO	OGIC	D	Ril	LL	.0G		PR0.00	T	F	USRAP			14501	-138	SHEET ND. 1 OF 1	MISS-243R
SIL	AYNO	00 1	NTERIM NJVI	STOR Is	AGE	SITE	-	COMPANY	B .			N800,E1	300			ANDLE	FICH HINE. 90°	N/A
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ar þ	AYNO	00 II	ITER]	IN S IVIS	TORAG	E SIT	-	COMPANY TES					1000,E14	00				AMBLE	Files 1 90		N/A
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nt ji			ITERIN NJV	ST		-		CONTINUET	3				N700,E1	400	<u> </u>	1		1 Filen 1 90 ⁴		N/A
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			OGIC					CONTRACT			F	USRAP			1454	1-138	I OF 1 FROM HERE.	MISS-246
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Į				ğ=	3			97.7		1	2							CHARACTER OF MILLING, ETC.
NUCER, 6°, THROUCHCUT.								97.2	5			STRATE TO NED		SAND (SM HONZON MED WITH	DANK 21 FINE RTELL POOR GRASS RDC COLOR 4 MOSTLY F 2022 ROLM	TTS AND	STTE RADII CONT EBER ANNA CONT	CHECKED FOR MACTIVE ANDIATION BY LINE YTICAL ORATION
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CEPE	NECENI N	DINE 1. VA	73	C	n/a	s sain N/		INF OF CA		(1801) 9	n.		MPTH/E	5.5'/				VEL. THP O	7 NGEX /A
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25	-		z iz.								Γ				<u></u>				E5. (21)
			AND TANK				ELEVAN		MMIC LOC				NESCRIPTI	III AND (LAN	FICATION (•		-	IR LEVELS, IR RETURN, MCTER #
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								10		• • • • • •		SLIGHTL 15-5.57 BLACK 567/72 PLACE POSSIBL	Y MOST	SIL I OLL-C OLS-LO PA LENSES, SO S ORGANICS NG ZONEL I	LE GRAYE LE GREED FT; DEDIS OIST.	H E N		EBERLIN ANALYI CURPOR PEDEOR LOGGING	CAL ATTON MED GANGA
							87.1					5-75': 55-75': 510-75-10 75-10.0' 101114/2	IR STRA IED AT LIGHT (MEDILM 1 DARK) 2 FINE 1	SAND CAN THED NOTS 6.5 FT. CLIVVE GRANEL YELLOWISH I TO COARSE E AT ELD	t to 1 (5)15/2 Brown Gramed.			•DESCR	PTION AND ICATION BY
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AUCER, 6', THROUGHOUT.								9	3.6				5988884		SH BHO NAL PE DCC/0 WT(H C POORL FT) AN BRICK A	SILL OF CES OF SANDSTI CCASION Y SORTI D ORGAN NO GLA SAND CS SES CO FILE TO DELISE		ITH REDOISH DSTLY FI REES AN RC ROOT TY PRECES			CONTAN CONTAN EDEFILIN ANALYT CORPOR ENERLIN ANALYT	
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	G	EO	100	X	DR		LOG		FR8.85 .7		F	USRAP	<u>.</u>			1-1 38	I OF 1	HILE MA. MISS-249R
L			N	UVI:	<u>S</u>	E SIT	E -	COSTORAT	L.			N900,E1	500			ANDLE	Film Hitter. 90°	BEARDIS N/A
1/2	1 8/16		1/28/				NORE 1 CHORENT	RENCH AL SERV	iœs	M		e ener. E 8-33		HOLE SHE	046381.080		0.0'	TOTAL SEPTS 5. 0'
C	NECON	DHF1 VA	<i>.</i> 79			i danes N/A	SAFL N/J		p of cas N/A	- (• • . 7. 9'		NCIE	UNITER OBSERVED		SEPTINE, TE	P OF NIECK. N/A
5.00 0	LE MAN					CAR		N/A	ABEN	J.			h	D.	. NCGRANE		_	
ANT LIANS ON		THE RECEIPT			•				Ē	MARE LOS	J			M AND CL.	AFEFICA THEM		1 1	NUTES CON In THE LEVELS, In THE RETURN,
33	35	3			N N N		¥=5	97.9	0	2								Children Ter of Million, Etc.
NUCER, 6', THROUGHOUT.								92.9	5			REDUSH REDUSH GRANED PENELES POORLY RDOTS FT. DECO	EFFCMIN WITH M AND G CONSOL MD ORG MPOSED	AND (SA NEROLS AVEL: PO DATED N ANELS N SANDST	THE TO MET SAMOSTONE SAMOSTONE UPPERMOST UPPERMOST ONE; DRY TO	ALM ASS OJ	ANAL	CHECKED FOR JACTIVE AMBIATION BY LINE YTICAL ORATION
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SITEN	AYNDO	ND IN	ITERIN	I ST(VIS	ORAGE	SITE	-	COMP		5			N1900,E	1500			2.1000	Filin 1 90		SEARCE N/A
7/2			/28/8	2	-		NORET						E 8-33		HELE SEE	0.00		MICK (71J 2.5'	TETAL SEPTE 2.5'
					CONE	LAVIA MONEL VA		5 1	LTP	er cale N/A			a.). 7'	SCPTN/C					-	
S.M.FL		0 1	11 774	1	<u> </u>	Criffe					I			P h	D.	NCORNE		.		
		5	at be	Τ								Π	.							CL 300
SHELL THE ON		TIGNED TO THE T	NUCET CH				2	2.57	* 1994	ž	PNINC LOG	Ż		HESCHPT	an 460 a.	NGEFICATION *			1841	UR LEVELS, UR HETLER, Recter of
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CHOUT.																ANELLAPED ANELLAPED NED, TOTAL WEATHENED NSOLDATED D AND CEMENTED TE AND OF				
			<u> </u>	+				97	1.2	2.5	* <u>*</u> .	Н	SPOLS LOOSE	CONSIST SOFT, S	OF LINCO	NSOLIDATEL D AND	SANDST	me l	EBERLA ANALY CURPO	E.
LUCER, C., THROLOHOUT.										5 -			I WANTL	קרנש שת	ASS ROO FT. DRY.	IS AND UN	MICS	Ď /		
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			OGIC					FR0.857		F	USRAP			14501	-138	I OF 1	NILLE NO. NISS-251R
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7/2	i 1/16		1/28/86				RENCH AL SERV				HD HIDEL LE 8-33		HELT SHE	0.0		1.0"	TUTAL BEPTH
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	CAN'N REAL		AND I LINK	豊고국		¥=	ELEVATO	2	BNARC LOS	Tens.		ESCHP1	in an 6.4	SFILATION			NATUR PETHON, CANDINGTER OF MELLING, ETC.
5				ST.P.		m ř	100.7 99.7				0.0-10-	1 200	152) 51				
ALCER, 6', THROUCHOUT,								5			PIRE 10 DECOMPC SPOILS (LOOSE), MODERAT GRAVEL; LPPERMO BOTTOM	NED TO SED TO SOFT, S ELY HA FEW GR ST 0.5	GRADIED: OF LINCON ALTY SAND ND, WELL (ASS ROOTS FT. DRY. E AT LD	IDTALLY EATHERED: A SOLIDATED (SHD AND) ZEMENTED S S AND ORGAN	NUCER ANDSTO NUCS IN		CHECKED FOR DACTIVE ANIMATION BY LYTECAL FORATION FORATION FORMED GAMMA
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			100, 57-000 P-1717(100)		6		Ł	35 -	NI DC		N STORAG	E SITE	-				NISS-251R

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			OGIC					CONTR				F	ISRAP			1450	1-138 TABLE	FINDE P	OF 1	NISS-252R
			IVLN	S									N1200,E	580				90		N/A
1/2			/28/86		E		NORET						e 19-33		HALE SEE	2. (NDCX (1.5'	TETAL SEPTE 3.5'
L				-	ine i N/		San L		- 19		•		9 EL 10.5'	167714/5	NONE (NTER BSERVED			2.0'	F NECK /38.6'
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6°, TH				_	+			97	.1	3.5			SANDST		NUMEROUS IVEL.	PECES OF				
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COPE	NECOM		/B	te		MIL	Sant.	8	Q_ 10P	N/A					8677N/8	NCHE	INTER OBSERVE	ED.	TU/EL. THE C	F NACE
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			ida, ST-ida P-FIT (2006)			•		TTL.	M	25 - 30 - 35 -				sto ra e Is	ESI	ITE -					1	* DESCI CLASS VISUU TION	MPTICH AND SPECATION BY L EXAMPLA- OF CUTTINGS MISS-256R	



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AUGER 6	ļ			\downarrow			<u> </u>	1	93.9	4	5		Ľ		DENSE	LO-13	1,005£) (1 FT); MOIS	UT CLAY	LT AND				
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7/1	1/16		/30/16		ii u		NORET	RENCH AL SERVI					e etet. .E 8-33		1.01	SHE L'	5.0		ROCK	FL) 0. 5 ⁴	TUTAL SEPTU 5.0'
	HECONG.					NOTES.	SAMPL	CS 61_ TO	-				0 R. 8, 8'		VE. 90			-			
5.00														Ph					<u> </u>		
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ER. 61, THROUGHOUT.								93.8	5	-			CONSO		0 (005 3 FT); 1	UBI OSI.	CLAYEY	D			
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	BOTTOM OF HOLE AT 5.0 FT. AUGER SPOILS WERE NAMEDIATELY REPLACED IN THE HOLE.																				
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ITE N	AYNO	00 11	TERIN :		RAGE	E SIT	E -	ľ	CONTRACTO	3				N1500,E1	386			AMOLE	Fildul I 90 ⁴		N/A
5 7/3	1/86		ALETED /30/86						ENCH L SERVIC					e 1896. E 8-33		HOLE SEE	OVER.000		NOCK (0.0'	TOTAL SEPTH 5. 0'
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Į	SAFLE ANA		ADACTA	3	-3		摸ᆂ	5	96. 8	0		2	•								CALTER OF
WGER, 6', THROUGHOUT.					Te	<u> 248 F</u>			94.8	5				BROWN SOFT-PO NAMERON ORGANIC ZJO-SJO STRATIF		SAND (SHA HORZONS HORZONS SAND (SHA HORZONS	ED (LOOSE) FTI AND COLOR FIDE TO OFLY	TE		SITE C RADIDA CONTAI HOLE G BY EDE ANALY CORPOR	ECKED FOR CTIVE MATION AND ANNA LOGGED REINE ICAL VATION.
NUCE									91.8	10 15 29 25 30		•[•]•		2.0-4.0 001N6/0 4.0-5.0 001R4/2 BOTTON	DATED DARK DARK DE MOST OF HO	ILOUSER MA Yellowsh Yellowsh Ly medium Le at 5.0	ORANGE BROWN GRAMED	LACED		* DESC CLAS	
	39-57		6426; 57=68				<u> </u>		ł	35 NAYN		111	ER	IN STORA	E SIT	E -					OF CUTTINES.
			MICHE										N	JVIS -49		-					NISS-263R



GEOLOGIC DRILL LOG	PREASET	FUSRAP	14561-138 1 OF 1 MISS-264R
SHE MAYNOOD INTERIN STORAGE SITE - NJVIS	CONTRACTES	N1460,E1200	ANDLE FREM HENEL. BEADING 90° N/A
ACAME COMPLETED ANALLER MORE 7/30/06 7/30/06 ENVIRONMEN		VE AND MENTEL MOLE SHE OVE OBILE 8-33 6°	INLINE (T) NCK (T) TUTAL MPTH
CARE RECONDINIFT./20 CARE DONES SAM		Mano E. (CP11/G. Cause SATER 98.5' 8.0'/90.	S' N/A
SAUPLE MANAGE NEDBYT/TALL CARDS LEF	'N NELS DAALDETH N/A	LOUD IN D. McGR	
		BESCHPTIGH AND GLASSFIC	
	99.5 0		CANNETTER OF DRALME, CTC.
AUGER, C', THROUCHOUT.	98.0	CLO-CLS': SANDY SET OLE MOD PROWN CSYRL/QFBE GRAMED POORLYCONSOLIDATED (LOOSE); GRASS ROOTS AND ORCANCS; C.S. DO'SELTY SANDYSMOLOLO SOIL HORIZONS; FINE-COARSE POORLY SORTED; POORLY CONS (LOOSE) WITH A DENSE CLAYEN O.5-2.0': DANK REDOSH BROWN CLAY BINDER; FINE TO MEDILM FEW ORGANICS. O.5-2.0': DANK REDOSH BROWN CLAY BINDER; FINE TO MEDILM FEW ORGANICS. O.5-2.0': DANK YELLOWISH ORA (DYRK/G); FINE TO MEDILM GR 6.0-0.0': DANK YELLOWISH BRO	INFST. HOLE GAMMA LOCCED R STRATIFIED GRAINED, COLDATED / ZONE. I OOF3/40, GRAINED; LO FT. NOE LO FT. I OF T. I OF T.
	88.5 10 - 1111 15	BOTTOM OF HOLE AT ELO FT. Auger spols were namediate in the Hole.	
SI-OPLE SPOND ST-ORLEY TUBD P-CENNING P-PERCED P-PERE	NE NAYNOOD IN	TERIN STORAGE SITE - NJVIS	INLE IN. HISS-264R



			OGIC						•			F	US	RAP				1-138	SHEET I	OF 1	HILE HA. HISS-265R
SHE N	AYND	00 1	NTERIN NJV		ORACI	E SITI	E -	COMP	INNTES				NI	300,E1	200			Anna	Film : 90		N/A
1/3	1 1/16		1/30/86	5			NDRE	TRENC		1	in. w			8-33		HILL SHE	04580.000		RECX	ет.) 9.9'	TOTAL MEPTS 5.0'
CEPE	NECON	JANE I.	Л 0			NONES VA	Salar I			of call VA			9. 1		SEP TH/E	NONE	OBSERVED			VEL THP (VF NOCK V/A
SAUPI			1997 / A.	L	.	CAR			6 80.A	DETH			ľ		h	D.	NEGRANE			-	
	THAN THE WORL	- TOTAL	MALL ROLL		M			ELEM	A THÈN	5	DAMAGE LOG				NESCUP II	III AND CL	NSSIFICA THEM ⁰				RES CON RER LEVIELS, RER RETURN, MACTER OF
	319	퀽러	a ne					33).1	0									·		
NUCER, 6", THROUGHOUT.								99	.8 1.1	5				13-5.0° TRATFI EDLM CONSOLE 13-1.0°: 12-5.0°: 0-5.0°:	GRAMED DATED (MODERA F DAAK SANDST(DARK Y)	HURZOR SOFT: PI COSEL M REDOISH REDOISH E GRAV	I (SYR3/4) U Brown El. Brown			STE C RADIDA CONTA HOLE G BY ED ANALY CORPOR	ECKED FOR CTIVE MATION AND AMMA LOCCED RLNE ICAL LATION.
R										10				OYR4/22 Teneles Intern	OF HOL	ROMAL RO E AT 5.0	INDED GLIAR		/		
										15 -											
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								71		39				P 4 4 4 4 4						CLASS Visilia Tion	uption and Spection by L examina- of cuttings.
						•			M		IU IN	<u> </u>	J N]	STORAG IS 51	E SITE	-					USS-26-3R



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			OGIC					PROJECT		F	USRAP			14501	-138	FINE H	¥F 1	NISS-266R
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7/30			1118 /30/16			NORET	RENCH AL SERVI	- F	NUL NO	_	E 8-33		HALE SEE	5.0		1	0.0'	TUTAL SEPTS 5. 0'
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8/4/06 8/4/06 EINVIRONMENT COME NECONERNY TU/20 COME NOMES SAMPL N/A N/A N/A	TRENCH MOBILE MO	HER. HER.E SEE OVERLASSIN #1.0 NOX. B-33 6" 5.0" NOX. INPRIVE SEPTINE SEPTINE SEPTINE	HERE. BEARDS OP N/A TOTAL BEPTH 0. 0' 5. 0' N/G THP OF RECK N/A
8/4/96 8/4/96 ENVIRONMENT CORE SECONDENT/L/D CORE NOTES SAMPLE N/A N/A N/A SAMPLE MAMER HOURT/ALL CORE NOTES SAMPLE N/A N/A N/A N/A N/A N/A SAMPLE MAMER HOURT/ALL Core Notes N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	TAL SERVICES MOBILE LES CL. TOP OF CARDING DI A N/A 100.0 II HILLE DA. ALBORTO	B-33 6° 5.0' L BPTN/CL STAND SATER 0' NDIE OBSERVED CHIEP Ph	0.0' 5.0'
	A N/A 100.(0" NONE OBSERVED	WAL THE OF RECK
			NIFTES CAN UN THE LEVELS,
AUGER, G., THROUCHOUT.	100.0 0	SCICUPTION AND CLASSIFICATION"	UNITER RETURN, COMMETER OF BRELON, EVC.
\$		O-O.3': ASPHALT. 3-5.0': S. LY SAND (SMB DANK DDOSH BRUNN (DR3/4) FINE TO MEDILM RANED SOFT: WITH MAERICUS PECES OF ODERATELY HAND, POORLY TO WELL EMENTED SAMDSTONE GRAVEL: POORLY DRSOLDATED (LODSE); DRY; DECOMPOSED ANDSTONE.	SITE CHECKED FOR RADIDACTIVE CONTAMINATION, AND HOLE CAMMA LOGGED, BY EBERLINE ANALYTICAL CONFORATION.
		UTTON OF HOLE AT SLO FT. LIGER SPOILS WERE MANEDIATELY REPLACED THE HOLE AND THE HOLE WAS RESEALED TH ASPHALT.	ELEVATIONS ESTABLISHED RELATIVE TO AN ANIITRARY DATUM.
SI-SPLIT SPORE ST-SIGLINT THESE ST			MLE III. HISS-274R



EART FLAN TOOLD INTERNAL STREE Committee N1344, E1 449 And Team Proc. <								LOG		7	0.007		F	USRAP			.458 18. 14581	-138	I OF 1	MILE ML. MISS-275R
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Image Image <th< th=""><th>MALL Y</th><th>10.00°</th><th></th><th>L'R.M.</th><th>LUNK</th><th>•</th><th></th><th>T</th><th>ELEWI</th><th></th><th>E.</th><th>8 2</th><th>3</th><th></th><th>BESCHPTR</th><th></th><th>ISFICATION®</th><th></th><th></th><th>MAR LIVELS,</th></th<>	MALL Y	10.00°		L'R.M.	LUNK	•		T	ELEWI		E.	8 2	3		BESCHPTR		ISFICATION®			MAR LIVELS,
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	G	EO	LOGIC	DF	ALL	LOG		PROJECT	•	F	USRAP			14561	-138	DELT IN. 1 OF 1	HILT HE. HISS-276R
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NUCER. 6°, THROUGHOUT.					ST P		3	<u>99.4</u> 94.4	0			do-oly Redotsh Graned WoolfRaft Consol Sanosto		LAND CANE DORS / 40, FI RD, POORLY STONE GRA LOOSED, DRY	E TO MED US PECES TO WELL EL: POOL DECOMPOS	Y ED	STTE C RADICA CONTA AND H LOGGE EBERLI ANALY	CINE CINE INATION ILE CANNA J. BY
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GEOLOGIC DRILL	_OG		RAP		I OF 1	nill.r nil. N1SS-279R
SHE NAYNOOD INTERIN STORAGE SIT	- COMPONITES	N	1900,E 300	ANNLE FI	101 HINE. 50°	N/A
11.1111 CHAPLETHE SHELLEN 8/4/86 8/4/86 ENVIR	NORE TRENCH DIDENTAL SERVICES	HEL WIE AND		10.0'	0.0'	TUTAL BEPTH 10.0"
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	¥=5		DESCRIPTION AND CLASHIFIC	a 70 00 ⁰		R LEVELS, R RETURN, NOTER OF JAR, CTC.
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SI-APLE SPORE ST-ARELIN THE D-BORNER P-FITCHER 0-011ER	STE NAY	NOOD INTERIN	STORAGE SITE -		IIILE III.	155-27 5



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	G	EOI	OGIC	; [)RI	LLI	100		_			F	US	RAP			1450	1-138		DF 1	MILE MA. MISS-624R
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	1/87	2	1/24/87			NORE			NV. SEI	v .		a	E-	55		HALE SHE	10.		ł). 9'	TOTAL DEPTH
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ATT 1	SHELE AVAIL	- ACCORT	L R M			TESTS			LEVA THEM	· NA	Durne: Los	Tent			EICHPR		FICATION®	·			US CHE UR LEVELS, UR ALTUBA,
12	弼			3	- 3		¥ z	5		0	3										RACTUR AF LAR, EYC.
6' AUGER				CLO-CLY: ASPHALT, CLO-CLY: ASPHALT, CLO-CLY: GRAVEL; LO-ZLO, LO-CLO': SELTY SAND CSM. FILL AND NDIGENOUS MATERIAL (2.0-R.07), COLOR STRATIFED, FINE TO MEDILAN GRAINED WITH FEW TO NUMEROUS PIECES OF SUBANGULAR - ROUNDED GRAVEL OF VARIOUS LITHOLOGIES; SOFT; UNCONSOLDATED; SOMETIMES CLAYEY (SC-ON), MOIST TO SATURATED AT 5.0'. LO-2.0': MODERATE BROWN; FEW ORGANICS; FILL? 2.0-ID.0': DARK YELLOWISH BROWN GOTR4/23; DECOMPOSED SANDSTONE. 10 BOTTOM OF HOLE AT IOLO FT. AUGER SPOILS WERE INMEDIATELY REPLACED N THE HOLE, 2/24/87.														SITE CI RADIDA CONTAL	MATION AND ANNA LOGGED RLDE TCAL		
										15 20 25 				uger si	Poils II Ole, 2/	ERE MMEDU 24/87.	ATELY REP	LACED		CLASSE By VIS NATION	PTION AND Fication Lial Exami- OF Cuttings, Available,
			64, 57-616 MPTFC362h			•				<u>35</u>	- N.J	. 1)	SPI	ECTION	STATI	CIN				<u>ir 16.</u> 1	155-624R



	G	EÔ	.OGIC	Df	RILL		.0C		-	LIET		F	USRAP			Jan 14. 14581	-130	SHEET IND 1 OF		HOLE HA. NISS-625R
SITE	ISS .	- N.,	J. INSP	ECTI	on s'	TATI	CN	COMPA	NTES				N1890,E1	307			ANNULL	71011 HUR 90°	2.	NEARDE N/A
2/2	i 4/87	1	ALTO /24/87		ille M	ORET	RENCH	ENV.	SEIN.	•	REL MA		10 11000. E-55		HOLE SHE	OVERLAND		NHCK (***). ().		TETAL BEPTH 10.0'
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5.007						-	S LET	N HELE					LONG P	1 ħ	<u> </u>	CGRAVE		<u> </u>		
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THE DWAY	AND ADA			i z	1	1	¥ = S	BLEVA			BANKE LOS	Ţ		BESCRIPT.	ini and clas	NFICA THEN"				UR NETHON, Inctur of Lunk, ETC.
6. AUGER										5 10 15 20 25			NDIGENO COLOR S GRANED SUBANGL LITHOLOU SOMETMI SATURAT OLO-2.0'S NUMEROL ORGANCS HORIZON 2.O-IOLO' GOYR4/2 BOTTOM	US MAT ITRATIFI WITH FI WITH FI WIT	SAND (SHL ERAL (2,0- ED) FINE - 1 EV - NUMED ROUNDED G FT: UNCONSI YEY (SC-ON S. ROOTS II REED UPPEI YELLOWSH (POSED SAN LE AT IOLO D. MAEDIATI 2/24/187.	10.0%. MEDILM ROLS PIECE: RAVEL OF N OLIDATED; ; MOIST - (SYR3/40; D.0-0.5% AN R SOL BROWN DSTONE. FT.	D		ESCRED TATE CI TATE CI TATE CI TATE SUBJECT TATE TATE TATE TATE TATE TATE TATE T	INATION AND AMMA LOGGED TRLINE
			000) 51-50 P-PFC205					TE.		<u>- 85</u> - 221	- N.J.	. 19	GPECTIO	STAT:	[(]))				<u></u>	1155- 625 R



	(ÆO	LOG	C	DRI	LLI	LOG		-			F	USRAP			14501	-1 30	SHEET HEL	HELE HEL HISS-626R
SIT	MISS	- N.	J. INS	PEC	TION	STAT	ION		-				N1935,E1	475			ANDLE	Film Hiller. 90°	N/A
	4/17		1/24/8			NORE"	TRENCI	ENV.	SERV	.	MEL M		B 1198		HELE SHEE	OVERLAND		NCL (1)	TETAL BEPTH 9.0'
CIPE	NECON		<i></i>			VA VA	Salf		L TOP C	F CHA	-		6 Q.P					SEPTIME. TH	P OF NECK
Sing			CDA / / /	<u>u</u>		CAG		N MALE						l /i	D. 1	CORNE		· · · · · · · · · · · · · · · · · · ·	
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6" AUGER										5 -			NDIGENCL STRATIFI FEW - N ROUNDED SOFT: UN (SC-ON); I 0.0-2.0': ORGANICS HORIZON? 2.0-9.0':	IS MATI ED; FINE GRAVE CONSOL WOIST - MODERA ; FILL O DARK Y	- NEDILIN S PIECES O L OF VARIO DATEDISONI SATURATED ITE BROWN	9.0%, COLOR GRANED W F SUBANGU US LITHOLO ETMES CLA AT 5.0%, (SYR3/40; F ED UPPER 5 ROWN	TH LAR - NGESI NTEY		₽ 2/24/177
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			J. INSP	EC1			CIN .						N1640,EI	400				Films 148 50°		SEANDS N/A
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SHE							1	U MLL M N/A	L		L	•		 Wh		ICERNE		L		· · · · · · · · · · · · · · · · · · ·
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AND PARE TYPE	Then we a			g z	3	1	¥=5			_	ł	2								NCTER OF LINK, ETC.
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Γ						6 ,	ľ				- N.J	1. 1	INSPECTI	DN STA	TIGN			ľ		NI 55-628R



	G	EO	LOGK		DRI		. O G		-	T	F	USRAP			1450	i-1 38	I OF 1	MISS-629R
SALE 1	155		J. INS	PECI	TION	STAT	i on					N1763,E1	395			ANNULL	FREM HERE. 90°	N/A
2/2	1 5/117		141.2789 2/25/81	,		INCRE 1	RENCH	ENV. SE	ERV.		a	10 1110. E-55		HOLE SHE	OVER.000		NCL (T) 0.0"	TOTAL DEPTH 7.0"
		VA				MANES VA	Sart.		P F C N/A	dans.		• D. ⁹⁴		4.0				of neck N/A
2.00				L	A	CAB		N/A		0			h	D. 1	CORNE			
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G' AUGER									5			NDIGENO STRATIFI FEW - N ROUNDED SOFT: UN SOMETIM SATURAT Q.O-3.5': NOTTLED	ED: FINE ED: FINE GRAVEL CONSOL ES CLAY ED AT MODERA GRAYES	- MEDILM S PIECES (L OF VARK DATED; 'EY (SC-OH 4.0 FT. .TE BROWN H BLACK (7.0% COLO GRANED W XF SUBANGU XUS LITHOLO II; MOIST - (SYR3/4); N2;; NUMERC	ith Lar - Xges;	SITE RADIO CONT	7 2/25/87 Checked For Active Mination and
									10			NDED FI 3.5-7.0': DOYB4/22 BOTTON HOLE BA	LL AND DARK Y DECON OF HOLI CITELLEI POILS A	STREAM SI Ellowsh e Posed San E at 7,0	IDSTONE. FT. Ely with C		BY EL	GAMMA LOGGED Erline Tical Ration
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		E0	LOG	IC	DR		LOG				F	USRAP			1450	-138		DF 1	NILL IN. NISS-630R
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2/2	n 15/87		2/25/			HORE	TRENCH	ENV. SEA	v .	Dilli an		e-55		HALE SHE	5. (ГТЈ 0.0'	TOTAL OUPTR 5. 0'
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5.44	LE ING		EBK /F	ALL		CAS	NG LIPT	N HELG DA./					<u></u> h	D. N	CERANE		L		
	SUCH ANNE		THE REAL		, 1 2 2 2		¥ = 2	E.Eva Tata	7	Counce Los	Ĩ		BESCHPTH	1 1 110 (1.10)	FICA THEY				3 CON R LEVELS, IR RETAIN, NETTER OF AND, ETC.
							1° 3 1		0 5 10 15 			NDIGENO STRATIFI FEW - N ROUNDED SOFT: UN SOMETMI SATURAT 0.0-0.5': NUMEROL 0.5-5.0': COYDAL/22 BOTTOM	US MATI ED: FINE Incensul Incensul Es clay fed at Modera Is grass Dark y Is decom OF Holl Crifulet	TEY SC-ON 5.0". ATE BROWN S ROOTS AN ELLOWISH B POSED SAM E AT 5.0 F D IMMEDIATED	5.0%. COLO GRANED W F SUBANCU US LITHOLO ; MOIST - (SYR3/40; NO ORGANI ROUN DSTONE T.	TH LAR - NGESy XS.		SITE CHI RADIOAC CONTAM	ARLETIC.
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	NECOVI		~			MANES VA	SINFL N/		N/A		•		0 Q. ³⁴		10-11/5	4.0				AL THE C	
Sar						CAR		N HALLS IN		1	1		LOBO		<u></u> h	D.	NCERANE		L		
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S AUGER				S		200 9			5				NDIG STRA FEV ROLN SOFT	ENOL TIFE DED UN	ES MATE ED; FINE GRAVEL CONSOLI ES CLAY	DINE GLO- - MEDILM S PIECES L OF VARI DATED; EY (SC-0)	FILL AND 5.0%, COLOI GRANED W OF SUBANGL OUS LITHOL(H; MOIST -	Th Lar -			¥2/25/17
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	C	EO	LOGIC		DRI		100	;	ľ		•	_	FU	SRAP				L 1-138	Sector 1	INCA. OF 1	NELE ME. NISS-632R
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6" AUGR.										5 -				NDIGENOI STRATIFI FEW - N ROUNDED SOFT; UN (SC-OH); 0.0-L0': NUMEROU FILL?	US MAT ED; FINE GRAVE Consol Moist Modera S Gras	ENAL ALD - MEDILA IS PIECES 1 OF VAR DATED; S - SATURA' TE BROM S ROOTS	L FILL AND -7.0% COLO I GRANED I OF SUBANG HOUS LITHOL DIMETIMES CL TED AT 5.0% I CSYR3/4D AND ORGAN	ITH ILAR - Ogiesi Ayey CS.			¥2/25/87
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			an 51-1 Million)	87	L			N.J.	INS	PECTION	STATI			- <u> </u>	I LON	NJSS-633R



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ant I	(] \$\$	- N.	J. IN	SPEC	TION	STAT	ION	Cas		k				N1776,EI	203			ANNALE	Files (BEARDS N/A
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			111	u.		CAS	16 LITT					I			h		CORANE				
TAN' TIME	LAPT, D. M. R.	THE REPORT	RACEN CAN	LOWER	P	WATER ESTA			00 71.71001	ž	MAR LA						FEATION ®				ts das Br Levels, Br Hernin,
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6' AUCER.									5			INDIGENO STRATIFI FEW - N ROUNDED SOFT; UN (SC-OND) 0.0-LO'1 MOTTLEI GRASS I LO-4.0'1	LIS HAT ED: FINE LINEROL ICONSOL MOIST MODER/ O GRAYI ROOTS / DARK R	: - MEDILM IS PIECES (ID OF VARIO ID ATED; SOI - SATURATI ATE BROWN SH BLACK (ND ORGANI	7.0%. COLOR GRANED WIT IF SLEANGLE NUS LITHOLO METMES CLA ED AT 4.0%. (SYR3/40) N2% NUMERO	in Lar - Gies _i Lyey		¥	2/75/87
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6' AUGER.				£	7 F		30 Ē			5			NDIGEN STRATI FEW - ROLINDE SOFT; L (SC-OH) 0.0-6.0 WOTTLE GRASS OCCASI ROLINDE	DUS MAT FED; FIN NUMERON D GRAM NCONSOL ; MODER D GRAM FLOOTS (DIAL PEED D PEBBL	ENAL (4.D) E - MEDIUM IS PIECES (IDATED; SO - SATURATI ATE BROIN SH BLACK (0.0-0.57 M CE OF GLA ES 65.5-64	FILL AND GRANED W GRANED W OF SLEANGU OUS LITHOL(METMES CL. ED AT 6.5'. I (SYR3/4); OZ; NLMEROL O ORGANICS SS; NLMEROL D'; FILL AND	ith Lar - Dries: Ayey NJS Is		RADIDA CONTAL HOLE (BY EBI ANALY	ENATION AND GANNA LOGGED ERLINE
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			Park ST-C							N1SS	- N.	J. :	INSPECTI	on sta	TION					NISS-636R



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	RECOVE	_			MARES VA	SAUFLI N/A		199 (8) N/	F cuint	•) R H		4. 0*				EL. THP O	A NOCK
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Statut steen strend at the NISS - N.J. INSPECTION STATION HISS-640R		20	2/26/87.	* DESCREPTION AND CLASSIFICATION BY VISIAL EXAM- NATION OF CLITTINGS. ** NOT AVAILABLE



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