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Formerly Utilized Sites Remedial Action Program (FUSRAP)

ADMINISTRATIVE RECORD

for Maywood, New Jersey

U.S. Department of Energy

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Formerly Utilized Sites Remedial Action Program (FUSRAP)
Contract No. DE-AC05-81OR20722

RADIOLOGICAL CHARACTERIZATION REPORT FOR THE RESIDENTIAL PROPERTY AT 14 LONG VALLEY ROAD

Lodi, New Jersey

September 1989

Bechtel National, Inc.

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RADIOLOGICAL CHARACTERIZATION REPORT FOR THE RESIDENTIAL PROPERTY AT 14 LONG VALLEY ROAD LODI, NEW JERSEY

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Prepared for

UNITED STATES DEPARTMENT OF ENERGY
OAK RIDGE OPERATIONS OFFICE
Under Contract No. DE-AC05-81OR20722

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ABBREVIATIONS

cm	centimeter
cm^2	square centimeter
cpm	counts per minute
dpm	disintegrations per minute
ft	foot
h	hour
in.	inch
km^2	square kilometer
L	liter
L/min	liters per minute
m	meter
m^2	square meter
MeV	million electron volts
μR/h	microroentgens per hour
mi	mile
mi^2	square mile
min	minute
mrad/h	millirad per hour
mrem	millirem
mrem/yr	millirem per year
pCi/g	picocuries per gram
pCi/L	picocuries per liter
WL	working level
yd	yard
yd^3	cubic yard

1.0 INTRODUCTION AND SUMMARY

This section provides a brief description of the history and background of the Maywood site and its vicinity properties. Data obtained from the radiological characterization of this vicinity property are also presented.

1.1 INTRODUCTION

The 1984 Energy and Water Appropriations Act authorized the U.S. Department of Energy (DOE) to conduct a decontamination research and development project at four sites, including the site of the former Maywood Chemical Works (now owned by the Stepan Company) and its vicinity properties. The work is being administered under the Formerly Utilized Sites Remedial Action Program (FUSRAP) under the direction of the DOE Division of Facility and Site Decommissioning Projects. Several residential, commercial, and municipal properties in Lodi, New Jersey, are included in FUSRAP as vicinity properties. Figure 1-1 shows the location of the Lodi vicinity properties in relation to the former Maywood Chemical Works.

The U.S. Government initiated FUSRAP in 1974 to identify, clean up, or otherwise control sites where low-activity radioactive contamination (exceeding current guidelines) remains from the early years of the nation's atomic energy program or from commercial operations that resulted in conditions Congress has mandated that DOE remedy (Ref. 1).

FUSRAP is currently being managed by DOE Oak Ridge Operations. As the Project Management Contractor for FUSRAP, Bechtel National, Inc. (BNI) is responsible to DOE for planning, managing, and implementing FUSRAP.

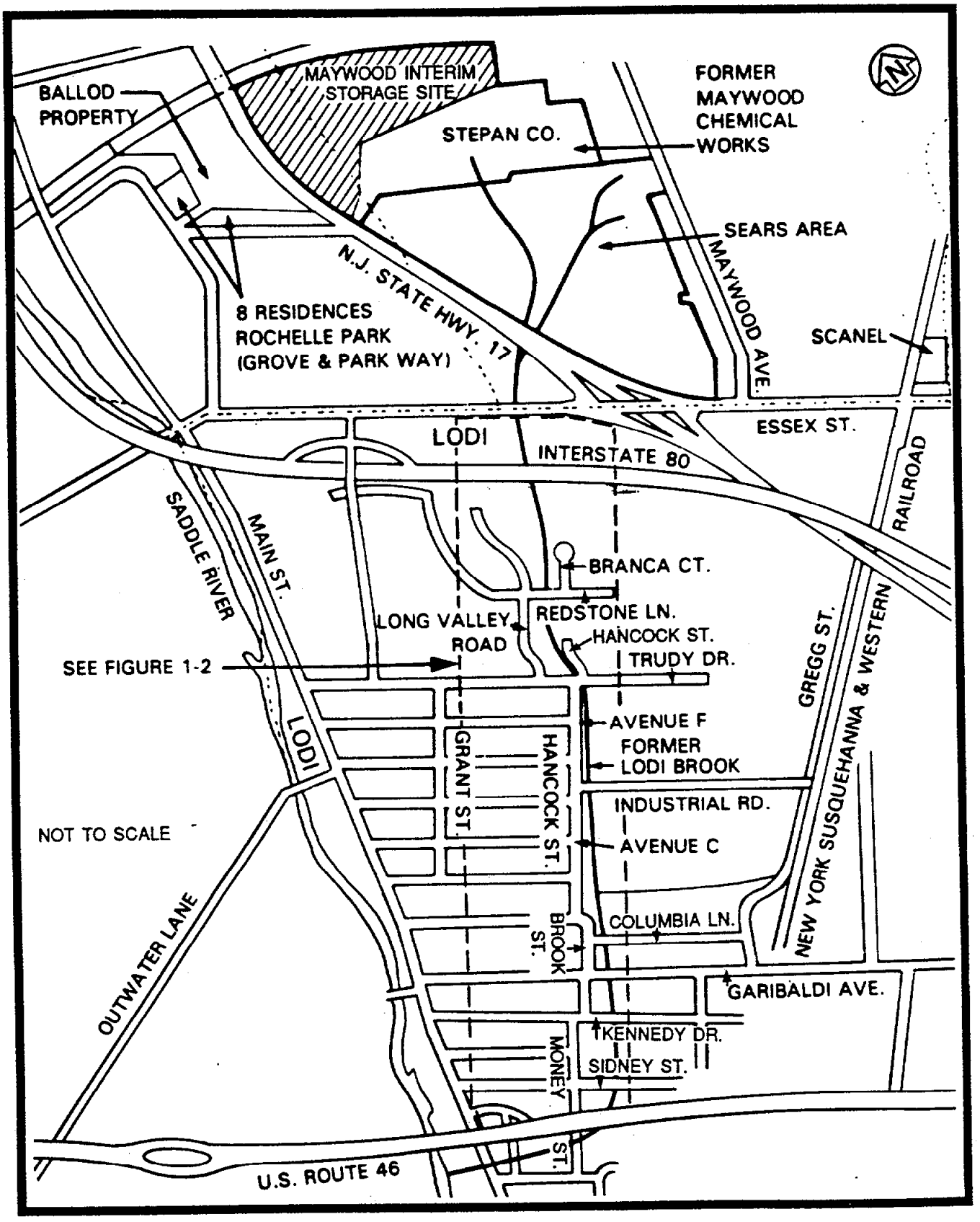

FIGURE 1-1 LOCATION OF LODI VICINITY PROPERTIES

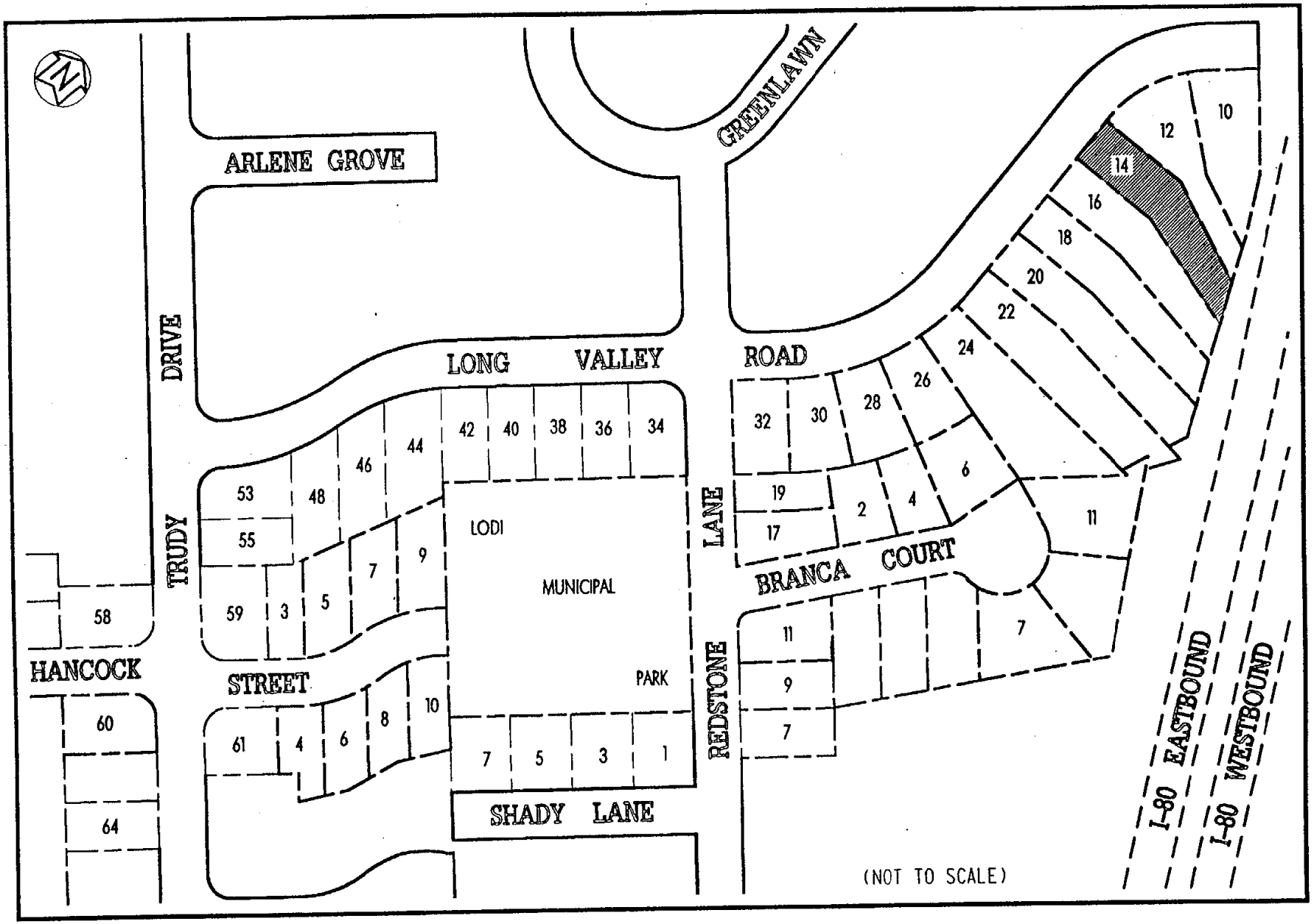

FIGURE 1-2 LOCATION OF 14 LONG VALLEY ROAD

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considering potential adverse health effects that might occur in the future from any residual contamination. The dose contributions from uranium and any other radionuclides not numerically specified in these guidelines are not expected to be significant following decontamination. In addition, the vicinity properties will be decontaminated in a manner so as to reduce future doses to levels that are as low as reasonably achievable (ALARA) (Ref. 2).

Soil analysis data for this property indicated surface contamination. Subsurface investigation by gamma logging indicated contamination to a depth of 0.30 m (1.0 ft).

Exterior gamma radiation exposure rates ranged from 5 to 49 μR/h, including background. No indoor measurement was obtained because access to the residence was denied by the property owner.

No interior measurements for radon and its progeny (radon and thoron daughters) could be obtained.

All data tables for this property appear at the end of this report.

1.4 CONCLUSIONS

Evaluation of data collected, analyses performed, and historical documentation reviewed indicates the presence of radiological contamination on the property located at 14 Long Valley Road. This contamination is both surface and subsurface contamination. The subsurface contamination ranges from depths of 15.2 cm (6.0 in.) to 0.30 m (1.0 ft). Near-surface gamma measurements indicated an isolated area of surface contamination indicated near the southeast corner of the residence. The total affected area is estimated to be

approximately 10 percent of the property. These conclusions are supported by documentation that establishes the presence of the former channel of Lodi Brook in this area. This channel is the suspected transport mechanism for the radiological contamination.

2.0 SITE HISTORY

The Maywood Chemical Works was founded in 1895. The company began processing thorium from monazite sand in 1916 (during World War I) for use in manufacturing gas mantles for various lighting devices. Process wastes from manufacturing operations were pumped to two areas surrounded by earthen dikes on property west of the plant. Subsequently, some of the contaminated wastes migrated onto adjacent and vicinity properties.

In 1928 and again between 1944 and 1946, some of the residues from the processing operations were moved from the company's property and used as mulch and fill in nearby low-lying areas. The fill material consisted of tea and coca leaves mixed with other material resulting from operations at the plant. Some fill material apparently contained thorium process wastes (Ref. 3).

Uncertainty exists as to how the properties in Lodi were contaminated. According to an area resident, fill from an unknown source was brought to Lodi and spread over large portions of the previously low-lying and swampy area. For several reasons, however, a more plausible explanation is that the contamination migrated along a drainage ditch originating on the Maywood Chemical Works property. First, it can be seen from photographs and tax maps of the area that the course of a previously existing stream known as Lodi Brook, which originated at the former Maywood Chemical Works, generally coincides with the path of contamination in Lodi. The brook was subsequently replaced by a storm drain system as the area was developed. Second, samples taken from Lodi properties indicate elevated concentrations of a series of elements known as rare earths. Rare earth elements are typically found in monazite sands, which also contain

thorium. This type of sand was feedstock at the Maywood Chemical Works, and elevated levels are known to exist in the by-product of the extraction process. Third, the ratio of thorium to other radionuclides found on these Lodi properties is comparable to the ratio found in contaminated material on other properties in Lodi (Ref. 4). And finally, long-time residents of Lodi recalled chemical odors in and around the brook in Lodi and steam rising off the water. These observations suggest that discharges of contaminants occurred upstream.

The Stepan Chemical Company (now called the Stepan Company) purchased Maywood Chemical Works in 1959. The Stepan Company itself has never been involved in the manufacture or processing of any radioactive materials (Ref. 5).

2.1 PREVIOUS RADIOLOGICAL SURVEYS

Numerous surveys of the Maywood site and its vicinity properties have been conducted. Among the past surveys, three that are pertinent to this vicinity property are detailed in this section.

January 1981--The Nuclear Regulatory Commission directed that a survey be conducted of the Stepan Company property and its vicinity properties in January 1981. Using the Stepan Company plant as the center, a 10.3-km^2 (4-mi^2) aerial survey was conducted by the EG&G Energy Measurements Group, which identified anomalous concentrations of thorium-232 to the north and south of the Stepan Company property. The Lodi vicinity properties were included in this survey (Ref. 6).

June 1984--In June 1984, Oak Ridge National Laboratory (ORNL) conducted a "drive-by" survey of Lodi using its

"scanning van." Although not comprehensive, the survey indicated areas requiring further investigation (Ref. 7).

September 1986--At the request of DOE, ORNL conducted radiological surveys of the vicinity properties in Lodi in September 1986 to determine which properties contained radioactive contamination in excess of DOE guidelines and would, therefore, require remedial action (Ref. 8).

2.2 REMEDIAL ACTION GUIDELINES

Table 2-1 summarizes the DOE guidelines for residual contamination. The thorium-232 and radium-226 limits listed in Table 2-1 will be used to determine the extent of remedial action required at the vicinity properties. DOE developed these guidelines to be consistent with the guidelines established by the U.S. Environmental Protection Agency (EPA) for the Uranium Mill Tailings Remedial Action Program.

TABLE 2-1
SUMMARY OF RESIDUAL CONTAMINATION GUIDELINES

BASIC DOSE LIMITS

The basic limit for the annual radiation dose received by an individual member of the general public is 100 mrem/yr.

SOIL GUIDELINES

Radionuclide	Soil Concentration (pCi/g) Above Background[a,b,c]
Radium-226 Radium-228 Thorium-230 Thorium-232	5 pCi/g when averaged over the first 15 cm of soil below the surface; 15 pCi/g when averaged over any 15-cm-thick soil layer below the surface layer.
Other Radionuclides	Soil guidelines will be calculated on a site-specific basis using the DOE manual developed for this use.

STRUCTURE GUIDELINES

Airborne Radon Decay Products

Generic guidelines for concentrations of airborne radon decay products shall apply to existing occupied or habitable structures on private property that has no radiological restrictions on its use; structures that will be demolished or buried are excluded. The applicable generic guideline (40 CFR 192) is: In any occupied or habitable building, the objective of remedial action shall be, and reasonable effort shall be made to achieve, an annual average (or equivalent) radon decay product concentration (including background) not to exceed 0.02 WL[d]. In any case, the radon decay product concentration (including background) shall not exceed 0.03 WL. Remedial actions are not required in order to comply with this guideline when there is reasonable assurance that residual radioactive materials are not the cause.

External Gamma Radiation

The average level of gamma radiation inside a building or habitable structure on a site that has no radiological restrictions on its use shall not exceed the background level by more than 20 μR/h.

Indoor/Outdoor Structure Surface Contamination

Radionuclide[f]	Allowable Surface Residual Contamination[e] (dpm/100 cm²) Average[g,h]	Maximum[h,i]	Removable[h,j]
Transuranics, Ra-226, Ra-228, Th-230, Th-228 Pa-231, Ac-227, I-125, I-129	100	300	20
Th-Natural, Th-232, Sr-90, Ra-223, Ra-224 U-232, I-126, I-131, I-133	1,000	3,000	200
U-Natural, U-235, U-238, and associated decay products	5,000 α	15,000 α	1,000 α
Beta-gamma emitters (radionuclides with decay modes other than alpha emission or spontaneous fission) except Sr-90 and others noted above	5,000 β - γ	15,000 β - γ	1,000 β - γ

TABLE 2-1
(CONTINUED)

[a]These guidelines take into account ingrowth of radium-226 from thorium-230 and of radium-228 from thorium-232, and assume secular equilibrium. If either thorium-230 and radium-226 or thorium-232 and radium-228 are both present, not in secular equilibrium, the guidelines apply to the higher concentration. If other mixtures of radionuclides occur, the concentrations of individual radionuclides shall be reduced so that 1) the dose for the mixtures will not exceed the basic dose limit, or 2) the sum of ratios of the soil concentration of each radionuclide to the allowable limit for that radionuclide will not exceed 1 ("unity").

[b]These guidelines represent allowable residual concentrations above background averaged across any 15-cm-thick layer to any depth and over any contiguous 100-m^2 surface area.

[c]Localized concentrations in excess of these limits are allowable, provided that the average concentration over a 100-m^2 area does not exceed these limits. In addition, every reasonable effort shall be made to remove any source of radionuclide that exceeds 30 times the appropriate soil limit, regardless of the average concentration in the soil.

[d]A working level (WL) is any combination of short-lived radon decay products in 1 liter of air that will result in the ultimate emission of 1.3 x 105 MeV of potential alpha energy.

[e]As used in this table, dpm (disintegrations per minute) means the rate of emission by radioactive material as determined by correcting the counts per minute observed by an appropriate detector for background, efficiency, and geometric factors associated with the instrumentation.

[f]Where surface contamination by both alpha- and beta-gamma-emitting radionuclides exists, the limits established for alpha- and beta-gamma-emitting radionuclides should apply independently.

[g]Measurements of average contamination should not be averaged over more than 1 m^2. For objects of less surface area, the average shall be derived for each such object.

[h]The average and maximum radiation levels associated with surface contamination resulting from beta-gamma emitters should not exceed 0.2 mrad/h and 1.0 mrad/h, respectively, at 1 cm.

[i]The maximum contamination level applies to an area of not more than 100 cm^2.

[j]The amount of removable radioactive material per 100 cm^2 of surface area should be determined by wiping that area with dry filter or soft absorbent paper, applying moderate pressure, and measuring the amount of radioactive material on the wipe with an appropriate instrument of known efficiency. When removable contamination on objects of surface area less than 100 cm^2 is determined, the activity per unit area should be based on the actual area and the entire surface should be wiped. The numbers in this column are maximum amounts.

3.0 HEALTH AND SAFETY PLAN

BNI is responsible for protecting the health of personnel assigned to work at the site. As such, all subcontractors and their personnel were required to comply with the provisions of BNI health and safety requirements and as directed by the on-site BNI Health and Safety Officer.

3.1 SUBCONTRACTOR TRAINING

Before the start of work, all subcontractor personnel attended an orientation session presented by the BNI Health and Safety Officer to explain the nature of the material to be encountered in the work and the personnel monitoring and safety measures that are required.

3.2 SAFETY REQUIREMENTS

Subcontractor personnel complied with the following BNI requirements:

- Bioassay--Subcontractor personnel submitted bioassay samples before or at the beginning of on-site activity, upon completion of the activity, and periodically during site activities as requested by BNI.
- Protective Clothing/Equipment--Subcontractor personnel were required to wear the protective clothing/equipment specified in the subcontract or as directed by the BNI Health and Safety Officer.
- Dosimetry--Subcontractor personnel were required to wear and return daily the dosimeters and monitors issued by BNI.
- Controlled Area Access/Egress--Subcontractor personnel and equipment entering areas where access and egress were controlled for radiation and/or chemical safety purposes were surveyed by the BNI Health and Safety Officer (or personnel representing BNI) for contamination before leaving those areas.

- Medical Surveillance--Upon written direction from BNI, subcontractor personnel who work in areas where hazardous chemicals might exist were given a baseline and periodic health assessment defined in BNI's Medical Surveillance Program.

Radiation and/or chemical safety surveillance of all activities related to the scope of work was under the direct supervision of personnel representing BNI.

Health and safety-related requirements for all activities involving exposure to radiation, radioactive material, chemicals, and/or chemically contaminated materials and other associated industrial safety hazards are generated in compliance with applicable regulatory requirements and industry-wide standards. Copies of these requirements are located at the BNI project office for use by project personnel.

4.0 CHARACTERIZATION PROCEDURES

A master grid was established by the surveyor. BNI's radiological support subcontractor, Thermo Analytical/Eberline (TMA/E), established a grid on individual properties. The size of the grid blocks was adjusted to characterize each property adequately. The grid origin allows the grid to be reestablished during remedial action and is correlated with the New Jersey state grid system. All data correspond to coordinates on the characterization grid. The grid with the east and north coordinates is shown on all figures included in Sections 4.0 and 5.0 of this report.

4.1 FIELD RADIOLOGICAL CHARACTERIZATION

This section provides a description of the instrumentation and methodologies used to obtain exterior surface and subsurface measurements during radiological characterization of this property.

4.1.1 Measurements Taken and Methods Used

An initial walkover survey was performed using an unshielded gamma scintillation detector [5.0- by 5.0-cm (2- by 2-in.) thallium-activated sodium iodide probe] to identify areas of elevated radionuclide activity. Near-surface gamma measurements taken using a cone-shielded gamma scintillation detector were also used to determine areas of surface contamination. The shielded detector ensured that the majority of the radiation detected by the instrument originated from the ground directly beneath the unit. Shielding against lateral gamma flux, or shine, from nearby areas of contamination minimized potential sources of error in the measurements. The measurements were taken 30.4 cm (12 in.) above the ground at the intersections of

3.0-m (10-ft) grid lines. The shielded detector was calibrated at the Technical Measurements Center (TMC) in Grand Junction, Colorado, to provide a correlation of counts per minute (cpm) to picocuries per gram (pCi/g). This calibration demonstrated that approximately 11,000 cpm corresponds to the DOE guideline of 5 pCi/g plus local average background of 1 pCi/g for thorium-232 in surface soils (Ref. 9).

A subsurface investigation was conducted to determine the depth to which the previously identified surface contamination extended and to locate subsurface contamination where there was no surface manifestation. The subsurface characterization consisted of drilling 13 boreholes (Figure 4-1), using either a 7.6-cm- (3-in.-) or 15.2-cm- (6-in.-) diameter auger bit, and gamma logging them. The boreholes were drilled to depths determined in the field by the radiological and geological support representatives.

The downhole gamma logging technique was used because the procedure can be accomplished in less time than collecting soil samples, and the need for analyzing these samples in a laboratory is eliminated. A 5.0- by 5.0-cm (2- by 2-in.) sodium iodide gamma scintillation detector was used to perform the downhole logging. The instrument was calibrated at TMC where it was determined that a count rate of approximately 40,000 cpm corresponds to the 15-pCi/g subsurface contamination guideline for thorium-232. This relationship has also been corroborated by results from previous characterizations where thorium-232 was found (Ref. 9).

Gamma radiation measurements were taken at 15.2-cm (6-in.) vertical intervals to determine the depth and concentration

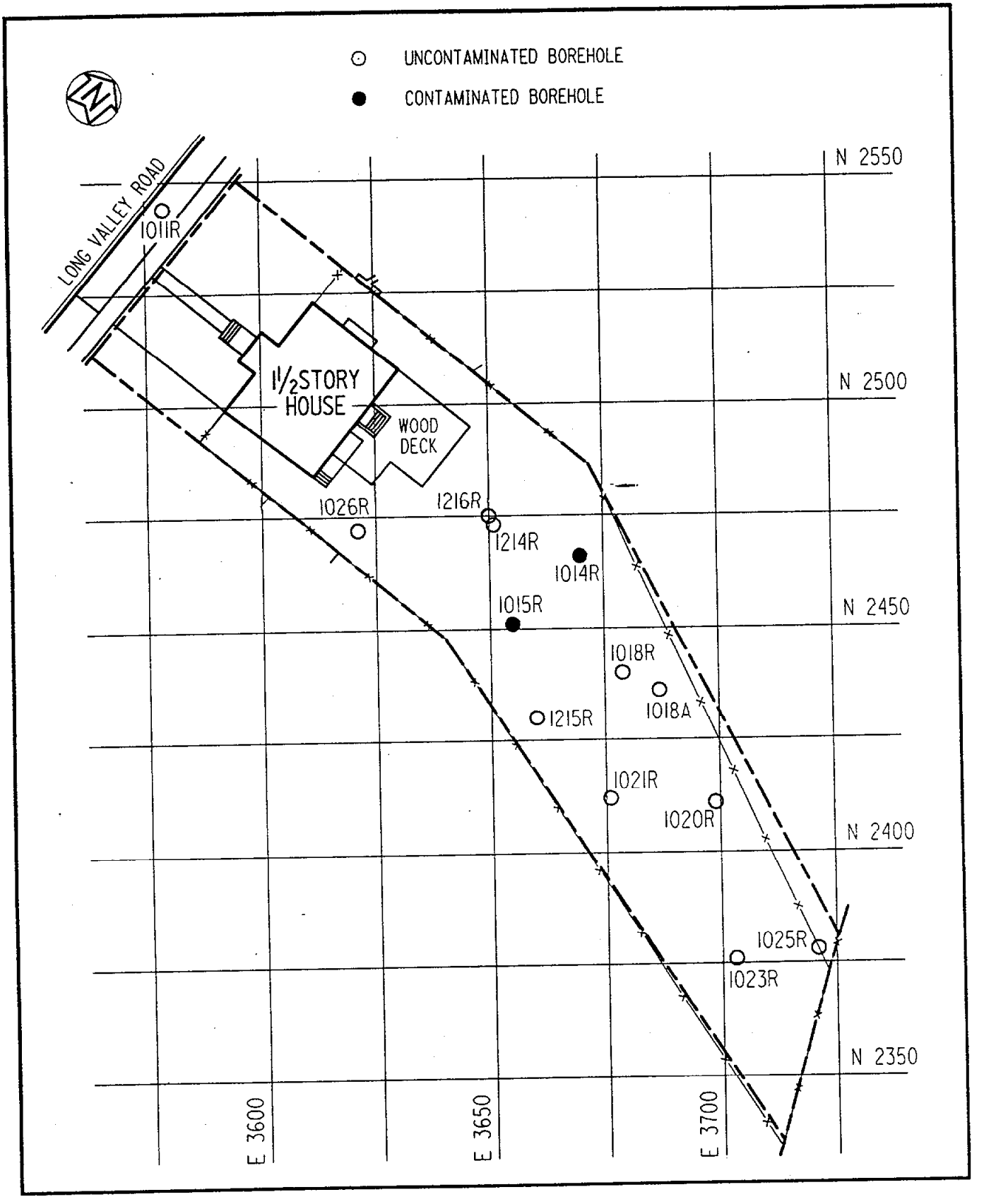

FIGURE 4-1 BOREHOLE LOCATIONS AT 14 LONG VALLEY ROAD

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of the contamination. The gamma-logging data were reviewed to identify trends, whether or not concentrations exceeded the guidelines.

4.1.2 Sample Collection and Analysis

To identify surface areas where the level of contamination exceeded the DOE guideline of 5 pCi/g for thorium-232, areas with measurements of more than 11,000 cpm were plotted. Using these data as well as data from previous surveys (Refs. 5, 6, 7, and 8), the locations of biased surface soil samples were selected to better define the limits of contamination. Surface soil samples were taken at seven locations (Figure 4-2) and analyzed for thorium-232, uranium-238, and radium-226. Each sample was dried, pulverized, and counted for 10 min using an intrinsic germanium detector housed in a lead counting cave lined with cadmium and copper. The pulse height distribution was sorted using a computer-based, multichannel analyzer. Radionuclide concentrations were determined by comparing the gamma spectrum of each sample with the spectrum of a certified counting standard for the radionuclide of interest.

Subsurface soil samples were collected from 15 locations (Figure 4-2) using a 7.6-cm (3.0-in.) outside diameter (O.D.) split-spoon sampler mounted on a tripod or attached to a truck mounted auger stem. The subsurface soil samples were analyzed for radium-226, uranium-238, and thorium-232 in the same manner as the surface soil samples.

4.2 BUILDING RADIOLOGICAL CHARACTERIZATION

After evaluating previous radiological survey data as well as data from this characterization, it was suspected that contamination might be present under the foundation of the

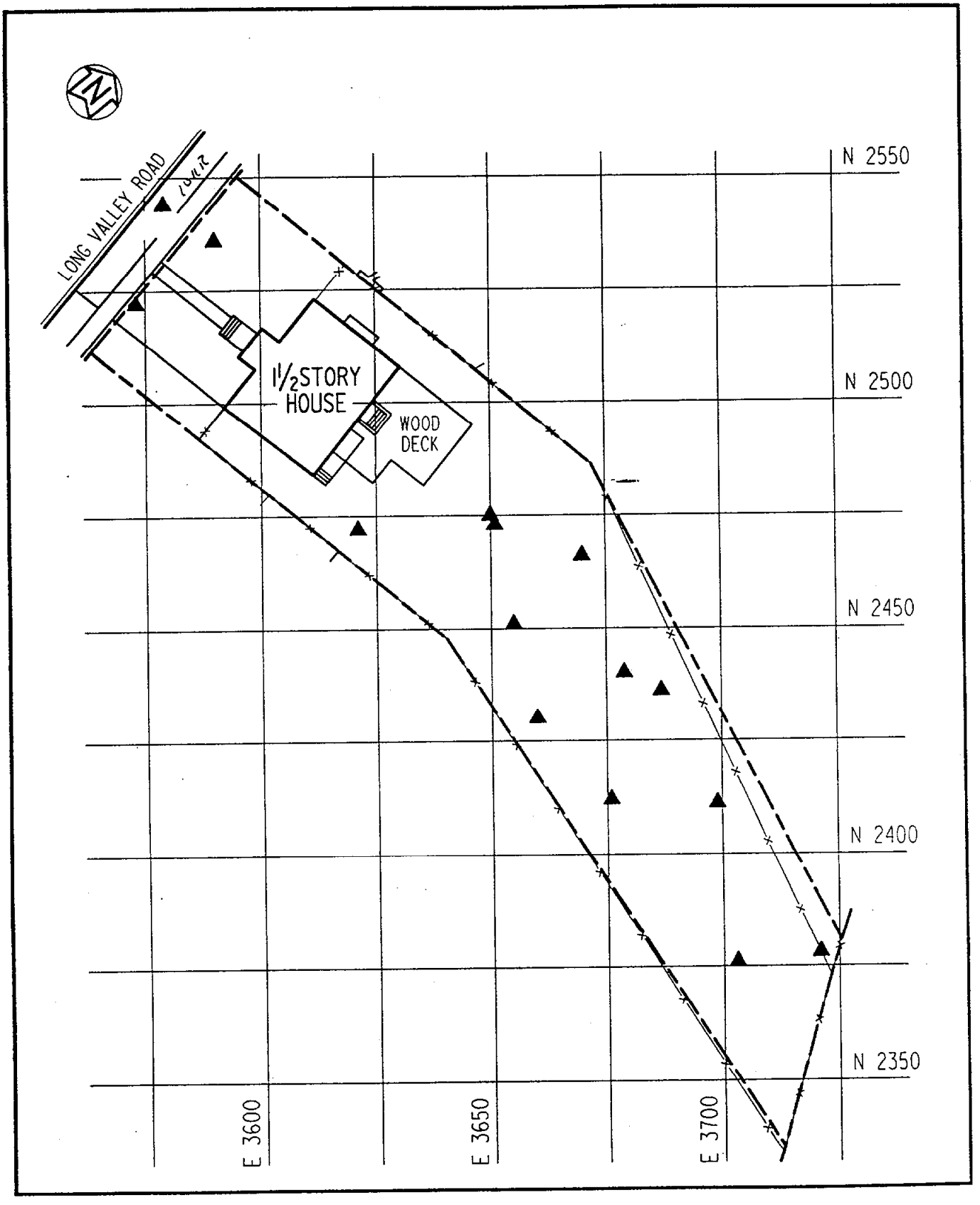

FIGURE 4-2 SURFACE AND SUBSURFACE SOIL SAMPLING LOCATIONS AT 14 LONG VALLEY ROAD

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residence. Because access to the residence was denied by the owner, a radon measurement could not be obtained to verify the presence of contaminated material under the residence and to estimate potential occupational exposures during future remedial actions.

Indoor measurements for radon progeny (radon and thoron daughters) could not be obtained.

Exterior gamma exposure rate measurements were made at 13 locations throughout the property grid system. To obtain exterior measurements, either a 5.0- by 5.0-cm (2- by 2-in.) thallium-activated sodium iodide gamma scintillation detector designed to detect gamma radiation only or a pressurized ionization chamber (PIC) was used. Measurement locations are shown in Figure 4-3. The PIC instrument has a response to gamma radiation that is proportional to exposure in roentgens. A conversion factor for gamma scintillation to the PIC was established through a correlation of these two measurements at four locations in the vicinity of the property. The unshielded gamma scintillation detector readings were then used to estimate gamma exposure rates for each location. These measurements were taken 1 m (3 ft) above the ground. The locations were determined to be representative of the entire property.

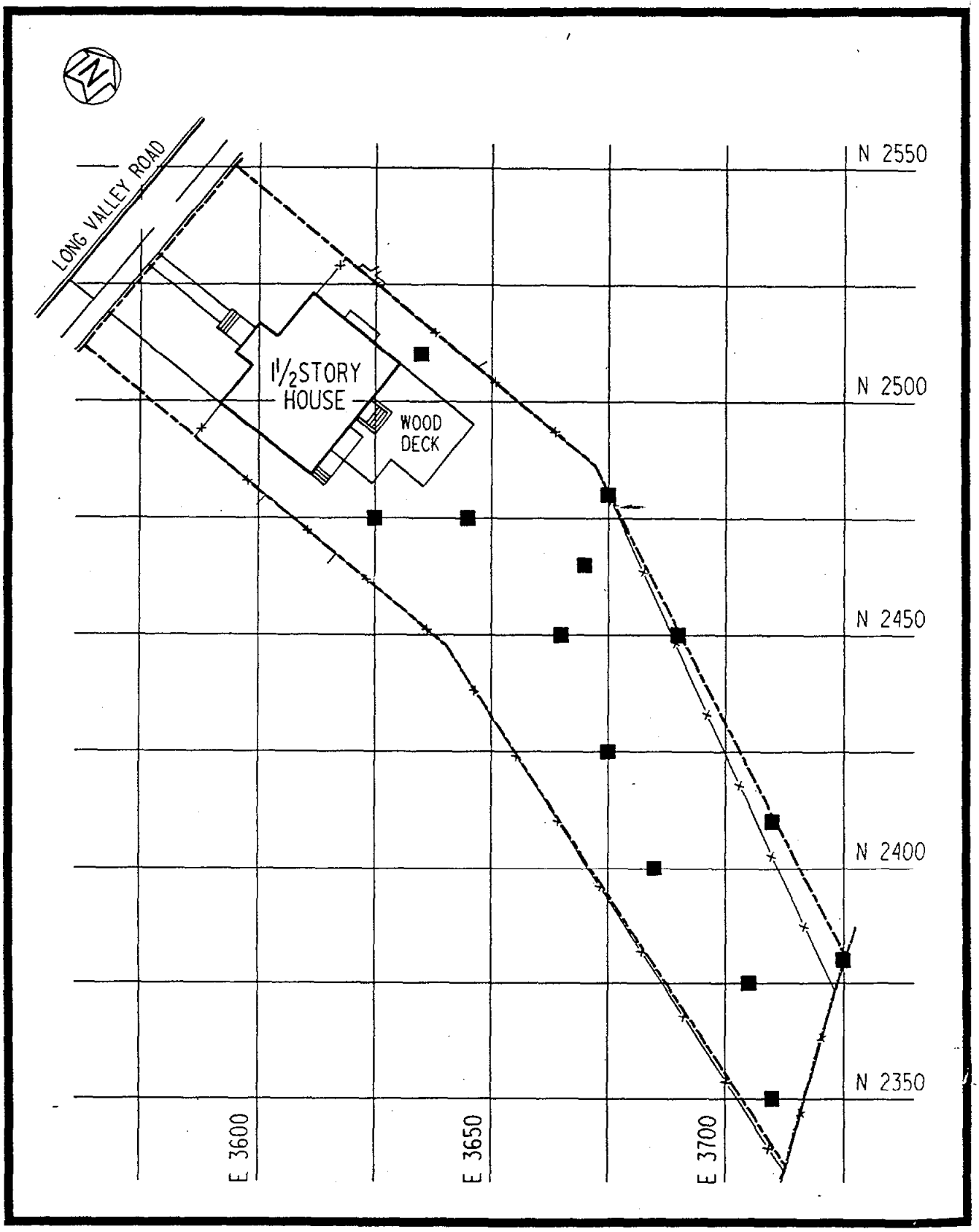

FIGURE 4-3 GAMMA EXPOSURE RATE MEASUREMENT LOCATIONS AT 14 LONG VALLEY ROAD

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5.0 CHARACTERIZATION RESULTS

Radiological characterization results are presented in this section. The data included represent exterior surface and subsurface radiation measurements and interior radiation measurements.

5.1 FIELD RADIOLOGICAL CHARACTERIZATION

Near-surface gamma radiation measurements on the property ranged from 5,000 cpm to approximately 88,000 cpm. The average background level for this area is 5,000 cpm. A measurement of 11,000 cpm is approximately equal to the DOE guideline for thorium-232 of 5 pCi/g above background for surface soil contamination. Using this correlation, the near-surface gamma measurements were used to determine the extent of surface contamination and the basis for selecting the locations of soil samples. Areas of surface contamination are shown in Figure 5-1.

Surface soil samples [depths from 0.0 to 15.2 cm (6.0 in.)] were taken at seven locations on the property (Figure 4-2). These samples were analyzed for thorium-232, uranium-238, and radium-226. The concentrations in these samples ranged from less than 4.5 to less than 10.3 pCi/g for uranium-238, from less than 1.5 to 14.4 pCi/g for thorium-232, and from less than 0.9 to 1.7 pCi/g for radium-226. Analytical results for surface soils are provided in Table 5-1; these data showed that concentrations of thorium-232 exceeded DOE guidelines (5 pCi/g plus background of 1 pCi/g for surface soils) with a maximum concentration of 14.4 pCi/g. Use of the "less than" (<) notation in reporting results indicates that the radionuclide was not present in concentrations that are quantitative with the instruments and techniques used. The "less than" value represents the lower bound of the

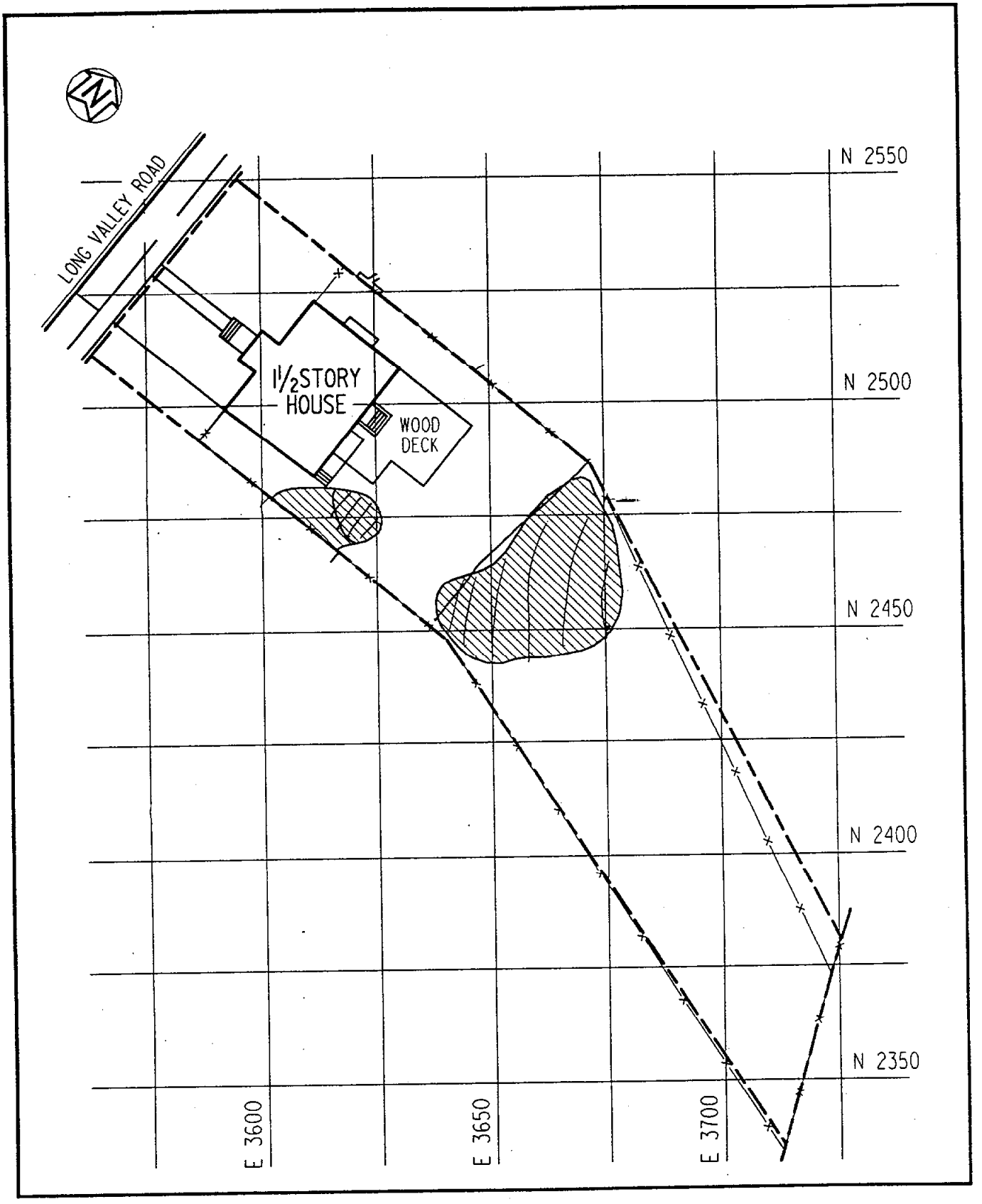

FIGURE 5-1 AREAS OF SURFACE CONTAMINATION AT 14 LONG VALLEY ROAD

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quantitative capacity of the instrument and technique used. The "less than" value is based on various factors, including the volume, size, and weight of the sample; the type of detector used; the counting time; and the background count rate. The actual concentration of the radionuclide is less than the value indicated. In addition, since radioactive decay is a random process, a correlation between the rate of disintegration and a given radionuclide concentration cannot be precisely established. For this reason, the exact concentration of the radionuclide cannot be determined. As such, each value that can be quantitatively determined has an associated uncertainty term (±), which represents the amount by which the actual concentration can be expected to differ from the value given in the table. The uncertainty term has an associated confidence level of 95 percent.

Thorium-232, the primary contaminant at the site, is the radionuclide most likely to exceed a specific DOE guideline in soil. Parameters for soil sample analysis were selected to ensure that the thorium-232 would be detected and measured at concentrations well below the lower guideline value of 5 pCi/g in excess of background level. Radionuclides of the uranium series, specifically uranium-238 and radium-226, are also potential contaminants but at lower concentrations than thorium-232. Therefore, these radionuclides (considered secondary contaminants) would not be present in concentrations in excess of guidelines unless thorium-232 was also present in concentrations in excess of its guideline level. Parameters selected for the thorium-232 analyses also provide detection sensitivities for uranium-238 and radium-226 that demonstrate that concentrations of these radionuclides are below guidelines. However, because of the relatively low gamma photon abundance of uranium-238, many of the uranium-238 concentrations were below the detection sensitivity of the analytical procedure; these concentrations

are reported in the data tables as "less than" values. To obtain more sensitive readings for the uranium-238 radionuclide with these analytical methods, much longer instrument counting times would be required than were necessary for analysis of thorium-232, the primary contaminant.

Analytical results for subsurface soil samples are given in Table 5-1, and gamma logging data are given in Table 5-2. The results in Table 5-2 showed a range from 7,000 cpm to 45,000 cpm. A measurement of 40,000 cpm is approximately equal to the DOE guideline for subsurface contamination of 15 pCi/g. Analyses of subsurface soil samples indicated uranium-238 concentrations ranging from 1.7 to 32.8 pCi/g, thorium-232 concentrations ranging from less than 0.8 to 8.7 pCi/g, and radium-226 concentrations ranging from less than 0.5 to less than 2.1 pCi/g.

On the basis of near-surface gamma radiation measurements, surface and subsurface soil sample analyses, and downhole gamma logging, contamination on this property is believed to consist of surface contamination and subsurface contamination at depths ranging from 15.2 cm (6.0 in.) to 0.30 m (1.0 ft). The areas of subsurface contamination are shown in Figure 5-2.

It is apparent from review of historical documentation (e.g., aerial photographs of the area, interviews with local residents, and previous radiological surveys) that the subsurface contamination on this property lies along the former channel of Lodi Brook and its associated floodplain. The contamination on this property is similar to contamination found on residential properties in close proximity to this property.

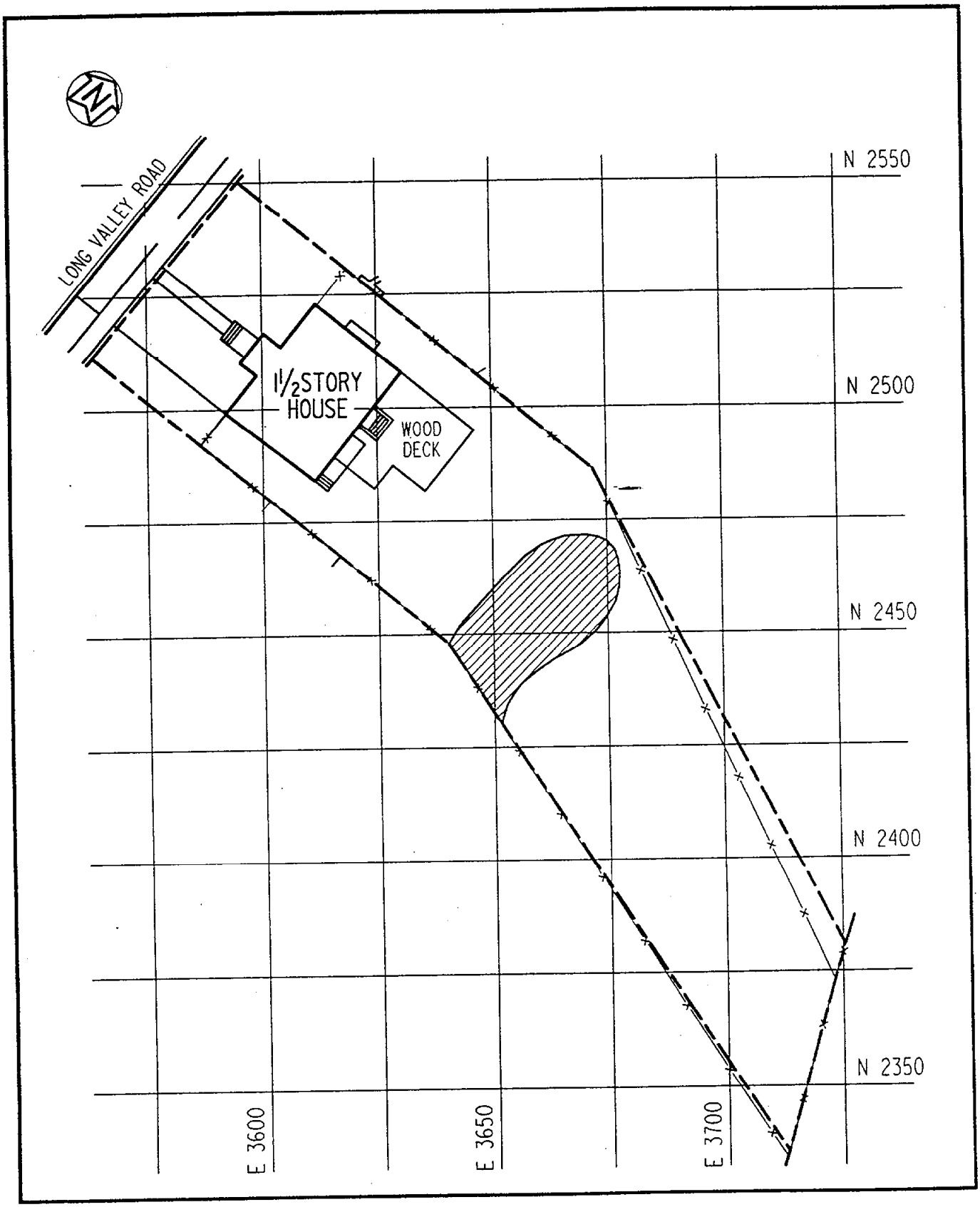

FIGURE 5-2 AREAS OF SUBSURFACE CONTAMINATION AT 14 LONG VALLEY ROAD

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It has been established that the Lodi Brook channel through these neighboring properties once occupied locations connecting to those where stream sediments were found at 14 Long Valley Road. Thus, the elevated gamma readings shown on gamma logs from boreholes drilled on this property serve as further indication of the suspected mechanism of transport for radiological contamination (i.e., stream deposition from Lodi Brook).

The vertical and horizontal limits of contamination as determined by this characterization effort are being evaluated to determine the volume of contaminated material that will require remedial action. To develop this estimate, BNI will consider the location of the contamination, construction techniques, and safety procedures.

5.2 BUILDING RADIOLOGICAL CHARACTERIZATION

Indoor measurements for radon and its progeny (radon and thoron daughters) could not be obtained because access to the residence was denied by the owner.

Exterior gamma radiation exposure rate measurements ranged from 5 to 49 μR/h, including background. These results can be found in Table 5-3.

Assuming the indoor exposure rate is equivalent to the average exterior exposure rate of 13 μR/h, and assuming the resident remains on the property every hour of the year, a yearly dose of 35 mrem could be expected (after subtracting average background of 9 μR/h; Ref. 10). The DOE guideline is 100 mrem/yr above background.

Based on the above information, the exposure rates and doses at this property are within DOE guidelines. Further, it

should be emphasized that natural background exposure rates vary widely across the United States and are often significantly higher than average background for this area.

TABLE 5-1

SURFACE AND SUBSURFACE RADIONUCLIDE CONCENTRATIONS IN SOIL

FOR 14 LONG VALLEY ROAD

Coordinates[a] East	Coordinates[a] North	Depth (ft)	Concentration (pCi/g ± 2 sigma) Uranium-238	Radium-226	Thorium-232
3573	2522	0.0 - 1.0	< 5.6	< 1.4	< 2.4
3573	2522	1.0 - 2.0	< 2.4	< 0.8	< 0.9
3573	2522	2.0 - 3.8	< 2.4	< 0.5	< 0.8
3579	2544	0.0 - 1.0	< 5.0	< 0.9	< 2.2
3579	2544	1.0 - 2.0	< 4.2	< 0.7	< 1.4
3579	2544	2.0 - 3.3	< 3.3	< 0.7	< 1.3
3579	2544	3.3 - 3.7	< 3.4	< 0.7	< 1.2
3579	2544	4.5 - 5.2	< 2.7	< 0.7	< 1.0
3579	2544	5.2 - 6.0	< 2.8	< 0.6	< 1.1
3579	2544	6.0 - 7.4	< 2.8	< 0.6	< 0.9
3579	2544	7.4 - 9.0	< 2.4	< 0.5	< 0.8
3579	2544	9.0 - 9.5	< 3.5	< 0.7	< 1.2
3579	2544	9.5 - 10.0	< 2.8	< 0.7	< 0.9
3579	2544	10.0 - 10.5	< 4.7	< 1.3	< 1.9
3579	2544	10.5 - 11.2	< 1.8	< 0.5	< 0.8
3579	2544	11.2 - 11.5	< 6.4	< 1.4	< 1.7
3590	2536	0.0 - 1.0	< 7.4	< 1.6	< 2.8
3590	2536	1.0 - 2.0	< 4.6	< 0.8	< 1.4
3590	2536	2.0 - 3.5	< 3.2	< 0.8	< 1.3
3621	2472	0.0 - 1.0	< 4.1	< 0.9	< 1.4
3621	2472	3.5 - 4.5	< 4.2	< 1.1	< 1.2
3621	2472	7.5 - 8.0	< 2.4	< 0.7	< 1.0

TABLE 5-1

(continued)

Coordinates[a] East	Coordinates[a] North	Depth (ft)	Concentration (pCi/g ± 2 sigma) Uranium-238	Radium-226	Thorium-232
3650	2475	0.0 - 1.0	< 5.6	< 1.4	< 2.3
3650	2475	3.0 - 4.0	< 4.3	< 1.0	< 1.8
3650	2475	6.0 - 7.0	< 3.5	< 0.8	< 1.2
3650	2475	7.0 - 8.0	< 4.5	< 1.0	< 1.6
3651	2473	0.0 - 0.5	< 5.4	< 1.4	< 2.4
3651	2473	3.0 - 5.0	< 4.0	< 1.0	< 1.3
3651	2473	5.0 - 7.0	< 2.6	< 0.5	< 0.9
3651	2473	7.0 - 8.5	< 3.7	< 0.8	< 1.1
3651	2473	8.5 - 9.5	< 3.2	< 0.7	< 1.0
3655	2451	0.0 - 0.5	< 10.3	< 1.7	14.4 ± 2.4
3655	2451	0.0 - 1.0	< 5.1	< 1.1	8.7 ± 1.2
3655	2451	2.0 - 3.3	< 5.3	< 1.2	< 1.6
3655	2451	4.0 - 5.5	< 2.8	< 0.6	< 1.2
3655	2451	5.5 - 6.0	< 5.5	< 1.5	< 2.1
3660	2430	0.0 - 0.5	< 7.0	< 1.5	< 2.2
3660	2430	2.0 - 3.0	< 4.7	< 1.0	< 1.6
3660	2430	3.0 - 4.0	< 3.0	< 0.6	< 1.2
3660	2430	5.0 - 6.0	< 3.5	< 0.7	< 1.1
3670	2466	0.0 - 1.0	32.8 ± 14.2	1.7 ± 0.6	7.8 ± 1.5
3670	2466	1.0 - 2.0	< 2.0	0.9 ± 0.3	4.0 ± 2.5
3670	2466	2.0 - 2.8	< 2.0	0.7 ± 0.4	1.3 ± 0.2
3670	2466	5.5 - 7.3	< 2.0	0.7 ± 0.1	1.3 ± 0.5
3670	2466	7.0 - 8.0	< 2.0	0.5 ± 0.2	1.2 ± 0.4
3670	2466	8.0 - 12.0	< 2.0	0.8 ± 0.3	1.9 ± 0.1
3670	2466	12.0 - 13.0	1.7 ± 1.7	0.8 ± 0.4	1.2 ± 0.6

TABLE 5-1

(continued)

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Coordinates[a] East	Coordinates[a] North	Depth (ft)	Concentration (pCi/g ± 2 sigma) Uranium-238	Radium-226	Thorium-232
3676	2412	0.0 - 0.5	< 5.0	< 1.1	< 1.5
3676	2412	2.0 - 3.2	< 4.0	< 0.9	< 1.7
3676	2412	4.7 - 5.0	< 4.5	< 0.8	< 1.4
3679	2440	0.0 - 1.0	< 3.6	< 1.0	< 1.6
3679	2440	2.0 - 2.8	< 3.7	< 1.0	< 1.4
3679	2440	2.8 - 3.4	< 2.1	< 0.6	< 0.9
3679	2440	3.4 - 3.6	< 2.2	< 0.5	< 0.9
3679	2440	3.6 - 3.8	< 4.9	< 1.2	< 1.6
3681	2436	0.0 - 0.5	< 8.1	< 2.1	< 2.9
3681	2436	2.0 - 3.0	< 2.9	< 0.7	< 1.1
3681	2436	3.0 - 3.5	< 4.9	< 1.1	< 1.5
3699	2411	0.0 - 0.5	< 4.5	< 0.9	< 1.5
3699	2411	2.0 - 2.7	< 2.5	< 0.8	< 1.1
3699	2411	2.7 - 3.0	< 4.6	< 1.1	< 1.5
3699	2411	4.5 - 5.8	< 1.9	< 0.6	< 0.8
3703	2376	0.0 - 1.0	< 6.8	< 1.6	< 2.1
3703	2376	2.0 - 3.5	< 4.5	< 0.9	< 1.4
3703	2376	4.3 - 5.2	< 7.4	< 1.6	< 2.2
3721	2378	0.0 - 0.5	< 4.5	< 1.3	< 1.5
3721	2378	2.0 - 2.5	< 4.6	< 1.1	< 1.3
3721	2378	3.5 - 4.5	< 3.3	< 0.7	< 1.0

[a]Sampling locations are shown in Figure 4-2.

TABLE 5-2

DOWNHOLE GAMMA LOGGING RESULTS

FOR 14 LONG VALLEY ROAD

Coordinates[a] East	Coordinates[a] North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 1011R[d]			
3579	2544	0.5	9000
3579	2544	1.0	10000
3579	2544	1.5	11000
3579	2544	2.0	11000
3579	2544	2.5	10000
3579	2544	3.0	10000
3579	2544	3.5	10000
3579	2544	4.0	8000
3579	2544	4.5	8000
3579	2544	5.0	8000
3579	2544	5.5	7000
3579	2544	6.0	7000
3579	2544	6.5	7000
Borehole 1026R[d]			
3621	2472	0.5	11000
3621	2472	1.0	12000
3621	2472	1.5	12000
3621	2472	2.0	12000
3621	2472	2.5	13000
3621	2472	3.0	12000
3621	2472	3.5	12000
3621	2472	4.0	13000
3621	2472	4.5	12000
3621	2472	5.0	10000
Borehole 1216R[d]			
3650	2475	0.5	10000
3650	2475	1.0	13000
3650	2475	1.5	12000
3650	2475	2.0	11000
3650	2475	2.5	12000
3650	2475	3.0	5000
3650	2475	3.5	12000
3650	2475	4.0	12000
3650	2475	4.5	12000
3650	2475	5.0	13000

TABLE 5-2

(continued)

Page 2 of 4

Coordinates[a] East	Coordinates[a] North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 1216R (continued)[d]			
3650	2475	5.5	12000
3650	2475	6.0	11000
3650	2475	6.5	12000
3650	2475	7.0	11000
Borehole 1214R[d]			
3651	2473	0.5	12000
3651	2473	1.0	13000
3651	2473	1.5	13000
3651	2473	2.0	18000
3651	2473	2.5	11000
3651	2473	3.0	11000
3651	2473	3.5	11000
Borehole 1015R[d]			
3655	2451	0.5	29000
3655	2451	1.0	20000
3655	2451	1.5	15000
3655	2451	2.0	13000
3655	2451	2.5	12000
3655	2451	3.0	11000
3655	2451	3.5	11000
3655	2451	4.0	11000
3655	2451	4.5	12000
3655	2451	5.0	12000
Borehole 1215R[d]			
3660	2430	0.5	7000
3660	2430	1.0	8000
3660	2430	1.5	7000
3660	2430	2.0	13000
3660	2430	2.5	16000
3660	2430	3.0	7000
3660	2430	3.5	8000
3660	2430	4.0	9000
3660	2430	4.5	8000

TABLE 5-2

(continued)

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Coordinates[a] East	Coordinates[a] North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 1014R[d]			
3670	2466	0.5	36000
3670	2466	1.0	45000
3670	2466	1.5	28000
3670	2466	2.0	17000
3670	2466	2.5	16000
3670	2466	3.0	13000
3670	2466	3.5	12000
3670	2466	4.0	12000
3670	2466	4.5	12000
3670	2466	5.0	13000
3670	2466	5.5	13000
3670	2466	6.0	13000
Borehole 1021R[d]			
3676	2412	0.5	11000
3676	2412	1.0	11000
3676	2412	1.5	11000
3676	2412	2.0	11000
3676	2412	2.5	12000
3676	2412	3.0	11000
3676	2412	3.5	11000
Borehole 1018R[d]			
3679	2440	0.5	11000
3679	2440	1.0	12000
3679	2440	1.5	12000
3679	2440	2.0	11000
3679	2440	2.5	11000
Borehole 1020R[d]			
3699	2411	0.5	12000
3699	2411	1.0	12000
3699	2411	1.5	12000
3699	2411	2.0	12000
3699	2411	2.5	11000
3699	2411	3.0	11000
3699	2411	3.5	11000
3699	2411	4.0	11000

TABLE 5-2

(continued)

Coordinates[a] East	Coordinates[a] North	Depth[b] (ft)	Count Rate[c] (cpm)
Borehole 1023R[d]			
3703	2376	0.5	12000
3703	2376	1.0	12000
3703	2376	1.5	13000
3703	2376	2.0	13000
3703	2376	2.5	12000
3703	2376	3.0	11000
3703	2376	3.5	11000
3703	2376	4.0	12000
Borehole 1025R[d]			
3721	2378	0.5	11000
3721	2378	1.0	11000
3721	2378	1.5	11000
3721	2378	2.0	10000
3721	2378	2.5	11000
3721	2378	3.0	10000

[a]Borehole locations are shown in Figure 4-1.

[b]The variations in depths of boreholes and corresponding results given in this table are based on the boreholes penetrating the contamination or the drill reaching refusal.

[c]Instrument used was 5.0- by 5.0-cm (2- by 2-in.) thallium-activated sodium iodide gamma scintillation detector.

[d]Bottom of borehole collapsed.

TABLE 5-3

GAMMA RADIATION EXPOSURE RATES

FOR 14 LONG VALLEY ROAD

Coordinates[a]		Rate[b]
East	North	(μR/h)
3625	2475	9
3635	2510	10
3645	2475	5
3665	2450	26
3670	2465	49
3675	2425	6
3675	2480	28
3685	2400	4
3690	2450	5
3705	2375	5
3710	2350	5
3710	2410	7
3725	2380	5

[a]Measurement locations are shown in Figure 4-3.

[b]Measurements include background.

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GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1011R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,544 E 3,579	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
9-24-87	9-29-87	G. Engel; BNI	Minuteman Auger	4"	11.5		11.5

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
7.4/64		8			▽ / ▼ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
N/A	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.0	0.5									0.0 - 4.0 Ft. SILT (ML). Dark reddish brown (10YR3/4) with streaks of moderate red (5R4/6). Chunks of brick. (FILL).	Borehole advanced 0-11.5 Ft. using 3" i.d. split-spoon sampler and 4" o.d. solid stem augers.
SS	1.0	0.7										
SS	1.3	0.7									2.0-4.0 Ft. Moderate reddish brown (10YR4/6).	
SS	0.4	0.4										
AU	0.8	0.0										
SS	0.7	0.5									4.0 - 11.5 Ft. Silty SAND (SM). Moderate reddish brown. Very fine- to medium-grained sand.	
SS	0.8	0.8						5				Borehole was radiologically sampled and gamma-logged by TMA-Eberline, Corp.
SS	1.4	1.4										
SS	1.6	0.0									7.0-7.4 Ft. Pale brown (5YR5/2).	
SS	0.5	0.4										
SS	0.5	1.5										
SS	0.5	0.5						10			10.0-11.5 Ft. Increased sand content. Brownish gray (5YR4/1) clumps.	Hole collapsed to 7.0 Ft. Gamma-scanned to 6.5 Ft.
SS	0.7	0.7										
SS	0.3	0.3									Bottom of boring at 11.5 Ft. Borehole backfilled with grout from 7.0 Ft. to the surface, 9/29/87.	
												Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; O = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1011R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1026R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,472 E 3,621	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
10-16-87	10-16-87	G. Engel; BNI	Minuteman Auger	4"	8.0		8.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
6.9/86		9			▽ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
N/A	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.0	0.7									0.0 - 4.9 Ft. Sandy Silty CLAY (CL-ML). Dark reddish brown (10R2/4) mottled with moderate reddish brown (10R4/6). Fine- to coarse-grained and a few pebbles.	Borehole advanced 0-8.0 Ft. using 3" i.d. split-spoon sampler and 0-5.0 Ft. using 4" o.d. solid stem augers.
SS	1.0	0.5									1.0-2.0 Ft. Moderate reddish brown (10R4/6).	
SS	0.5	0.5										
SS	1.3	1.1									2.0-2.5 Ft. Dark reddish brown (10R3/4).	
SS	1.1	1.1						5			3.0-3.7 Ft. Very dusky red (10R2/2) zones 0.1 in. wide.	Borehole was radiologically sampled and gamma-logged by TMA-Eberline, Corp. Augered and gamma-logged to 5.0 Ft.
SS	1.0	0.9									3.8-4.9 Ft. Mottled very dusky red (10R2/2)with grayish red (10R4/2).	
SS	0.6	0.6									4.9 - 6.1 Ft. SAND (SP). Grayish red (5R4/2), fine- to very coarse-grained.	
SS	1.0	1.0									6.1 - 6.5 Ft. Sandy CLAY (CL). Moderate red (5R4/6), fine- to very coarse-grained sand.	
SS	0.5	0.5									6.5 - 7.2 Ft. Clayey SAND (SC). Grayish red (10R4/6), fine- to coarse-grained sand. Increased clay content with depth.	
											7.2 - 8.0 Ft. Sandy CLAY (CL). Moderate red (5R4/6), fine- to very coarse-grained sand. Two large pebbles (>1.0 in.) imbedded in tip of auger bit.	
											Bottom of borehole at 8.0 Ft. Borehole backfilled with spoils, 10/16/87.	

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1026R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1216R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,475 E 3,650	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-9-87	12-9-87	G. Engel; BNI.	Tripod\Little Beaver	4"	8.0		8.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
6.9/86		8				

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./18 in.	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE
SS	1.0	0.8								
SS	1.0	0.9								
SS	1.0	0.9								
SS	1.0	1.0								
SS	1.0	0.4								
SS	1.0	1.0						5		
SS	1.0	0.9								
SS	1.0	1.0								

DESCRIPTION AND CLASSIFICATION

0.0 - 1.2 Ft. Silty CLAY (CL-ML). Dusky yellowish brown (10YR2/2). Humus in upper 0.2 Ft.

1.2 - 3.1 Ft. Clayey SAND (SC). Moderate reddish brown (10R4/6), fine- to coarse-grained with Brunswick Sandstone fragments.

1.2-1.3 Ft. Moderate red (5R4/6).

3.1 - 5.2 Ft. Silty SAND (SM). Pale red (5R6/2), very fine- to fine-grained.

5.2 - 6.1 Ft. Sandy CLAY (CL-ML). Pale reddish brown (10R5/4) mottled with light brown (5YR5/6) and moderate reddish brown (10R4/6).

6.1 - 8.0 Ft. Pebbly clayey silty SAND (SC-GC). Moderate red (5R4/6) to moderate reddish brown (10R4/6). Pebbles to 1" in diam.

Bottom of borehole at 8.0 Ft.
Borehole backfilled with spoils, 11/25/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-8 Ft. with 3" o.d. split-spoon sampler and 4" o.d. solid-stem auger.
Boring radiologically sampled and gamma-logged by TMA-Eberline, Corp.

7.5 Ft. *Auger* refusal.
Gamma-logged to 7.0 Ft.

8.0 Ft. *Spoon* refusal.

Description and classification of samples by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1216R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1214R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,473 E 3,651	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-9-87	12-9-87	G. Engel; BNI.	Tripod/Little Beaver	4"	9.5		9.5

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
6.4/67		7			▽ / ▼ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./18 in.	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE "N" BLOWS % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.0	7.0									0.0 - 1.1 Ft. Silty sandy CLAY (CL-ML). Dusky brown (5YR2/2). Fine- to medium-grained humus.	Borehole advanced 0-9.5 Ft. with 3" o.d. split-spoon sampler and 4" o.d. solid-stem auger. Boring radiologically sampled and gamma-logged by TMA-Eberline, Corp.
SS	1.0	0.6										
SS	1.0	0.7									1.1 - 3.3 Ft. Clayey SAND (SC). Light brownish gray (5YR6/1), layered with moderate reddish brown (10R4/6) that dips about 30 deg.	
SS	2.0	1.0										
SS	2.0	1.1						5			3.2-3.3 Ft. Light gray (N7) irregular zone.	
SS	1.5	1.3									3.3 - 9.5 Ft. Pebbly clayey SAND (SG-SC). Moderate reddish brown (10R4/6). Fine- to very coarse-grained Brunswick SS pebbles to 2 in. or larger. Rounded to subrounded near bottom of hole.	5.5 Ft. Auger refusal.
SS	1.0	1.0									7.5-7.7 Ft. Pebbly zone.	
											9.3-9.5 Ft. Clayey zone.	9.5 Ft. Spoon refusal.
											Bottom of borehole at 9.5 Ft. Borehole backfilled with spoils, 12/9/87.	

Description and classification of samples by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; O = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1214R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1015R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,451 E 3,655	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
10-2-87	10-2-87	G. Engel; BNI	Minuteman Auger	4"	6.0		6.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
3.4/56		6			▽ / ▼ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
N/A	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE "N" BLOWS % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION
SS	1.0	0.5									0.0 - 3.3 Ft. Sandy Silty CLAY (CL-ML). Dusky brown (5YR2/2), mottled with moderate reddish orange (10R6/6).
SS	1.0	0.5									
SS	1.3										
SS	0.9	0.8									3.3 - 4.7 Ft. Silty Clayey SAND (SM). Pale brown (5YR5/2), very fine- to medium-fine grained.
SS	0.5	0.5						5			
SS	0.8	0.6									4.7 - 6.0 Ft. Silty CLAY (CL-ML). Dark reddish brown (10R3/4).
SS	0.5	0.5									
											Bottom of borehole at 6.0 Ft. Borehole backfilled with grout, 10/2/87.

NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.

Borehole advanced 0-6.0 Ft. using 3" i.d. split-spoon sampler and 4" o.d. solid stem augers.

Borehole was radiologically sampled and gamma-logged by TMA-Eberline, Corp.

Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1015R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1215R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,430 E 3,660	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
12-9-87	12-9-87	G. Engel; BNI.	Tripod\Little Beaver	4"	6.0		6.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
5.1/85		6			▽ / ▼ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
140 lbs./18 in.	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE "N" BLOWS % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.0	0.7									0.0 - 1.4 Ft. Sandy silty CLAY (CL-ML). Dusky brown (5YR2/2), fine- to medium-grained, humus.	Borehole advanced 0-6 Ft. with 3" o.d. split-spoon sampler and 4" o.d. solid-stem auger. Boring radiologically sampled and gamma-logged by TMA-Eberline, Corp.
SS	1.0	0.7										
SS	1.0	0.9									1.4 - 3.9 Ft. SAND (SP). Fine- to medium-grained with scattered pebbles up to 0.5" in diam.	
SS	1.0	1.0										
SS	1.0	0.8									2.9-3.9 Ft. Dark yellowish orange (10YR6/6).	
SS	1.0	1.0						5			3.9 - 5.1 Ft. SILT (ML). Light brown (5YR5/6).	5.0 Ft. Auger refusal.
											5.1 - 5.7 Ft. SAND (SP). Moderate brown (5YR4/4) fine- to coarse-grained.	
											5.7 - 6.0 Ft. Pebbly clayey SAND (SC-GC). Moderate reddish brown (10R4/6), fine- to medium-grained with subangular clasts to 3.0" diam.; glacial till?	6.0 Ft. Spoon refusal.
											Bottom of borehole at 6.0 Ft. Borehole backfilled with spoils, 11/25/87.	

Description and classification of samples by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1215R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1014R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,466 E 3,670	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
10-1-87	10-1-87	G. Engel; BNI	Minuteman Auger	4"	13.0		13.0

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
4.9/37		10			▽ / ▼ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
N/A	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.0	0.1									0.0 - 3.8 Ft. Sandy Silty CLAY (CL-ML). Dusky red (5R3/4). Fine- to medium-grained sand component. Pebbly with up to 1.0 in. mottled blackish red (5R2/2) pebbles.	Borehole advanced 0-13.0 Ft. using 3" i.d. split-spoon sampler and 4" o.d. solid stem augers.
SS	1.0	0.7										
SS	0.8	0.5										
SS	1.0	0.5										
SS	1.0	0.6									3.0 Ft. Decreasing sand content, and no pebbles.	
SS	0.7	0.7						5			3.8 - 7.0 Ft. Clayey SILT (ML-CL). Dark reddish brown (10R3/4).	Borehole was radiologically sampled and gamma-logged by TMA-Eberline, Corp. Sampler unable to advance from 4.8-5.7 Ft. Used grab-sample from the auger flights.
SS	0.2	0.0										
AU	1.6	0.0										
SS	0.8	0.8									7.0 - 12.4 Ft. Silty SAND (SM). Dark reddish brown (10R3/4), fine- to medium-grained.	
AU	3.9	0.0									7.7 Ft. Some pebbles.	Auger refusal at 10.0 Ft. Gamma-scan to this depth.
								10				
SS	1.0	1.0									12.4 - 13.0 Ft. Silty Sandy CLAY (CL-ML). Dark reddish brown (10R3/4), fine- to medium-grained sand.	
											Bottom of borehole at 13.0 Ft. Borehole backfilled with spoils, 10/1/87.	
												Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1014R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1021R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,412 E 3,676	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
10-12-87	10-12-87	G. Engel; BNI	Minuteman Auger	4"	4.6		4.7

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
3.9/82		8			▽ / ▼ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
N/A	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE "N" BLOWS % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.0	0.7									0.0 - 4.7 ft. Silty Sandy CLAY (CL-ML). Dusky brown (5YR2/2) mottled with moderate red (5YR5/4). Fine- to medium-grained with increasing sand with depth.	Borehole advanced 0-4.7 Ft. using 3" i.d. split-spoon sampler and 4" o.d. solid stem augers.
SS	1.0	0.9									1.0-2.0 ft. Moderate brown (5YR4/4).	
SS	1.2	0.9									2.0-3.0 ft. Pale reddish brown (10R5/4).	
SS	0.2	0.2									3.0-3.4 Ft. Moderate red (5R5/4).	Borehole was radiologically sampled and gamma-logged by TMA-Eberline, Corp.
SS	0.4	0.4									3.4-4.7 Ft. Grayish red (5R4/2) and streaks of blackish red (5R2/2). Pieces of Brunswick SS in a matrix of sandy clayey silt.	
SS	0.1	0.1									Bottom of borehole at 4.7 Ft. Borehole backfilled with spoils, 10/12/87.	Auger refusal at 4.7 Ft. Refusal with clay bit at 3.9 Ft.
SS	0.7	0.7										
SS	0.1	0.0										

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

Description and classification of soils by visual examination.

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1021R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1018R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,440 E 3,679	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
10-6-87	10-6-87	G. Engel; BNI	Minuteman Auger	4"	4.5		4.5

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
2.5/65		6			▽ / ▼ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
N/A	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.0	0.5									0.0 - 3.8 Ft. Silty CLAY (CL-ML).	Borehole advanced 0-3.8 Ft. using 3" i.d. split-spoon sampler and to 4.5 ft. using 4" o.d. solid stem augers.
SS	1.0	0.5									0.0-1.0 Ft. Dusky brown (5YR2/2).	
SS	0.8	0.5									1.0-2.0 Ft. Moderate red (5R4/6).	
SS	0.6	0.6									2.0-2.9 Ft. Moderate brown (5YR3/4).	
SS	0.2	0.2									2.8-3.8 Ft. Increasing sand and pebbles with depth.	Borehole was radiologically sampled and gamma-logged by TMA-Eberline, Corp.
											2.9-3.4 Ft. Dusky red (5R3/4).	
											3.4-3.8 Ft. Moderate reddish brown (10R4/6).	
											Bottom of borehole at 4.5 Ft. Borehole backfilled with spoils, 10/6/87.	
												Augered to 4.5 Ft; gamma-logged to 3.5 Ft.
												Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO.: 1018R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1020R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,411 E 3,699	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
10-9-87	10-14-87	G. Engel; BNI	Minuteman Auger	4"	7.5		7.5

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
5.0/94		9			▽ / ▼ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
N/A	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN. CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.0	1.0									0.0 - 3.0 Ft. Silty Sandy CLAY (CL-ML). 0.0-1.0 Ft. Dusky brown (5YR2/1); rich humus appearance. Fine- to medium-grained sand.	Borehole advanced 0-7.5 Ft. using 3" i.d. split-spoon sampler and 4" o.d. solid stem augers.
SS	1.0	1.0									1.0-3.0 Ft. Moderate brown (5YR4/4) mottled with light brown (5YR5/6) and dusky yellowish brown (10YR2/2). Fine- to medium-grained sand.	
SS	0.7	0.6									2.0-3.0 Ft. Decreasing sand.	
~~SS~~	~~0.3~~	~~0.3~~										
~~SS~~	~~0.5~~	~~0.3~~										
~~SS~~	~~0.5~~	~~0.5~~										
~~SS~~	~~0.5~~	~~0.5~~										
SS	0.8	0.8						5			3.0 - 3.5 Ft. Clayey SILT (ML-CL). Grayish red (10R4/2).	Borehole was radiologically sampled and gamma-logged by TMA-Eberline, Corp.
AU	2.2										3.5 - 7.5 Ft. Silty SAND (SM). Moderate reddish brown (10R4/6), very fine- to fine-grained. 4.3-4.9 Ft. Moderate red (5R5/4).	
											4.5-5.3 Ft. Increasing silt content.	Re-augered to 4.6 Ft. on 10/14/87; gamma-logged to 4.0 Ft.
											4.9-5.3 Ft. Grayish red (5R4/2).	
											5.3 Ft. Small rounded pebbles.	
											Bottom of borehole at 7.5 Ft. Borehole backfilled with spoils, 10/14/87.	Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1020R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1023R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,376 E 3,703	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
10-13-87	10-14-87	G. Engel; BNI	Minuteman Auger	4"	10.2		5.2

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
4.1/78		6			▽ / /	

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
N/A	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE "N" BLOWS % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.0	0.7									0.0 - 2.0 Ft. Sandy Silty CLAY (CL-ML). Dusky brown (5Y2/2). Fine- to medium-grained sand. Pieces of paper.	Borehole advanced 0-5.2 Ft. using 3" i.d. split-spoon sampler and 4" o.d. solid stem augers.
SS	1.0	0.9									1.0-2.0 Ft. Moderate reddish brown (10R4/6) mottled with very dusky red (10R2/2).	
SS	1.5	1.5										
SS	0.5	0.5									2.0 - 3.9 Ft. Silty CLAY (CL-ML). Moderate reddish brown (10R4/6) with grayish brown (5YR3/2).	Borehole was radiologically sampled and gamma-logged by TMA-Eberline, Corp.
~~SS~~	~~0.3~~	~~0.3~~						5				
SS	0.9	0.2									3.9 - 5.2 Ft. Clayey SILT (ML-CL). Pale reddish brown (10R5/4), grayish red (10R4/2).	4.6-5.0 Ft. augered with pronounced 'chattering'.
											Bottom of borehole at 5.2 Ft. Borehole backfilled with spoils, 10/14/87.	Augered to 5.0 Ft. and gamma-logged to 4.0 Ft.
												Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1023R

GEOLOGIC DRILL LOG

PROJECT	JOB NO.	SHEET NO.	HOLE NO.
FUSRAP	14501-138	1 OF 1	1025R

SITE	COORDINATES	ANGLE FROM HORIZ	BEARING
14 Long Valley Rd. (LODI)	N 2,378 E 3,721	Vertical	------

BEGUN	COMPLETED	DRILLER	DRILL MAKE AND MODEL	SIZE	OVERBURDEN	ROCK (FT.)	TOTAL DEPTH
10-15-87	10-15-87	G. Engel; BNI	Minuteman Auger	4"	4.2		4.2

CORE RECOVERY (FT./%)	CORE BOXES	SAMPLES	EL. TOP CASING	GROUND EL.	DEPTH/EL. GROUND WATER	DEPTH/EL. TOP OF ROCK
3.4/80		6			▽ / ▼ /	/

SAMPLE HAMMER WEIGHT/FALL	CASING LEFT IN HOLE: DIA./LENGTH	LOGGED BY:
N/A	NONE	R. Migues

SAMP. TYPE AND DIAM.	SAMP. ADV. LEN CORE	SAMPLE REC. CORE REC.	SAMPLE BLOWS "N" % CORE RECOVERY	WATER PRESSURE TESTS: LOSS IN G.P.M	WATER PRESSURE TESTS: PRESS. P.S.I.	WATER PRESSURE TESTS: TIME IN MIN.	ELEV.	DEPTH	GRAPHICS	SAMPLE	DESCRIPTION AND CLASSIFICATION	NOTES ON: WATER LEVELS, WATER RETURN, CHARACTER OF DRILLING, ETC.
SS	1.0	0.5									0.0 - 1.0 Ft. Sandy Silty CLAY (TOPSOIL/CL-ML). Dusky brown (5YR2/2). Fine- to medium-grained. Humus.	Borehole advanced 0-4.2 Ft. using 3" i.d. split-spoon sampler and 4" o.d. solid stem augers.
SS	1.0	0.7									1.0 - 4.2 Ft. Sandy Silty CLAY (CL-ML). Moderate reddish brown, Fine- to coarse-grained with fragments of Brunswick SS up to 1.0 in.	
SS	0.5	0.5									2.0-2.5 Ft. Increasing sand.	Borehole was radiologically sampled and gamma-logged by TMA-Eberline, Corp. Augered and gamma-logged to 2.5 Ft. Refusal on boulder.
SS	0.5	0.5									3.9-4.2 Ft. Grayish red (10R4/2) mixed with very dusky red (10R2/2).	
SS	0.7	0.7									Bottom of borehole at 4.2 Ft. Borehole backfilled with spoils, 10/15/87.	
SS	0.5	0.5										Description and classification of soils by visual examination.

SS = SPLIT SPOON; ST = SHELBY TUBE; D = DENNISON; P = PITCHER; O = OTHER

SITE: 14 Long Valley Rd. (LODI)

HOLE NO. 1025R